

METEOROLOŠKI GODIŠNJAK I

ANNUAIRE METEOROLOGIQUE I

GODINA 1973 ANNÉE

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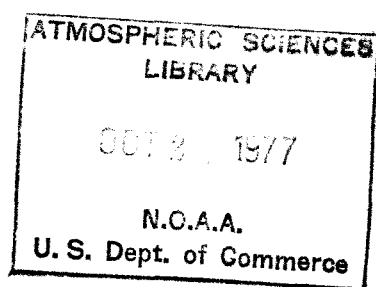
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HIDROMETEOROLŠKA SLUŽBA — SERVICE HYDRO-MÉTÉOROLOGIQUE

D 823

METEOROLOŠKI GODIŠNJAK I

ANNUAIRE MÉTÉOROLOGIQUE I

GODINA 1973 ANNÉE



IZDANJE SAVEZNOG HIDROMETEOROLOŠKOG ZAVODA
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S A D R Ź A J

	Strana
Objašnjenja	
Azbučni spisak meteoroloških stanica	I
A) Dnevna osmatranja	1
B) Mesečni i godišnji pregled	99

TABLE DES MATIERES

	Pages
Notice explicative	
Liste alphabétique des stations météorologiques	I
A) Observations journalières	1
B) Revue mensuelle et annuelle	99

O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljuju se podaci 8 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG vremenska razlika u odnosu na Grinič, H_s = nadmorska visina podnožja termometarskog zaklona, H_b = nadmorska visina rezervoara barometra, h_t = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema međunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na 0°C; T = temperatura u °C; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insolacija = trajanje osunčavanja u satima; R = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan međunarodnim simbolima.

U rubrici "razvoj vremena" su potrebne ove skraćenice:

n = u toku noći; a = pre podne; p = posle podne; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računane su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P, e, U, N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su očitavani i uređivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake M_{ax} i M_{in} ; za rubrike broj dana sa $\bullet$ ili $\circ$, $\times$ ili $\triangle$, i $\star$ prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Azbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1973. godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Greenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, H_s = altitude du pied de l'abri météorologique, H_b = altitude de la ouvette du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à 0°C); T = température en °C; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Razvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = pendant la nuit; a = avant midi; p = après midi; i = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4},$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faits à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications M_{ax} et M_{in} ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) • ou •, ✕ ou ✕, et ✕ sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1973; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

STANICA	Broj stanice	Nadomska visina H, m	Geografska širina φ'N	Geografska dužina λ' E	Red stanice	Vrednosti pritiska	Temperatura vazduha	Vlaga vazduha	Vetar	Oblaknost	Insolacija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
SOCIJALISTIČKA REPUBLIKA SLOVENIJA													
Ajdovščina	29	110	45°53'	13°54'	ob	X	X	X	X	X	X	X	X
Babno Polje	35	756	45 39	14 33	ob		X	X	X	X		X	X
Bovec	1	425	46 20	13 33	ob		X	X	X	X	X	X	X
Brnik-letalište	11	362	46 13	14 29	gl	X	X	X	X	X	X	X	X
Celje-Levec	18	244	45 15	15 14	ob		X	X	X	X	X	X	X
Črnomelj	38	156	45 34	15 12	ob		X	X	X	X		X	X
Dom na Kozni	5	1520	46 17	13 46	ob		X		X	X		X	X
Golnik	10	500	46 20	14 20	ob		X	X	X	X	X	X	X
Gornji Lenart	39	150	45 56	15 34	ob		X	X	X	X	X	X	X
Ilirska Bistrica	31	414	45 34	14 15	ob		X	X	X	X		X	X
Javorje nad Poljanami	9	695	46 10	14 11	ob		X	X	X	X		X	X
Jeruzalem	23	345	46 28	16 12	ob		X	X	X	X	X	X	X
Jezerško	12	879	46 24	14 30	ob		X	X	X	X		X	X
Klenik pri Vačah	14	550	46 07	14 51	ob		X	X	X	X		X	X
Kočevje	36	461	45 38	14 52	ob		X	X	X	X		X	X
Koper-Semedela	27	33	45 33	13 43	gl	X	X	X	X	X	X	X	X
Kredarica	6	2514	46 23	13 51	gl	X	X	X	X	X	X	X	X
Kubed	28	262	45 31	13 52	ob		X		X	X		X	X
Ljubljana-Bežigrad	13	299	46 04	14 31	gl	X	X	X	X	X	X	X	X
Maribor	20	275	46 32	15 39	gl	X	X	X	X	X	X	X	X
Mašun	32	1017	45 38	14 22	ob		X		X	X		X	X
Murska Sobota	22	184	46 38	16 11	gl	X	X	X	X	X	X	X	X
Navelo pri Temnici	26	350	45 51	13 40	ob		X	X	X	X	X	X	X
Nova Gorica	25	113	45 57	13 39	gl	X	X	X	X	X	X	X	X
Nova Vas na Blokah	34	722	45 46	14 31	ob		X	X	X	X		X	X
Novo Mesto-Gotna Vas	37	220	45 48	15 11	gl	X	X	X	X	X	X	X	X
Postojna-Zalog	30	533	45 46	14 12	gl		X	X	X	X	X	X	X
Pragersko	21	251	46 24	15 39	ob		X	X	X	X		X	X
Radeče	16	230	46 04	15 11	ob		X	X	X	X		X	X
Radlje ob Dravi	17	365	46 37	15 13	ob		X	X	X	X		X	X
Radovljica	8	495	46 21	14 11	ob		X	X	X	X		X	X
Rakitna	33	787	45 53	14 26	ob		X		X	X		X	X
Rateče-Planica	3	864	46 30	13 43	gl	X	X	X	X	X	X	X	X
Sela pri Planini nad Sevnico	19	550	46 06	15 24	ob		X	X	X	X		X	X
Šmartno pri Slovenjgradcu	15	452	46 29	15 07	gl		X	X	X	X	X	X	X
Tolmin	4	180	46 11	13 44	ob		X	X	X	X		X	X
Vedrijan	2	258	46 01	13 33	ob		X	X	X	X	X	X	X
Veliki Dolenci	24	308	46 51	16 17	ob		X	X	X	X		X	X
Vojsko	7	1070	46 01	13 55	ob		X		X	X		X	X
SOCIJALISTIČKA REPUBLIKA HRVATSKA													
Bjelovar	63	141	45°54'	16°51'	ob	X	X	X	X	X		X	X
Božjakovina	60	110	45 49	16 18	ob		X	X	X	X		X	X
Brestača-Novska	64	152	45 22	16 58	ob		X	X	X	X		X	X
Brestovac-Belje	72	91	45 42	18 44	ob	X	X	X	X	X	X	X	X

S T A N I C A	Broj stanice	Nadmořna visina H, m	Geografska širina y' N	Geografska dužina x' E Gr.	Red stanice	Važujući pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Cres	76	10	44° 58'	14° 24'	ob		X	X	X	X		X	X
Crikvenica	49	2	45 10	14 42	ob		X	X	X	X		X	X
Čazma	62	144	45 45	16 38	ob		X	X	X	X		X	X
Daruvar	66	161	45 36	17 14	gl	X	X	X	X	X	X	X	X
Donji Meljani	67	120	45 44	17 38	ob		X	X	X	X		X	X
Donji Miholjac	70	97	45 46	18 10	ob		X	X	X	X		X	X
Dubrovnik	100	49	42 39	18 06	ob		X	X	X	X		X	X
Djakovo	71	98	45 17	18 25	ob		X	X	X	X		X	X
Gospić	84	564	44 33	15 22	gl	X	X	X	X	X	X	X	X
Gračac	85	560	44 18	15 51	ob		X	X	X	X		X	X
Hvar	90	20	43 10	16 27	gl	X	X	X	X	X	X	X	X
Ilok	74	133	45 14	19 23	ob		X	X	X	X		X	X
Karlovac	53	112	45 30	15 33	ob	X	X	X	X	X	X	X	X
Knin	86	234	44 02	16 12	ob	X	X	X	X	X	X	X	X
Komiža	88	6	43 03	16 05	ob		X	X	X	X		X	X
Koprivnica	43	141	46 11	16 49	ob		X	X	X	X		X	X
Korčula	97	15	42 58	17 09	ob		X	X	X	X		X	X
Kostel	40	270	46 11	15 45	ob		X	X	X	X		X	X
Križevci	42	155	46 02	16 33	ob	X	X	X	X	X	X	X	X
Lastovo	96	186	42 46	16 54	gl	X	X	X	X	X	X	X	X
Ličko Lešće	83	463	44 48	15 19	ob		X	X	X	X		X	X
Lipik	65	154	45 25	17 10	ob		X	X	X	X		X	X
Makarska	92	2	43 18	17 01	ob		X	X	X	X		X	X
Mali Lošinj	77	53	44 32	14 28	gl	X	X	X	X	X	X	X	X
Ogulin	52	328	45 16	15 14	gl	X	X	X	X	X	X	X	X
Opuzen	93	2	43 01	17 34	ob		X	X	X	X		X	X
Orebić	98	6	42 58	17 10	ob		X	X	X	X		X	X
Osijek	73	89	45 32	18 44	gl	X	X	X	X	X	X	X	X
Pag	81	3	44 27	15 04	ob		X	X	X	X	X	X	X
Palagruž	94	98	42 24	16 16	ob	X	X	X	X	X	X	X	X
Parg	48	863	45 36	14 38	ob	X	X	X	X	X	X	X	X
Pazin	46	291	45 14	13 56	ob	X	X	X	X	X		X	X
Preč	44	15	45 14	13 36	ob		X	X	X	X		X	X
Pula	75	30	44 52	13 51	ob		X	X	X	X	X	X	X
Puntijarka	55	988	45 55	15 58	gl	X	X	X	X	X	X	X	X
Rab	78	24	44 45	14 46	ob	X	X	X	X	X	X	X	X
Rijeka	47	104	45 20	14 27	ob	X	X	X	X	X	X	X	X
Rovinj	45	5	45 05	13 39	ob		X	X	X	X	X	X	X
Senj	79	26	44 59	14 54	gl	X	X	X	X	X	X	X	X
Sinj	91	308	43 43	16 40	ob		X	X	X	X	X	X	X
Sisak	61	98	45 30	16 22	ob	X	X	X	X	X	X	X	X
Skrad	51	668	45 25	14 55	ob		X	X	X	X		X	X
Sl. Požega	68	152	45 20	17 41	ob		X	X	X	X		X	X
Sl. Brod	69	88	45 10	18 00	gl	X	X	X	X	X	X	X	X
Slunj	54	258	45 07	15 35	ob		X	X	X	X		X	X

S T A N I C A	Broj stanice	Nadomska visina H _m	Geografska širina	Geografska dužina	Med stanice	Vasodni pritisak	Temperatura vasodba	Vlaktost vasodba	Vetar	Oblaknost	Insolacija	Padarine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Split-Marjan	89	122	43°31'	16°26'	gl	X	X	X	X	X	X	X	X
Ston	99	2	42 50	17 42	ob		X	X	X	X		X	X
Stubička Gora	56	620	45 56	15 59	ob		X	X	X	X		X	X
Šibenik	87	77	43 44	15 55	gl	X	X	X	X	X	X	X	X
Topusko	58	129	45 18	15 59	ob		X	X	X	X		X	X
Varaždin	41	169	46 18	16 21	ob	X	X	X	X	X	X	X	X
Vela Luka	95	30	42 58	16 43	ob		X	X	X	X		X	X
Zadar	82	5	44 08	15 13	ob	X	X	X	X	X	X	X	X
Zagreb-Grič	57	157	45 49	15 59	gl	X	X	X	X	X	X	X	X
Zagreb-Maksimir	59	123	45 49	16 02	gl	X	X	X	X	X	X	X	X
Zalesina	50	750	45 23	14 53	ob		X	X	X	X		X	X
Zavižan	80	1594	44 49	14 59	gl	X	X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A B O S N A I H E R C E G O V I N A													
Banja Luka	111	153	44°47'	17°13'	gl	X	X	X	X	X	X	X	X
Berkovići	139	537	43 06	18 11	ob		X	X	X	X		X	X
Bihać	103	246	44 49	15 53	gl	X	X	X	X	X	X	X	X
Bijeljina-Novo Selo	127	90	44 47	19 16	ob		X	X	X	X	X	X	X
Bileća	149	491	42 53	18 27	ob		X	X	X	X		X	X
Bjelašnica	140	2067	43 43	18 16	gl	X	X	X	X	X	X	X	X
Bos. Krupa	104	176	44 53	16 10	ob		X	X	X	X		X	X
Bos. Novi	101	119	45 03	16 23	ob		X	X		X		X	X
Brčko	125	96	44 53	18 50	ob		X	X	X	X		X	X
Bugojno	115	562	44 04	17 28	gl	X	X	X	X	X	X	X	X
Čapljina-Klepci	133	5	43 05	17 43	ob		X	X	X	X		X	X
Čemerno	145	1305	43 14	18 36	gl	X	X	X	X	X	X	X	X
Derventa	102	105	45 00	17 55	ob		X	X	X	X		X	X
Doboј	120	146	44 44	18 06	ob		X	X	X	X	X	X	X
Domanovići	135	146	43 09	17 47	ob		X	X	X	X		X	X
Drinić	106	730	44 31	16 28	ob		X	X	X	X		X	X
Drvar	105	485	44 23	16 24	gl	X	X	X	X	X	X	X	X
Gacko	144	960	43 10	18 33	ob		X	X	X	X		X	X
Glamoč	110	1031	44 03	16 52	ob		X	X	X	X		X	X
Goražde	147	345	43 40	18 59	ob		X	X	X	X		X	X
Ivan Sedlo	138	970	43 46	18 02	ob		X	X	X	X	X	X	X
Jablanica	134	192	43 40	17 46	ob		X	X	X	X		X	X
Jajce	112	430	44 21	17 16	gl		X	X	X	X	X	X	X
Kalinovik	143	1073	43 31	18 27	ob	X	X	X	X	X		X	X
Kotor Varoš	114	266	44 38	17 23	ob		X	X		X		X	X
Kupres	113	1190	44 00	17 17	ob		X	X	X	X		X	X
Lastva	150	295	42 43	18 29	ob		X	X	X	X		X	X
Lidštica	131	320	43 23	17 36	ob		X	X	X	X		X	X
Livno	129	724	43 50	17 01	gl	X	X	X	X	X	X	X	X
Ljubinje	148	413	42 58	18 06	ob		X	X	X	X		X	X
Maoča	123	335	44 19	18 26	ob		X	X	X	X		X	X

A Z B U Č N I S P I S A K S T A N I C A
PO NARODNIM REPUBLIKAMA

IV

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadmořna visina H ₂ m	Geografska širina φ° N	Geografska dužina λ° E Gr.	Red. stanice	Važujući pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblatnost	Insolacija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Mlinišće	109	1130	44°16'	16°52'	ob		X	X	X	X		X	X
Modriča	121	115	44 59	18 18	ob		X	X	X	X		X	X
Mostar	136	99	43 21	17 48	gl	X	X	X	X	X	X	X	X
Ponikve	122	970	44 11	18 22	ob		X	X	X	X		X	X
Potoci-Željuša	137	96	43 24	17 53	ob		X	X	X	X		X	X
Prijedor	108	135	44 59	16 45	ob		X	X	X	X		X	X
Prnjavor	117	150	44 52	17 42	ob		X	X	X	X		X	X
Prozor	132	800	43 50	17 38	ob		X	X	X	X		X	X
Rakitno	130	915	43 34	17 27	ob		X	X	X	X		X	X
Sanski Most	107	158	44 46	16 42	gl		X	X	X	X	X	X	X
Sarajevo-aerodrom	141	503	43 50	18 20	gl	X	X	X	X	X	X	X	X
Sarajevo	142	630	43 52	18 26	gl	X	X	X	X	X	X	X	X
Sokolac	146	872	43 57	18 49	ob		X	X	X	X	X	X	X
Srebrenica	128	550	44 07	19 19	ob		X	X	X	X		X	X
Teslić	118	225	44 36	17 54	ob		X	X	X	X		X	X
Travnik	116	581	44 14	17 40	ob		X	X	X	X		X	X
Tuzla	124	305	44 33	18 42	gl	X	X	X	X	X	X	X	X
Vlasenica	126	680	44 12	18 57	ob		X	X	X	X		X	X
Zenica	119	344	44 13	17 54	gl	X	X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A S R B I J A													
Aleksandrovac	201	360	43°27'	21°04'	ob		X	X	X	X		X	X
Babušnica	213	495	43 04	22 26	ob		X	X	X	X		X	X
Bačka Topola	155	100	45 49	19 39	ob		X	X	X	X		X	X
Bački Petrovac	154	85	45 22	19 34	ob		X	X	X	X	X	X	X
Bečej	160	78	45 38	20 02	ob		X	X	X	X	X	X	X
Bela Crkva	182	90	44 54	21 25	ob		X	X	X	X		X	X
Bele Vode-Golija	196	1500	43 25	20 17	ob		X	X	X	X	X	X	X
Beograd	172	132	44 48	20 28	gl	X	X	X	X	X	X	X	X
Bor	187	380	44 05	22 06	ob		X	X	X	X		X	X
Bosiljgrad	234	830	42 30	22 28	ob		X	X	X	X		X	X
Bujanovac	227	400	42 27	21 47	ob		X	X	X	X		X	X
Bukovička Banja	175	265	44 18	20 33	ob		X	X	X	X		X	X
Čačak	197	250	43 53	20 19	ob		X	X	X	X		X	X
Čuprija	206	123	43 56	21 23	gl	X	X	X	X	X	X	X	X
Debeli Lug	186	290	44 22	21 55	ob		X	X	X	X		X	X
Dimitrovgrad	216	446	43 01	22 45	gl	X	X	X	X	X	X	X	X
Dragaš	221	1060	42 04	20 39	ob		X	X	X	X		X	X
Flamunda	180	160	44 56	21 05	ob		X	X	X	X	X	X	X
Gladnoš	159	185	45 08	20 00	ob		X	X	X	X		X	X
Gornji Milanovac	173	330	44 02	20 29	ob		X					X	X
Istok	219	465	42 47	20 30	ob		X			X		X	X
Ivanjica	195	465	43 35	20 14	ob		X	X	X	X		X	X
Jaša Tomić	164	80	45 27	20 51	ob		X	X	X	X		X	X
Kikinda	163	81	45 51	20 28	gl		X	X	X	X	X	X	X

AKBUCNI SPISAK STANICA
 PO NARODNIM REPUBLIKAMA

Izak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

V

STANICA	Broj stanice	Nadmořna visina H, m	Geografska širina φ N	Geografska dužina λ E Gr.	Red stanice	Važujući pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Klina	220	385	42° 38'	20° 34'	ob		X			X		X	X
Knjaževac	211	280	43 34	22 16	ob		X			X		X	X
Kos. Mitrovica	223	510	42 53	20 52	ob		X	X	X	X		X	X
Kragujevac	178	190	44 02	20 56	ob		X	X	X	X	X	X	X
Kraljevo	199	219	43 44	20 41	gl	X	X	X	X	X	X	X	X
Kruševac	205	166	43 34	21 21	gl		X	X	X	X	X	X	X
Kukavica	229	1250	42 45	21 59	ob		X	X	X	X		X	X
Kuršumlija	204	380	43 08	21 16	gl		X	X	X	X	X	X	X
Leskovac	210	224	43 01	21 56	gl	X	X	X	X	X		X	X
Loznica	166	121	44 33	19 14	gl	X	X	X	X	X	X	X	X
Ljubovija	167	170	44 11	19 23	ob		X	X	X	X		X	X
Mitrovac - Tara	190	1080	43 55	19 26	ob		X	X	X	X	X	X	X
Negotin	189	42	44 14	22 33	gl	X	X	X	X	X	X	X	X
Niš	209	202	43 20	21 54	gl	X	X	X	X	X	X	X	X
Novi Pazar	198	545	43 08	20 31	ob		X	X	X	X		X	X
Novi Sad-Petrovaradin	158	132	45 15	19 52	gl	X	X	X	X	X	X	X	X
Novi Sad-Rimski Šančevi	157	84	45 20	19 51	ob	X	X	X	X	X	X	X	X
Palić	151	102	46 06	19 46	gl	X	X	X	X	X	X	X	X
Pančevo	176	80	44 53	20 40	ob		X	X	X	X		X	X
Peć	217	498	42 40	20 18	gl	X	X	X	X	X	X	X	X
Petrovac	183	120	44 23	21 25	ob		X	X	X	X		X	X
Pirot	214	370	43 09	22 36	ob		X	X	X	X		X	X
Predejane	231	318	42 50	22 08	ob		X	X	X	X		X	X
Priština	224	573	42 39	21 09	gl	X	X	X	X	X	X	X	X
Prizern	222	402	42 13	20 44	gl		X	X	X	X	X	X	X
Prokuplje	207	265	43 14	21 36	ob		X	X	X	X		X	X
Rekovac	202	230	43 52	21 06	ob		X	X	X	X		X	X
Rudnik	174	700	44 08	20 31	ob		X			X		X	X
Senta	161	80	45 56	20 05	ob		X	X	X	X		X	X
Sijarinska Banja	226	455	42 47	21 36	ob		X			X	X	X	X
Sjenica	193	1015	43 16	20 01	gl	X	X	X	X	X	X	X	X
Skivjane-Djakovica	218	415	42 26	20 21	ob		X		X	X		X	X
Smederevo	177	90	44 39	20 54	ob		X			X		X	X
Smed. Palanka	179	121	44 22	20 57	gl	X	X	X	X	X	X	X	X
Sokobanja	208	300	43 39	21 51	ob		X	X	X			X	X
Sombor	152	88	45 45	19 05	gl		X	X	X	X	X	X	X
Sr. Mitrovica	168	81	44 58	19 38	gl		X	X	X	X		X	X
Surdulica	232	500	42 41	22 11	ob		X			X		X	X
Svetožarevo	203	115	43 59	21 14	ob		X		X	X		X	X
Šabac	169	80	44 46	19 41	ob		X	X	X	X		X	X
Šid	153	105	45 07	19 15	ob		X	X	X	X		X	X
Šušara	181	180	44 56	21 08	ob		X	X	X	X		X	X
Tekija	188	50	44 41	22 25	ob		X	X	X	X		X	X
Titovo Užice	192	440	43 52	19 51	ob		X	X	X	X		X	X
Topli Do	215	700	43 20	22 41	ob		X			X		X	X

A R B U Ţ N I S P I S A K S T A N I C A
PO MACEDONIAN REPUBLICAMA

VI Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadmoćna visina H ₀ m	Geografska širina y' N	Geografska dužina x' E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padarina	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Uroševac	225	580	42°23'	21°10'	ob		X	X	X	X	X	X	X
Už. Požega	194	311	43 51	20 02	gl	X	X	X	X	X	X	X	X
Valjevo	171	174	44 17	19 55	gl	X	X	X	X	X	X	X	X
Veliko Gradište	184	79	44 46	21 31	gl	X	X	X	X	X		X	X
Vladimirci	170	120	44 37	19 47	ob		X	X	X			X	X
Vlasina	233	1190	42 44	22 21	ob		X	X	X	X	X	X	X
Vlasotince	230	270	42 58	22 08	ob		X			X		X	X
Vranje	228	458	42 33	21 55	gl	X	X	X	X	X	X	X	X
Vrbas	156	87	45 34	19 39	ob		X	X	X	X	X	X	X
Vrnjačka Banja	200	235	43 37	20 54	ob		X	X	X	X	X	X	X
Vršac	165	84	45 09	21 19	gl	X	X	X	X	X	X	X	X
Zaječar	212	137	43 53	22 18	ob		X	X	X	X	X	X	X
Zlatibor	191	1029	43 44	19 43	gl	X	X	X	X	X	X	X	X
Zrenjanin	162	80	45 24	20 21	gl		X	X	X	X	X	X	X
Žagubica	185	314	44 12	21 47	ob		X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A C R N A G O R A													
Bar	246	1	42°06'	19°06'	gl	X	X	X	X	X	X	X	X
Bijelo Polje	238	560	43 02	19 45	ob		X	X	X	X	X	X	X
Budva	242	2	42 17	18 51	ob	X	X	X	X	X	X	X	X
Cetinje	243	655	42 24	18 56	ob		X	X	X	X		X	X
Grahovo	240	710	42 39	18 41	ob		X		X	X		X	X
Hercegnovi - Igalo	239	40	42 28	18 30	gl	X	X	X	X	X	X	X	X
Ivangrad	249	670	42 50	19 52	ob	X	X	X	X	X		X	X
Kolašin	248	943	42 50	19 32	gl	X	X	X	X	X	X	X	X
Krstac	235	950	43 00	18 44	ob		X		X	X		X	X
Nikšić	244	647	42 46	18 57	gl	X	X	X	X	X	X	X	X
Pljevlja	237	784	43 21	19 21	gl	X	X	X	X	X	X	X	X
Titograd	247	49	42 26	19 17	ob	X	X	X	X	X	X	X	X
Tivat	241	6	42 26	18 42	ob	X	X	X	X	X		X	X
Ulcinj	250	97	41 55	19 13	gl	X	X	X	X	X	X	X	X
Virpazar	245	14	42 14	19 05	ob		X	X	X	X		X	X
Žabljak	236	1450	43 09	19 08	gl	X	X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A M A K E D O N I J A													
Berovo	282	824	41°43'	22°51'	gl	X	X	X	X	X	X	X	X
Bitola	266	586	41 03	21 22	gl	X	X	X	X	X	X	X	X
Debar	256	675	41 31	20 32	ob		X	X	X	X		X	X
Delčevo	281	630	41 58	22 46	ob		X	X	X	X		X	X
Demir Kapija	274	125	41 25	22 15	gl	X	X	X	X	X		X	X
Erdželija	271	253	41 50	22 02	ob		X	X	X	X		X	X
Gevgelija	277	59	41 09	22 30	ob		X	X	X	X		X	X
Gostivar	261	525	41 48	20 55	ob		X	X	X	X		X	X
Kavadarci	272	265	41 26	22 02	ob		X	X	X	X		X	X
Kičevo	262	620	41 31	20 58	ob		X	X	X	X		X	X

A Z B U Č N I S P I S A K S T A N I C A
PO MAKEDONSKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

VII

S T A N I C A	Broj stanice	Nadmořna visina H, m	Geografska širina φ° N	Geografska dužina λ° E Gr.	Red stanice	Važujući pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Kočani	275	345	41°55'	22°25'	ob		X	X	X	X		X	X
Kratovo	254	640	42 05	22 09	ob		X	X	X	X		X	X
Kriva Palanka	255	691	42 12	22 20	gl	X	X	X	X	X	X	X	X
Kruševo	265	1230	41 22	21 15	ob		X	X	X	X		X	X
Kumanovo	253	338	42 08	21 43	ob		X	X	X	X		X	X
Lazaropole	258	1332	41 32	20 42	gl	X	X	X	X	X	X	X	X
Makedonski Brod	264	545	41 31	21 13	ob		X	X	X	X		X	X
Mavrovi Anovi	259	1240	41 42	20 45	ob		X	X	X	X	X	X	X
Novi Dojran	280	180	41 13	22 43	ob		X	X	X	X		X	X
Ohrid	260	760	41 07	20 48	gl	X	X	X	X	X	X	X	X
Popova Šapka	251	1250	42 01	20 53	ob		X	X	X	X		X	X
Prilep	269	673	41 20	21 34	gl	X	X	X	X	X	X	X	X
Radoviš	276	380	41 38	22 27	ob		X	X	X	X		X	X
Resen	263	881	41 05	21 01	ob		X	X	X	X		X	X
Skopje	267	232	41 57	21 38	gl	X	X	X	X	X	X	X	X
Struga	257	695	41 11	20 41	ob		X	X	X	X		X	X
Strumica	279	224	41 26	22 39	ob		X	X	X	X		X	X
Štip	273	326	41 45	22 11	gl	X	X	X	X	X	X	X	X
Tetovo	252	462	42 00	20 58	ob		X	X	X	X		X	X
Titov Veles	270	175	41 43	21 46	ob		X	X	X	X		X	X
Trubarevo	268	233	41 59	21 31	ob		X	X	X	X		X	X
Valandovo	278	100	41 19	22 34	ob		X	X	X	X		X	X

A) Dnevna osmatranja

$\varphi = 46^{\circ} 04' N$ $\lambda = 14^{\circ} 31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napoin vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vetra D, f (0—12)			
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21	
1	749.9	748.9	749.1	-02.8	-00.9	-01.3	-01.6	-00.8	-02.9	-05.0	02.9	03.0	03.5	80	70	85	78	W	1	-	0
2	747.5	745.0	744.9	-01.4	00.2	00.2	-00.2	00.6	-01.6	-01.9	03.9	03.9	04.0	96	85	86	89	SW	1	NE	1
3	743.8	742.1	743.4	-00.6	03.1	01.0	01.1	03.6	-00.8	-02.5	04.1	04.1	04.6	94	71	93	86	-	0	N	1
4	744.5	744.9	746.2	00.0	01.5	00.8	00.8	01.6	-00.2	-01.0	04.3	04.3	04.4	93	85	91	90	E	1	NE	1
5	748.0	748.2	749.5	00.8	02.2	01.2	01.4	02.6	00.3	-00.5	04.2	04.3	04.5	86	81	90	86	E	1	NW	1
6	750.2	750.3	750.6	00.2	01.9	00.7	00.9	02.0	-00.6	-04.6	04.0	03.9	03.7	86	74	78	79	-	0	-	0
7	749.0	748.0	748.9	-03.8	03.4	-01.5	-00.8	04.1	-04.3	-09.0	03.1	03.8	03.8	94	65	92	84	NE	1	-	0
8	748.6	746.9	746.5	-01.4	01.0	01.0	00.4	01.4	-02.1	-06.5	03.7	04.3	04.3	91	86	86	88	-	0	NW	1
9	745.4	745.0	745.7	-00.3	00.1	-00.6	-00.4	01.2	-00.6	-00.7	04.1	04.0	03.7	91	88	85	88	SE	1	SE	2
10	745.6	745.3	744.7	-01.2	-00.6	-00.6	-00.8	-00.1	-01.4	-02.0	03.2	03.7	03.3	76	84	75	78	SE	2	N	2
11	742.7	743.8	745.8	-01.7	00.7	-02.2	-01.4	01.6	-02.3	-02.5	03.2	03.3	03.4	81	69	88	79	SE	1	NE	1
12	745.8	745.7	746.6	-03.7	-00.3	00.1	-01.0	00.6	-04.6	-09.1	03.0	03.5	03.9	90	79	84	84	NE	1	NE	1
13	746.7	746.4	747.6	-01.0	02.5	-02.7	-01.0	02.9	-02.8	-06.5	03.3	03.3	03.2	78	61	88	76	NE	1	NE	1
14	746.6	743.4	741.1	-06.4	-01.8	-02.8	-03.4	-01.3	-07.7	-11.4	02.6	03.4	03.5	98	87	96	94	NE	1	S	1
15	736.9	734.3	732.6	02.2	04.6	05.1	04.2	05.6	-02.8	-02.8	04.1	04.4	05.3	76	69	80	75	SW	3	WSW	3
16	729.8	728.9	730.9	02.6	00.6	-00.4	00.6	05.9	-00.4	01.0	05.3	04.6	04.3	95	97	96	96	NE	1	SE	1
17	733.1	733.4	734.3	-01.6	-01.6	-01.6	-01.6	00.2	-02.0	-02.0	03.3	03.2	03.7	83	80	93	85	NE	1	NE	1
18	734.1	733.6	734.4	-00.4	01.6	00.6	00.7	02.3	-01.6	-01.6	04.3	04.8	04.6	96	93	95	95	-	0	-	0
19	734.3	734.5	734.2	00.8	01.0	00.4	00.6	01.5	00.3	00.0	04.8	04.8	04.6	98	97	98	98	SW	1	-	0
20	732.9	732.7	734.6	00.4	02.2	01.2	01.2	02.6	00.0	00.0	04.6	04.6	04.7	97	86	93	92	-	0	-	0
21	737.1	737.0	736.9	00.8	01.0	01.0	01.0	01.8	00.4	-00.2	04.8	04.9	04.8	98	100	97	98	-	0	-	0
22	737.8	738.5	741.9	01.0	02.7	01.5	01.7	03.0	00.5	-00.4	04.7	05.1	04.7	95	92	92	93	SE	1	-	0
23	744.2	744.9	746.2	00.6	01.4	00.4	00.7	01.7	00.3	-00.2	04.5	04.7	04.5	95	93	95	94	-	0	-	0
24	745.4	744.9	746.8	00.8	02.1	00.7	01.1	02.6	00.4	-00.2	04.4	04.1	03.9	91	77	81	83	SE	1	SE	1
25	747.8	747.8	748.3	01.0	02.6	-00.6	00.6	02.7	-00.8	-00.5	03.4	03.7	03.0	70	67	67	68	NE	2	NE	2
26	745.0	742.2	740.9	-05.8	-01.0	-03.6	-03.5	-00.4	-06.6	-09.9	02.5	02.9	02.4	88	70	71	76	NW	1	S	1
27	735.9	730.7	728.3	-05.4	-01.6	-02.4	-03.0	-01.1	-05.6	-05.8	02.3	02.8	02.9	80	71	77	76	SE	2	S	1
28	727.9	729.1	732.8	-06.0	04.9	-00.6	-00.6	06.1	-06.3	-10.5	02.6	03.5	03.7	93	53	84	77	N	1	SSE	1
29	736.3	737.8	736.9	-05.2	06.3	-00.7	-00.1	06.4	-05.9	-09.2	02.8	03.2	03.4	93	45	78	72	NE	1	S	1
30	736.2	735.0	735.5	-05.6	00.8	-00.8	-01.6	01.6	-05.6	-09.0	02.7	03.7	03.6	93	76	83	84	E	1	NE	1
31	735.9	734.5	734.8	-03.9	03.7	01.4	00.6	04.2	-04.6	-08.0	03.2	04.0	04.7	96	68	93	86	NE	1	-	0
MES.																					
VRED.	741.4	740.8	741.3	-01.5	01.4	-00.2	-00.1	02.2	-02.3	-04.0	03.7	03.9	04.0	89	78	87	85	0.9	0.8	1.0	

1973 FEBRUAR

LJUBLJANA BEŽIGRAD

1	733.0	734.1	737.0	00.4	01.9	01.4	01.3	02.3	00.2	00.0	04.6	04.8	04.7	57	92	93	94	NW	1	SW 1	SE 1
2	737.9	740.1	742.8	00.8	01.0	00.6	00.8	01.7	00.5	-00.1	04.7	04.8	04.5	97	97	93	96	SW	1	SE 2	E 1
3	745.1	746.3	747.6	00.6	04.4	01.9	02.2	04.5	00.4	-00.5	04.5	04.8	04.8	95	77	92	88	SE	1	-	0 N 1
4	747.3	747.1	748.1	-01.4	-00.7	-01.0	-01.0	02.4	-01.9	-04.6	04.1	04.2	04.2	100	98	100	99	-	0	N	1 N 1
5	747.9	745.8	745.0	-00.5	07.0	-00.9	01.2	07.2	-01.8	-01.6	04.3	04.8	04.0	98	64	95	86	-	0	-	0 - 0
6	741.4	740.2	741.6	-02.3	-00.4	-01.6	-01.6	-00.4	-02.4	-07.0	03.7	04.4	03.9	98	98	98	98	N	1	NE 1	NE 1
7	739.1	737.1	736.9	-02.8	04.6	01.2	01.0	06.6	-03.0	-02.5	03.6	04.6	04.7	100	73	95	89	-	0	-	0 - 0
8	736.4	735.2	736.6	-03.8	11.3	06.3	05.0	11.4	-03.8	-07.7	03.3	05.0	05.7	98	50	80	76	-	0	SW 2	S 1
9	735.0	733.7	732.6	06.7	08.1	07.9	07.6	08.2	03.0	00.5	06.2	06.0	06.0	84	74	75	78	SW	1	NW 2	W 2
10	729.3	727.1	728.3	06.6	06.0	00.8	03.6	08.2	00.6	01.5	05.9	06.8	04.7	80	97	97	91	SW	2	NW 1	SW 1
11	728.9	731.6	735.2	00.5	04.0	00.3	01.3	06.3	00.2	-00.2	04.6	04.8	04.4	97	78	93	89	-	0	S	1 SE 1
12	736.9	734.5	731.1	-02.0	01.7	-01.4	-00.8	03.1	-02.6	-06.5	03.7	03.8	03.8	96	74	92	87	SW	1	-	0 W 1
13	724.1	721.7	720.6	-03.6	01.7	00.6	-00.2	02.2	-04.3	-08.5	03.1	04.3	04.5	92	84	95	90	W	1	NW 1	NE 1
14	718.6	718.0	718.5	02.1	00.6	00.5	00.9	02.6	00.4	-01.9	05.2	04.5	04.6	97	95	97	96	NW	1	S	1 - 0
15	720.1	720.7	722.1	-00.4	02.8	-00.6	00.3	04.4	-00.6	-00.5	04.3	04.3	04.2	96	77	96	90	-	0	NE 1	- 0
16	723.4	723.6	725.4	-01.0	05.4	00.2	01.2	06.7	-01.2	-01.1	03.9	03.6	04.0	93	53	87	78	NW	3	-	0 N 1
17	728.4	728.4	729.9	-02.0	05.4	00.8	01.2	05.7	-02.4	-05.2	03.8	03.8	03.9	98	57	80	78	-	0	S	1 N 3
18	732.5	733.6	735.5	-04.4	04.0	-01.2	-00.7	05.0	-04.8	-11.3	02.9	02.9	03.0	91	47	71	70	N	1	-	0 NE 1
19	737.7	736.8	737.2	-05.8	05.7	-01.4	-00.7	06.2	-06.6	-11.6	02.5	02.7	03.1	88	40	76	68	N	1	-	0 - 0
20	740.2	739.7	740.7	-04.9	06.2	00.0	00.3	06.8	-05.2	-10.3	02.8	03.2	03.6	91	46	79	72	NW	1	SW 1	SE 1
21	739.2	736.6	734.7	-04.6	03.6	02.6	01.0	04.9	-04.8	-09.5	02.9	03.7	04.1	93	62	74	76	N	1	N	1 NE 1
22	732.3	731.1	730.6	-00.2	09.4	03.4	04.0	10.1	-00.6	-03.3	04.1	04.3	04.4	91	49	76	72	SE	1	SE 1	NE 1
23	725.8	728.4	728.8	00.7	05.6	00.8	02.0	06.0	00.7	-03.0	04.5	04.8	04.3	93	70	88	84	N	1	SE 3	S 3
24	724.4	721.2	723.2	-01.4	04.0	01.7	01.5	04.8	-01.6	-06.5	04.0	04.3	03.4	98	71	65	78	SE	1	NW 1	NW 1
25	724.6	724.6	726.5	-04.5	05.8	01.1	00.9	07.0	-05.4	-09.5	02.5	01.7	01.7	79	25	35	46	N	1	SW 1	NW 2
26	727.8	727.8	730.3	-04.2	04.8	-01.4	-00.6	05.2	-04.8	-10.2	02.3	02.3	02.4	73	35	59	56	S	1	W	2 S 2
27	732.1	733.2	737.2	-06.6	04.2	-00.6	-00.9	04.2	-07.0	-11.6	02.2	01.6	01.3	83	25	30	46	S	1	NW 4	N 2
28	741.7	742.7	744.4	-06.8	05.0	-00.4	-00.6	05.0	-07.3	-12.0	01.8	01.4	01.8	68	21	41	43	W	1	N	1 - 0
MES.																					
VRED.	733.4	732.9	733.9	-01.6	04.4	00.6	01.1	05.3	-02.4	-05.2	03.8	04.0	03.9	92	65	80	79	0.8	1.1	1.1	

BR. ST. 13

 $H_s = 299 \text{ m}$ $H_D = 300.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.5 \text{ m}$

Dan	Velikost 0-9	Oblaknost N (0-10)				Inzolacija broj soni	Padavine R mm	Snežni pokrivalo h cm	Razvoj vremena w
		14	7	14	21	Sred Dies	7	7	
1	6	10 ²	10 ²	10 ²	10 ²	00.0	01.0	.	$\square$ n-n, = n-n, ω 4 ³ / ₄ -6 ³ / ₄ , Δ 15 ¹ / ₂ -15 ¹ / ₂ , ω 15 ¹ / ₂ -16 ³ / ₄ , ω 16 ³ / ₄ -17, 20 ¹ / ₂ -n
2	5	10 ²	10 ²	10 ²	10 ²	00.0	01.1	.	$\square$ n-n, = n-n, ω 4 ³ / ₄ -6 ³ / ₄ , Δ 15 ¹ / ₂ -15 ¹ / ₂ , ω 15 ¹ / ₂ -16 ³ / ₄ , ω 16 ³ / ₄ -17, 20 ¹ / ₂ -n
3	4	10 ²	05 ¹	10 ²	05.7	00.0	00.0	.	$\square$ n-12, = n-n, ω 4 ³ / ₄ -6 ³ / ₄ , Δ 15 ¹ / ₂ -15 ¹ / ₂ , ω 15 ¹ / ₂ -16 ³ / ₄ , ω 16 ³ / ₄ -17, 20 ¹ / ₂ -n
4	5	10 ²	10 ²	10 ²	10 ²	00.0	03.6	02	$\square$ n-n, = n-n, ω 4 ³ / ₄ -6 ³ / ₄ , Δ 15 ¹ / ₂ -15 ¹ / ₂ , ω 15 ¹ / ₂ -16 ³ / ₄ , ω 16 ³ / ₄ -17, 20 ¹ / ₂ -n
5	6	10 ²	05 ¹	10 ²	05.7	00.0	00.0	01	$\square$ n-n, = n-n, ω 4 ³ / ₄ -6 ³ / ₄ , Δ 15 ¹ / ₂ -15 ¹ / ₂ , ω 15 ¹ / ₂ -16 ³ / ₄ , ω 16 ³ / ₄ -17, 20 ¹ / ₂ -n
6	6	10 ²	10 ²	10 ²	10 ²	00.0	.	.	$\square$ n-10, ω n-10, = n-n
7	6	00	01 ⁰	01 ⁰	00.7	04.5	.	.	$\square$ n-10 ³ / ₄ , 18 ³ / ₄ -n, = n-13 ¹ / ₂ , 17 ³ / ₄ -n, ω 13 ¹ / ₂ -14 ³ / ₄ , ω
8	6	10 ²	10 ²	10 ²	10 ²	00.0	.	.	$\square$ n-11 ¹ / ₂ , = n-n
9	6	10 ²	10 ²	10 ²	10 ²	00.0	00.0	.	$\square$ n-n, ω n-12 ² / ₅ , 16 ¹ / ₄ -17 ² / ₅ , 20 ¹ / ₂ -n
10	7	10 ²	10 ²	10 ²	10 ²	00.0	00.0	.	$\square$ n-9 ¹ / ₄ , ω n-8 ³ / ₄ -12 ¹ / ₄ , Δ 12 ¹ / ₄ -12 ² / ₅ , ω 13 ⁵ / ₁₀ -14 ¹ / ₂
11	6	10 ²	02 ¹	05 ¹	07.0	01.6	00.0	.	$\square$ n-15 ¹ / ₂ , 17 ³ / ₄ -n, ω 20 ¹ / ₂ -n, ω
12	5	05 ¹	10 ²	10 ²	05.7	00.0	.	.	$\square$ n-n, ω n-15
13	7	02 ¹	01 ⁰	00	01.0	04.0	.	.	$\square$ n-12 ¹ / ₄ , 18 ¹ / ₄ -n, ω n-10 ¹ / ₄ , 20 ¹ / ₄ -n, ω 12 ¹ / ₄ -18 ¹ / ₄ , ω
14	3	10 ²	00 ⁰	10 ²	06.7	00.0	.	.	$\square$ n-n, ω n-11 ¹ / ₂ , 15 ¹ / ₄ -15 ¹ / ₄ , 17 ¹ / ₄ -14 ¹ / ₂ , ω 2 ¹ / ₄ -11 ¹ / ₂ , ω 15 ¹ / ₄ -n, ω
15	7	10 ²	10 ²	10 ²	10 ²	00.0	.	.	$\square$ n-9 ¹ / ₂ , ω 9 ¹ / ₂ -n
16	4	10 ²	10 ²	10 ²	10 ²	00.0	00.6	.	$\square$ n-n, ω n-4 ³ / ₄ , ω n-12 ¹ / ₄ , ω 12 ¹ / ₄ -12 ¹ / ₂ , ω 12 ¹ / ₂ -n, ω
17	6	10 ²	10 ²	10 ²	10 ²	00.0	13.5	02	$\square$ n-n, ω n-10 ¹ / ₄ -16 ¹ / ₂ , ω n-16 ¹ / ₂ -n, ω
18	4	10 ²	10 ²	10 ²	10 ²	00.0	04.6	03	$\square$ n-16 ¹ / ₄ , ω n-5 ¹ / ₄ , ω n-15 ¹ / ₄ -6 ¹ / ₄ , ω n-6 ¹ / ₄ -10 ¹ / ₄ , ω n-11 ¹ / ₂ , ω n-16 ¹ / ₄ -n, ω
19	2	10 ²	10 ²	10 ²	10 ²	00.0	07.7	04	$\square$ n-4 ³ / ₄ , 18 ¹ / ₄ -n, ω n-11 ¹ / ₂ , ω n-11 ¹ / ₂ -12 ¹ / ₄ , ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -18 ¹ / ₄ -n, ω
20	6	10 ²	10 ²	10 ²	10 ²	00.0	10.6	07	$\square$ n-6 ¹ / ₂ , 9 ¹ / ₄ -n, ω n-11 ¹ / ₂ , ω n-11 ¹ / ₂ -9 ¹ / ₄ , ω n-18 ¹ / ₄ , ω
21	1	10 ²	10 ²	10 ²	10 ²	00.0	00.1	06	$\square$ n-7 ¹ / ₂ , 18 ¹ / ₄ -n, ω n-12 ¹ / ₄ , ω n-12 ¹ / ₄ -18 ¹ / ₄ , ω n-18 ¹ / ₄ -11 ¹ / ₂ , ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -18 ¹ / ₄ -n, ω
22	4	10 ²	10 ²	10 ²	10 ²	00.0	04.2	04	$\square$ n-4 ³ / ₄ , 18 ¹ / ₄ -n, ω n-11 ¹ / ₂ , ω n-11 ¹ / ₂ -12 ¹ / ₄ , ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -18 ¹ / ₄ -n, ω
23	4	10 ²	10 ²	10 ²	10 ²	00.0	02.3	04	$\square$ n-9 ¹ / ₄ -n, ω n-3 ¹ / ₂ , 8 ¹ / ₄ -16 ¹ / ₂ , ω n-3 ¹ / ₂ -8 ¹ / ₄ , 16 ¹ / ₂ -n, ω n-9 ¹ / ₄ , ω n-20 ¹ / ₂ -20 ¹ / ₂ , ω
24	6	10 ²	04 ¹	10 ²	08.0	00.0	05.6	05	$\square$ n-n, ω n-6 ¹ / ₂ , 20 ¹ / ₂ -n, ω n-15 ¹ / ₂ , ω n-15 ¹ / ₂ -20 ¹ / ₂ , ω
25	7	10 ²	09 ¹	05 ¹	06.0	00.0	00.0	04	$\square$ n-7 ¹ / ₂ , ω n-6 ¹ / ₂ -8 ¹ / ₄ , ω n-8 ¹ / ₄ -10 ¹ / ₂ , ω
26	7	04 ¹	05 ¹	10 ²	06.3	02.4	00.0	03	$\square$ n-11 ¹ / ₂ , ω n-11 ¹ / ₂ -16 ¹ / ₂ , ω n-15 ¹ / ₂ -17 ¹ / ₂ , ω
27	6	10 ²	10 ²	10 ²	10 ²	00.0	.	02	$\square$ n-n, ω n-11 ¹ / ₂ -16 ¹ / ₂ , ω n-15 ¹ / ₂ -17 ¹ / ₂ , ω
28	6	10 ²	02 ¹	10 ²	04.3	05.5	.	03	$\square$ n-10 ¹ / ₂ , ω n-12 ¹ / ₄ , 18 ¹ / ₄ -n, ω n-12 ¹ / ₄ -18 ¹ / ₄ , ω
29	6	00	02 ¹	10 ²	01.0	05.1	.	03	$\square$ n-9 ¹ / ₄ , ω n-5 ¹ / ₂ -9 ¹ / ₄ , ω n-5 ¹ / ₂ -6 ¹ / ₂ , ω
30	6	05 ¹	07 ¹	02 ¹	04.7	00.0	.	03	$\square$ n-n, ω n-12 ¹ / ₄ , ω n-12 ¹ / ₄ -18 ¹ / ₄ , ω
31	4	10 ²	09 ²	10 ²	05.7	00.0	.	02	$\square$ n-n, ω n-9 ¹ / ₄ , ω n-9 ¹ / ₄ -5 ¹ / ₂ , ω n-15 ¹ / ₄ , 17 ¹ / ₂ -n, ω n-9 ¹ / ₂ -13 ¹ / ₄ , ω n-15 ¹ / ₄ -17 ¹ / ₂ , ω n-17 ¹ / ₂ -19 ¹ / ₂ , ω n-19 ¹ / ₂ -20 ¹ / ₂ , ω
MES.									
RED.		06.7	07.7	08.4	08.3	22.1	55.7		

1	4	10 ²	10 ²	10 ²	10 ²	00.0	12.7	07	ω n-11 ¹ / ₄ , ω n-13 ¹ / ₂ , ω n-9 ¹ / ₂ -11 ¹ / ₂ , ω n-11 ¹ / ₂ -15 ¹ / ₂ , 17 ¹ / ₄ -19 ¹ / ₄ , ω n-13 ¹ / ₂ -n, ω
2	4	10 ²	10 ²	10 ²	10 ²	00.0	04.8	06	ω n-14 ³ / ₈ , 18 ¹ / ₄ -n, ω n-10 ¹ / ₂ , 14 ¹ / ₄ -n, ω n-10 ¹ / ₂ -14 ¹ / ₄ , ω
3	5	10 ²	06 ¹	10 ²	05.3	00.4	06.2	08	ω n-n, ω n-8 ¹ / ₂ -9 ¹ / ₂ , ω
4	2	10 ²	10 ²	10 ²	10 ²	00.0	00.0	07	ω n-n, ω n-9 ¹ / ₂ , ω
5	5	10 ²	00 ⁰	00 ⁰	03.3	04.0	.	06	ω n-6 ⁵ / ₁₀ , 18 ¹ / ₂ -n, ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -18 ¹ / ₂ , ω
6	2	10 ²	10 ²	10 ²	10 ²	00.0	.	04	ω n-n, ω n-5 ¹ / ₂ -13 ¹ / ₂ , ω
7	4	10 ²	07 ¹	03 ⁰	06.7	03.5	.	04	ω n-11 ¹ / ₂ , ω n-11 ¹ / ₂ -11 ¹ / ₄ , ω n-11 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -n, ω
8	7	05 ¹	06 ¹	10 ²	07.0	03.5	.	02	ω n-7 ¹ / ₂ , ω n-12 ¹ / ₄ , 19 ¹ / ₂ -n, ω n-12 ¹ / ₄ -19 ¹ / ₂ , ω
9	6	10 ²	10 ²	10 ²	10 ²	00.0	.	.	ω n-15 ¹ / ₄
10	7	06 ²	10 ²	10 ²	05.3	00.0	00.5	.	ω n-5 ¹ / ₄ , 14 ³ / ₄ -n, ω n-10 ¹ / ₂ , ω n-10 ¹ / ₂ -20 ¹ / ₄ , 18 ³ / ₄ -20 ¹ / ₄ , ω n-20 ¹ / ₄ -20 ¹ / ₂ , ω n-20 ¹ / ₂ -n, ω n-20 ¹ / ₂ -20 ¹ / ₂ , ω
11	6	10 ²	06 ¹	04 ¹	06.7	02.5	00.7	06	ω n-6 ⁵ / ₁₀ , ω n-n, ω n-12 ¹ / ₄ -9 ¹ / ₂ , ω n-9 ¹ / ₂ -13 ¹ / ₄ , ω n-13 ¹ / ₄ -20 ¹ / ₂ -n, ω
12	5	10 ²	02 ⁰	00	04.0	04.7	.	03	ω n-15 ¹ / ₄ , 18 ¹ / ₄ -n, ω n-10 ¹ / ₂ -10 ¹ / ₂ , ω n-15 ¹ / ₄ -18 ¹ / ₄ , ω
13	6	03	10 ²	10 ²	07.7	00.0	00.0	02	ω n-9 ¹ / ₄ , 12 ¹ / ₄ -n, ω n-11 ¹ / ₂ -12 ¹ / ₄ , ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -16 ¹ / ₂ , ω
14	4	10 ²	10 ²	10 ²	10 ²	00.0	25.6	02	ω n-9 ¹ / ₄ , ω n-15 ¹ / ₄ , 18 ¹ / ₄ -n, ω n-12 ¹ / ₄ -13 ¹ / ₂ , ω n-13 ¹ / ₂ -16 ¹ / ₂ , ω n-16 ¹ / ₂ -19 ¹ / ₂ , ω n-19 ¹ / ₂ -20 ¹ / ₂ , ω
15	6	10 ²	05 ¹	10 ²	05.7	02.5	31.4	05	ω n-9 ¹ / ₄ , 17 ¹ / ₄ -n, ω n-9 ¹ / ₄ -10 ¹ / ₄ , 16 ¹ / ₄ -17 ¹ / ₄ , ω n-16 ¹ / ₄ -16 ¹ / ₄ , ω
16	7	10 ²	03 ⁰	00	04.3	07.6	.	07	ω n-6 ⁵ / ₁₀ , ω n-10 ¹ / ₂ , 18 ¹ / ₂ -n, ω n-14 ¹ / ₂ -16 ¹ / ₂ , ω
17	6	10 ²	10 ²	10 ²	10 ²	00.0	02.5	04	ω n-6 ⁵ / ₁₀ , ω n-15 ¹ / ₂ -15 ¹ / ₂ , ω n-15 ¹ / ₂ -17 ¹ / ₂ , ω n-17 ¹ / ₂ -16 ¹ / ₂ , ω n-16 ¹ / ₂ -20 ¹ / ₂ -n, ω
18	7	01 ²	06 ¹	00	03.0	05.0	00.0	03	ω n-11 ¹ / ₄ , ω n-11 ¹ / ₄ -15 ¹ / ₄ , ω n-15 ¹ / ₄ -17 ¹ / ₄ , ω
19	7	00	00 ⁰	00	00.0	06.7	.	03	ω n-13 ¹ / ₄ , ω n-5 ¹ / ₂ , ω n-11 ¹ / ₂ -17 ¹ / ₄ , ω
20	7	06 ⁰	01 ⁰	00	02.3	06.2	.	03	ω n-13 ¹ / ₄ , ω n-6 ¹ / ₄ , ω n-13 ¹ / ₄ -n, ω
21	7	04 ¹	05 ¹	10 ²	07.7	00.3	.	02	ω n-4 ¹ / ₂ , ω n-12 ¹ / ₄ , ω n-12 ¹ / ₄ -n, ω
22	6	10 ²	05 ⁰	05 ¹	08.0	03.5	.	.	ω n-4 ¹ / ₂ , ω n-16 ¹ / ₂ , 18 ¹ / ₂ -n, ω
23	7	05 ¹	04 ⁰	02 ¹	05.0	01.8	00.2	00	ω n,

$\varphi = 46^{\circ} 04' N$ $\lambda = 14^{\circ} 31' E$ Gr. $\Delta G = + 58 \text{ min.}$

BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vetra D, f (0—12)					
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21			
1	745.2	743.1	742.6	-05.8	07.9	02.0	01.5	10.8	-06.0	-10.8	02.5	03.0	02.3	88	38	44	57	NE	1	W	1	WSW	2
2	741.0	738.9	739.2	-05.1	07.6	01.8	01.5	09.5	-05.4	-10.0	02.8	02.9	03.8	93	37	73	68	N	1	SE	1	NE	1
3	740.6	740.9	742.4	-00.4	12.3	06.2	06.1	12.9	-00.6	-03.6	03.7	02.1	02.7	83	20	38	47	N	1	SW	1	NW	1
4	742.8	743.6	745.6	00.3	10.3	02.9	04.1	11.0	-00.1	-02.0	03.8	03.8	04.4	81	41	78	67	NE	1	NE	2	NE	2
5	745.2	743.4	742.6	00.3	10.6	03.4	04.4	12.5	-00.3	-05.0	04.4	04.7	04.6	93	50	79	74	NE	1	SE	1	SE	1
6	740.3	738.1	738.2	-01.4	11.4	05.4	05.2	14.2	-01.6	-05.9	03.9	04.3	04.9	94	42	72	69	NE	1	NE	1	N	1
7	737.6	737.6	740.5	01.5	08.9	05.6	05.4	10.0	00.5	-02.5	04.6	05.7	05.1	90	67	75	77	E	1	NE	3	NE	3
8	741.0	740.8	741.9	04.6	06.8	03.9	04.8	06.9	03.8	02.4	04.4	03.6	03.4	69	49	56	58	E	4	NE	4	NE	2
9	739.3	738.8	741.1	-02.4	02.8	01.7	01.0	06.4	-03.4	-08.5	03.2	04.6	02.5	86	83	49	73	SW	1	N	3	NE	3
10	740.8	741.0	742.1	00.2	03.9	01.8	01.6	04.1	-00.2	-03.8	02.4	02.7	02.8	51	44	54	50	E	2	E	4	NE	3
11	740.8	738.2	738.2	00.6	04.9	00.8	01.8	05.9	00.3	-01.6	02.4	02.9	03.1	50	44	65	53	NE	3	NE	3	E	1
12	736.9	734.7	735.5	-05.2	06.8	02.2	01.5	07.7	-05.3	-10.1	02.6	03.0	02.9	89	40	53	61	NE	1	SW	1	NE	1
13	735.2	732.8	733.4	01.6	04.9	01.8	02.5	06.7	-00.2	-01.2	03.6	03.5	04.6	71	53	89	71	NE	2	E	3	NE	2
14	732.4	733.2	735.9	00.4	04.2	00.8	01.6	05.5	-00.4	-03.5	03.7	03.5	04.3	79	57	88	75	E	2	E	2	NE	1
15	736.8	737.6	740.1	00.2	04.9	01.7	02.1	05.2	00.0	-01.1	04.3	04.0	03.8	93	61	74	76	E	1	SE	3	E	2
16	740.4	740.4	741.7	-00.6	05.8	02.1	02.4	06.3	-00.2	-03.6	04.0	03.6	04.0	91	52	74	72	NW	1	NE	3	SE	2
17	741.2	739.2	738.0	00.3	09.3	02.6	03.7	09.8	00.2	-02.4	04.4	03.5	04.0	93	40	72	68	NE	1	SE	2	N	1
18	734.6	731.0	731.2	-02.7	10.6	04.4	04.2	12.6	-03.0	-07.1	03.5	03.7	03.5	96	39	56	64	NE	1	SW	1	N	1
19	733.1	734.2	739.0	-01.4	11.2	07.0	06.0	12.9	-01.8	-00.4	03.6	02.6	03.4	89	26	45	53	NE	1	NW	2	NE	1
20	743.6	743.0	743.2	-02.4	11.4	04.6	04.6	11.7	-03.0	-09.6	03.3	02.9	03.6	86	29	56	57	NE	1	S	1	SE	1
21	744.4	742.7	743.6	-02.6	12.6	07.2	06.1	14.0	-03.0	-08.8	03.2	03.7	04.3	86	34	57	59	NE	1	NW	1	SE	1
22	740.2	743.7	743.1	-00.8	13.6	07.7	07.0	14.7	-01.3	-08.6	04.2	04.1	04.5	96	35	57	63	NE	1	SW	1	-	0
23	742.5	740.3	740.4	-01.0	16.6	08.6	08.2	17.0	-01.6	-08.3	04.1	03.9	04.6	96	28	55	60	N	1	S	2	SE	1
24	740.1	737.8	737.6	-00.4	16.9	10.5	09.6	18.0	-01.4	-08.5	04.4	03.6	04.5	98	25	46	56	NE	1	SE	3	S	3
25	736.8	735.6	736.9	04.1	16.5	09.8	10.0	17.5	03.8	-00.6	04.8	05.2	06.0	78	37	67	61	SW	1	NE	1	SW	2
26	737.7	737.2	735.0	02.0	17.4	12.1	10.9	18.6	02.0	-02.4	05.1	05.6	07.5	97	38	71	69	NE	1	E	1	NE	1
27	739.1	737.4	736.6	06.5	16.0	11.9	11.6	17.3	06.0	01.2	06.8	06.5	07.5	93	48	72	71	SW	1	SE	2	NW	2
28	735.4	733.0	734.5	06.2	18.4	13.0	12.6	19.0	05.6	00.0	06.3	06.3	05.8	89	39	52	60	NE	1	ENE	3	NE	2
29	734.9	737.4	738.0	09.6	09.2	08.6	09.0	13.3	08.0	01.3	04.3	06.1	05.3	48	70	63	60	NE	3	NE	1	E	1
30	736.5	735.5	735.1	08.4	11.7	09.8	09.6	12.2	06.8	03.8	04.9	05.2	05.5	59	51	60	57	SE	2	NE	3	W	1
31	735.0	733.6	735.4	02.0	18.1	09.4	09.7	18.5	01.7	-01.6	05.0	05.1	05.6	93	32	63	63	E	1	S	2	NE	1
MES.																							
MED.	739.1	738.2	739.1	00.5	10.4	05.5	05.5	11.7	00.0	-04.2	04.0	04.1	04.3	84	44	63	64		1.4		2.0		1.5

1973 APRIL

LJUBLJANA BEŽIGRAD

1	737.1	735.5	735.8	06.1	18.0	10.6	11.3	18.1	05.3	-00.4	06.0	06.0	06.9	85	39	72	65	SE	1	S	1	SW	1
2	735.5	731.2	728.2	05.9	18.4	12.2	12.2	18.8	05.7	02.4	06.2	06.3	06.1	89	39	57	62	N	1	S	3	SE	4
3	724.3	730.4	731.9	08.8	01.8	02.9	04.1	12.5	00.7	02.4	07.1	05.0	04.9	83	95	88	89	NE	1	S	2	SE	1
4	734.7	736.6	741.3	05.0	11.4	06.0	07.1	11.9	02.3	-01.7	03.3	03.0	02.8	51	30	40	40	NE	1	NE	4	NE	1
5	742.0	739.2	739.0	00.3	13.2	07.2	07.0	13.6	-01.3	-07.3	03.2	03.4	03.5	69	30	45	48	N	1	SW	3	NE	1
6	739.9	736.4	734.8	01.0	17.0	11.9	10.4	18.3	00.3	-05.6	04.1	04.8	04.6	82	33	44	53	NE	1	SE	1	SE	2
7	732.4	729.4	731.0	05.2	18.8	11.0	11.5	19.0	03.6	-01.6	05.4	05.2	06.2	82	32	63	59	N	1	SW	2	SW	1
8	733.9	732.7	731.8	02.5	04.0	03.2	03.2	11.1	02.4	02.0	05.4	05.7	05.5	98	94	95	96	NE	1	NE	2	NE	1
9	728.6	726.9	726.1	02.0	04.4	05.0	04.1	05.2	01.0	00.2	05.1	06.1	06.4	97	97	97	97	N	1	NW	1	SW	1
10	721.5	725.0	727.4	06.4	09.8	05.9	07.0	10.6	04.4	03.2	06.8	05.6	05.9	95	61	85	80	SW	3	E	3	N	1
11	730.3	730.6	731.2	04.0	09.0	05.4	06.0	10.7	03.5	01.6	05.6	04.1	05.9	91	48	87	75	NW	1	S	3	E	1
12	732.1	731.0	731.4	03.6	07.6	04.8	05.2	08.1	03.4	01.0	05.6	06.0	06.1	94	77	94	88	N	1	SW	1	NE	1
13	732.4	733.2	735.1	02.2	03.4	02.2	02.5	08.1	01.4	00.5	05.0	04.8	04.7	94	82	87	88	SE	1	NW	3	SE	1
14	735.5	735.9	737.3	-00.2	08.9	05.2	04.8	09.6	-00.6	-04.0	03.9	02.8	03.3	86	33	50	56	SW	2	NW	4	NW	3
15	737.5	737.5	738.3	02.0	10.1	05.7	05.9	11.2	01.2	-03.2	04.1	04.4	05.1	78	48	74	67	E	1	NE	2	SE	1
16	738.8	739.0	740.2	04.0	10.6	06.0	06.6	11.4	01.7	-01.8	05.0	04.8	04.8	82	50	68	67	SE	1	NE	3	N	1
17	740.7	737.5	735.6	01.7	15.7	11.5	10.1	16.8	-00.3	-06.1	04.3	03.4	04.6	84	25	45	51	NE	1	SE	1	SE	3
18	734.6	734.1	734.0	06.8	07.6	05.0	06.1	11.7	05.0	-00.5	05.4	06.0	06.2	73	77	94	81	N	1	N	2	NE	1
19	729.9	725.9	726.5	03.6	10.7	05.4	06.3	11.0	02.7	-01.0	05.8	05.8	06.4	97	60	94	84	SE	1	SE	2	N	2
20	725.6	724.7	725.3	01.9	04.9	05.4	04.4	07.7	01.6	01.2	04.8	05.7	05.2	92	87	77	85	SE	1	S	2	S	2
21	725.5	727.4	730.2	04.5	11.9	06.4	07.3	12.3	03.5	01.2	05.6	03.1	04.8	88	30	66	61	SE	1	NW	2	SE	1
22	732.1	733.6	735.6	02.4	12.5	07.2	07.4	13.7	00.0	-05.0	04.8	03.7	05.8	87	34	76	66	NE	1	S	3	S	3
23	736.3	732.9	731.9	03.2	15.6	10.6	10.0	16.2	00.8	-04.2	04.5	04.9	03.7	79	37	39	52	SE	1	NW	1	NE	2
24	725.0	728.1	728.4	07.7	08.4	06.8	07.4	11.0	06.8	05.9	06.5	06.0	07.2	82	72	97	84	NE	3	NE	2	SW	1
25	727.8	730.5	733.3	06.2	09.2	08.2	08.0	09.7	05.7	05.0	06.8	07.9	07.5	96	90	92	93	W	1	SW	1	-	0
26	736.0	735.6	736.4	06.5	15.7	10.0	10.6	16.3	06.0	02.3	07.3	05.9	07.1	100	44	77	74	NE	1	SE	1	SW	1
27	737.1	736.5	736.3	08.6	14.6	10.0	10.8	14.9	07.4	03.9	07.5	06.7	07.3	90	54	79	74	NW	1	E	2	SW	1
28	734.9	733.5	733.4	05.0	14.6	12.0	10.9	17.3	03.2	-00.2	06.4	07.2	07.0	99	58	67	75	N	1	SW	3	W	2
29	731.9	732.3	733.4	11.0	11.7	12.0	11.7	12.6	05.4	07.2	07.4	09.1	09.4	75	88	89	84	SW	2	NW	2	SW	2
30	737.9	738.0	738.6	09.2	20.9	14.4	14.7	22.2	06.1	00.7	07.3	09.4	08.8	83	51	71	68	NE	1	SW	3	SW	3
MES.																							
WED.	733.2	732.7	733.3	04.6	11.3	07.7	07.8	13.0	03.1	-00.1	05.5	05.4	05.8	86	56	74	72	1.2		2.2		1.5	

BR. 51.13

 $H_s = 299 \text{ m}$ $H_b = 300.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.5 \text{ m}$

Dan	Vrijeme 0-6	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8	C4 ¹	00	00	00	C1.3	C6.2	.	$\angle^{\circ}n-10_1 = 6^{\circ}4-7_1 \odot$
2	7	C5 ¹	00	00	00	04.7	C5.6	.	$\angle^{\circ}n-10^{\circ}_{14} = n-12^{\circ}_{14} \odot$
3	6	C9 ¹	02	01	01	C7.0	C6.6	.	$\angle^{\circ}n-10_1 = n-11^{\circ}_{12} \odot 7^{\circ}_{14}-9_1 \odot$
4	5	09 ¹	07	00	00	05.3	C4.6	.	$\angle^{\circ}n-8^{\circ}_{14} \odot$
5	7	10 ²	C4 ¹	00	00	04.7	C5.1	.	$\angle^{\circ}n-9^{\circ}_{14} = n-12_1 \odot 12-16^{\circ}_{14} \odot$
6	7	00 ¹	10 ¹	10 ¹	10 ¹	06.7	04.2	.	$\angle^{\circ}n-10^{\circ}_{12} = n-13^{\circ}_{12} 19^{\circ}_{12}-n_1 \odot 13^{\circ}_{12}-19^{\circ}_{12} \odot$
7	7	05 ¹	10 ¹	10 ¹	10 ¹	05.7	00.6	.	$\angle^{\circ}n-8^{\circ}_{12} = n-12_1 \odot n_1 \odot 12-n_1 \odot$
8	7	10 ¹	10 ¹	05 ¹	05 ¹	05.7	00.0	.	$\odot n-4^{\circ}_{12} \odot 10^{\circ}_{14}-16^{\circ}_{12} \odot$
9	7	C6 ¹	10 ²	10 ¹	05 ¹	06.7	01.8	.	$\angle^{\circ}n-8^{\circ}_{12} \odot n-8^{\circ}_{12} \odot 7^{\circ}_{12}-8^{\circ}_{12} \odot = 9^{\circ}_{14}-10^{\circ}_{14} \odot \text{tr-} 13-16^{\circ}_{12} \odot$
10	9	C6 ¹	06 ¹	06 ¹	06 ¹	06.7	C5.1	C0.2	$\odot 10-14^{\circ}_{12} \odot$
11	8	C5 ¹	02 ¹	00	00	03.7	C8.2	.	$\odot$
12	7	03 ¹	10 ¹	10 ¹	07 ¹	07.7	C8.1	.	$\angle^{\circ}n-8^{\circ}_{12} = n-10^{\circ}_{12} 20-n_1 \odot 11^{\circ}_{12}-19^{\circ}_{12} \odot 19^{\circ}_{14}-n_1 \odot$
13	6	C9 ¹	10 ²	03 ¹	07 ¹	07.3	02.3	.	$\odot$
14	8	C7 ¹	05 ¹	05 ¹	05 ¹	08.3	C5.3	.	$\odot n-9^{\circ}_{14} \odot$
15	7	10 ¹	10 ¹	10 ¹	10.0	00.0	C0.0	00	$\text{tr-} n-8^{\circ}_{12} = n-7^{\circ}_{14} \odot$
16	7	C5 ¹	C6 ¹	10 ¹	05.0	05.0	C0.0	C0	$\odot = 6^{\circ}_{12}-10^{\circ}_{12} 19^{\circ}_{12}-n_1 \odot$
17	7	C6 ¹	03 ¹	00	03.7	05.1	.	.	$\odot = 4^{\circ}_{12}-9^{\circ}_{14} \odot$
18	7	06 ¹	09 ¹	00	05.0	C5.4	.	.	$\angle^{\circ}n-10_1 = 5^{\circ}_{12}-12^{\circ}_{14} \odot 12^{\circ}_{14}-16^{\circ}_{12} \odot$
19	8	C5 ¹	05 ¹	03 ¹	05.7	07.6	.	.	$\angle^{\circ}n-8^{\circ}_{14} = 4^{\circ}_{12}-10^{\circ}_{12} \odot$
20	6	00 ¹	C5 ¹	00	03.0	05.4	.	.	$\odot = n-4^{\circ}_{14} \odot \angle^{\circ}n-8^{\circ}_{12} \odot 9^{\circ}_{12}-11^{\circ}_{12} \odot$
21	7	C4 ¹	05 ¹	00	03.0	C6.7	.	.	$\angle^{\circ}n-8^{\circ}_{12} = 4^{\circ}_{12} 11^{\circ}_{12} \odot 11^{\circ}_{12}-18_1 \odot$
22	8	C1 ¹	00 ¹	00	00.3	10.2	.	.	$\angle^{\circ}n-8^{\circ}_{12} = 5^{\circ}_{12}-10^{\circ}_{12} \odot$
23	8	C0 ¹	00 ¹	00	00.0	08.8	.	.	$\odot = n-9^{\circ}_{14} \odot n-9_1 \odot 9^{\circ}_{14}-11^{\circ}_{12} \odot$
24	8	C1 ¹	04 ¹	10 ¹	05.0	08.4	.	.	$\odot = n-11^{\circ}_{12} \odot n-11^{\circ}_{12} 8^{\circ}_{12} \odot$
25	6	C9 ¹	C5 ¹	02 ¹	05.3	07.3	.	.	$\odot$
26	6	C8 ¹	04 ¹	10 ¹	07.3	C6.7	.	.	$\text{tr-} 17^{\circ}_{12} 18^{\circ}_{14} 20^{\circ}_{12}-n_1 \odot$
27	8	C8 ¹	10 ¹	05 ¹	05.0	04.4	C0.0	.	$\odot = n-8^{\circ}_{12} \odot \text{tr-} 5^{\circ}_{12} 5^{\circ}_{12} \odot \text{tr-} 13^{\circ}_{14}-14_1 \odot$
28	8	C3 ¹	C7 ¹	02 ¹	04.0	07.5	C0.0	.	$\angle^{\circ}n-8^{\circ}_{14} = n-10^{\circ}_{12} \odot$
29	7	10 ²	10 ¹	10 ¹	10.0	00.0	.	.	$\odot \text{tr-} 8^{\circ}_{12}-13^{\circ}_{14} \odot$
30	8	C9 ¹	10 ¹	05 ¹	05.3	00.1	00.6	.	$\odot$
31	8	C4 ¹	05 ¹	02 ¹	03.7	07.6	.	.	$\angle^{\circ}n-8^{\circ}_{14} = n-10^{\circ}_{12} \odot$
PES.									
RED.		C6.4	C6.5	C5.0	06.0	172.0	C0.6		

LJUBLJANA BEŽIGRAC

1973 APRIL

1	8	C6 ¹	03 ¹	00	03.0	06.4	C0.0	.	$\text{tr-} 5^{\circ}_{14}-5^{\circ}_{12} \odot$
2	8	10 ¹	06 ¹	08 ¹	06.0	C3.7	.	.	$\angle^{\circ}n-9_1 = 1^{\circ}_{12} 12^{\circ}_{14} \odot$
3	5	10 ¹	10 ¹	10 ¹	10.0	00.0	C0.2	.	$\odot = 5^{\circ}_{14}-15^{\circ}_{12} \odot 8^{\circ}_{14}-9^{\circ}_{12} 12^{\circ}_{12} 13^{\circ}_{12} \odot \text{tr-} 2^{\circ}_{12} 9^{\circ}_{12} 12^{\circ}_{12} \odot \odot$
4	8	C7 ¹	03 ¹	01 ¹	03.7	10.1	28.4	C3	$\odot \odot$
5	8	01 ¹	05 ¹	00	02.0	11.7	.	.	$\angle^{\circ}n-8_1 \odot$
6	8	03 ¹	02 ¹	05 ¹	03.3	10.5	.	.	$\angle^{\circ}n-7^{\circ}_{14} \odot$
7	8	C8 ¹	01 ¹	03 ¹	04.0	10.2	.	.	$\odot$
8	6	10 ¹	10 ¹	10 ¹	10.0	00.0	10.0	.	$\odot = n-n_1 \odot \text{tr-} n-n_1$
9	5	10 ¹	10 ¹	10 ¹	10.0	00.0	12.5	.	$\odot = n-n_1 \odot \text{tr-} n-n_1$
10	7	10 ¹	05 ¹	04 ¹	07.7	C6.5	28.5	.	$\odot = n-9^{\circ}_{12} \odot \text{tr-} 2^{\circ}_{12} n-10_1 = 4^{\circ}_{12}-7^{\circ}_{12} \odot \text{tr-} 10-16^{\circ}_{12} \odot 18^{\circ}_{12} 19^{\circ}_{14} \odot 18^{\circ}_{14} \odot$
11	8	C7 ¹	05 ¹	10 ¹	06.7	C5.6	14.5	.	$\text{tr-} 0^{\circ}_{12} 7^{\circ}_{12} 17^{\circ}_{12} 20^{\circ}_{14} \odot$
12	7	10 ¹	10 ¹	10 ¹	10.0	00.0	C0.3	.	$\odot = n-10^{\circ}_{12} 18^{\circ}_{12} \odot \text{tr-} 0^{\circ}_{12} 11^{\circ}_{12} 18^{\circ}_{12} \odot$
13	7	10 ¹	10 ¹	10 ¹	10.0	02.8	C7.2	.	$\odot \text{tr-} n-7^{\circ}_{14} \odot = 16^{\circ}_{12} 10^{\circ}_{12} \odot 13^{\circ}_{12} 13^{\circ}_{12} \odot 13^{\circ}_{12} 14^{\circ}_{12} \odot 20-n_1 \odot$
14	8	C6 ¹	05 ¹	10 ¹	09.0	03.8	C0.3	00	$\odot = n-4^{\circ}_{12} \odot \angle^{\circ}n-7^{\circ}_{12} \odot 14^{\circ}_{12} 5^{\circ}_{12} = 5^{\circ}_{12} 8^{\circ}_{12} \odot$
15	8	03 ¹	07 ¹	01 ¹	03.7	07.2	.	.	$\odot = n-4_1 \odot n-9_1 19^{\circ}_{12} \odot \text{tr-} 16^{\circ}_{12} 16^{\circ}_{12} \odot$
16	8	10 ¹	10 ¹	01 ¹	07.0	01.8	C0.0	.	$\angle^{\circ}n-9^{\circ}_{12} = 6^{\circ}_{14}-7^{\circ}_{14} \odot$
17	7	01 ¹	05 ¹	10 ¹	05.3	10.5	.	.	$\angle^{\circ}n-7^{\circ}_{12} = 4^{\circ}_{12}-10^{\circ}_{12} \odot$
18	7	C5 ¹	10 ¹	03 ¹	07.3	01.4	.	.	$\angle^{\circ}n-9_1 = 4^{\circ}_{12}-8^{\circ}_{12} 15^{\circ}_{12} 19^{\circ}_{12} \odot \text{tr-} 0^{\circ}_{12} 13^{\circ}_{12} 19^{\circ}_{12} \odot$
19	7	10 ¹	10 ¹	10 ¹	10.0	01.8	C2.0	.	$\odot = n-1^{\circ}_{12} 8^{\circ}_{12} \odot = 0^{\circ}_{12} 4^{\circ}_{12}-5^{\circ}_{12} 14^{\circ}_{12}-8^{\circ}_{12} \odot = 8^{\circ}_{14}-9^{\circ}_{12} \odot 14^{\circ}_{12} 15^{\circ}_{14} \odot \text{tr-} 20^{\circ}_{12} 21^{\circ}_{12} \odot$
20	7	10 ¹	10 ¹	10 ¹	10.0	01.4	C1.6	00	$\odot \text{tr-} 6^{\circ}_{12} 8^{\circ}_{12} 16^{\circ}_{12} \odot = 5^{\circ}_{12} 12^{\circ}_{12} \odot \text{tr-} 6^{\circ}_{12} 8^{\circ}_{12} \odot$
21	8	10 ¹	07 ¹	07 ¹	06.0	C4.5	C2.0	C0	$\angle^{\circ}n-9^{\circ}_{12} \odot$
22	8	C0 ¹	C4 ¹	01 ¹	01.7	C6.6	.	.	$\angle^{\circ}n-8_1 = 4^{\circ}_{14}-9^{\circ}_{12} \odot$
23	6	C2 ¹	05 ¹	10 ¹	05.7	C7.2	.	.	$\angle^{\circ}n-7^{\circ}_{12} = 4^{\circ}_{12}-7^{\circ}_{12} \odot$
24	7	10 ¹	10 ¹	10 ¹	10.0	00.0	C0.2	.	$\text{tr-} 0^{\circ}_{12} 4^{\circ}_{12} 10^{\circ}_{12} 13^{\circ}_{12} \odot = 5^{\circ}_{12} 18^{\circ}_{12} \odot$
25	7	10 ¹	10 ¹	10 ¹	10.0	00.0	17.1	.	$\text{tr-} 0^{\circ}_{12} n-20^{\circ}_{14} \odot = n-10^{\circ}_{14} \odot$
26	7	10 ¹	04 ¹	03 ¹	05.7	C7.1	C8.6	.	$\odot n_1 = 0^{\circ}_{12}-7^{\circ}_{12} = 17^{\circ}_{12} 7^{\circ}_{12} = 7^{\circ}_{12} 11^{\circ}_{12} \odot 13^{\circ}_{12}-17_1 \odot$
27	7	10 ¹	06 ¹	02 ¹	06.7	C1.5	C0.4	.	$\odot n-14^{\circ}_{12} \odot \text{tr-} 0^{\circ}_{12} 4^{\circ}_{12}-5^{\circ}_{12} 14^{\circ}_{12} 13^{\circ}_{12} \odot \text{tr-} 19^{\circ}_{12} n_1 \odot$
28	7	C6 ¹	05 ¹	10 ¹	06.0	C5.2	C0.0	.	$\odot = n-9^{\circ}_{12} \odot 2^{\circ}_{12}-9^{\circ}_{12} \odot 9^{\circ}_{12}-n_1 \odot$
29	7	10 ¹	10 ¹	05 ¹	05.7	C0.0	C0.0	.	$\odot \text{tr-} 17^{\circ}_{12} 17^{\circ}_{12} \odot$
30	8	C0 ¹	C7 ¹	00	02.3	12.1	C0.7	.	$\odot = n-6^{\circ}_{12} \odot n-10^{\circ}_{12} \odot$
PES.									
RED.		C7.4	C7.4	C6.3	C7.0	138.1	136.2		

$\varphi = 46^{\circ} 04' N$ $\lambda = 14^{\circ} 31' E$ Gr. ΔG = + 58 min.

BR. ST.13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napoin vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21
1	736.4	737.5	737.5	10.1	20.4	15.3	15.3	20.6	07.7	02.3	08.4	08.1	08.9	91	45	68	68	NE	1	SW 3
2	736.7	736.3	736.3	15.3	24.2	17.1	18.4	24.3	13.0	10.1	09.0	09.1	07.9	69	40	54	54	SW	3	SW 4
3	735.1	733.9	735.4	16.4	24.1	16.6	16.4	24.2	13.1	08.5	10.1	08.9	07.8	72	39	55	55	SW	3	SW 4
4	736.3	737.3	739.4	13.0	23.0	17.5	18.0	23.6	09.4	04.9	09.4	10.2	11.8	84	48	76	69	NE	1	SW 3
5	739.4	736.6	739.5	17.3	25.7	19.6	20.6	26.3	15.5	10.4	09.7	10.7	11.5	66	43	66	58	SW	3	SW 4
6	739.3	737.1	735.8	15.0	27.3	20.4	20.6	27.7	12.1	06.6	10.7	09.4	09.6	84	34	54	57	E	1	S 3
7	735.3	735.5	736.3	17.7	22.3	15.0	17.5	22.4	15.0	12.5	11.0	07.4	07.9	72	37	62	57	S	3	SW 4
8	735.1	734.9	737.3	13.3	19.8	11.0	13.6	19.8	09.5	02.6	07.4	07.7	07.6	64	44	78	62	SW	1	SW 4
9	740.2	737.8	738.9	07.2	16.4	05.6	10.7	16.7	06.6	03.4	07.1	07.0	07.1	93	50	79	74	S	2	NW 1
10	736.5	735.4	735.0	07.0	18.4	12.3	12.5	19.7	02.4	-01.5	06.5	04.9	07.2	87	31	67	62	SE	1	SE 2
11	736.0	735.3	736.3	05.9	19.3	12.6	13.6	21.0	06.7	02.2	06.9	06.4	07.7	76	38	71	62	NW	1	SW 5
12	742.5	741.8	742.8	08.4	14.0	05.0	10.1	14.6	08.2	07.8	08.1	06.5	06.7	97	54	78	76	S	2	SE 2
13	743.4	741.3	741.3	04.6	17.4	11.2	11.2	19.7	02.0	-01.6	06.3	05.1	07.3	99	34	72	68	S	1	SSW 3
14	742.3	739.1	736.1	07.7	22.1	16.5	15.7	23.8	03.9	-01.2	06.7	06.5	07.0	85	33	50	56	NE	1	NE 1
15	738.0	736.0	736.4	10.9	24.1	15.5	16.5	24.9	07.4	03.5	07.9	07.7	09.8	81	34	74	63	NE	1	SSW 3
16	740.1	740.1	740.3	08.8	10.6	09.0	09.4	15.7	08.4	03.0	07.2	06.4	05.5	85	66	64	72	SE	1	E 3
17	739.6	738.0	738.5	08.8	15.4	10.6	11.4	16.3	04.9	00.5	06.2	05.2	06.3	73	39	64	59	E	1	M 2
18	738.1	737.2	736.4	07.0	15.0	13.1	12.0	16.3	05.2	00.3	05.9	06.5	08.0	79	51	71	67	NE	1	SW 2
19	735.0	731.4	729.5	05.9	22.6	16.6	16.5	23.1	07.6	03.1	07.9	08.2	09.9	86	40	69	65	NW	1	SSW 2
20	730.7	732.5	733.5	15.3	20.0	15.2	16.4	20.4	12.7	08.5	11.2	09.0	09.0	86	51	69	65	SSW	2	SW 5
21	734.0	734.8	734.3	16.2	19.5	16.0	16.5	22.8	10.4	05.6	09.0	09.7	09.5	65	57	70	64	SW	2	SSW 4
22	736.5	735.8	736.8	14.6	25.2	17.6	18.8	25.6	05.6	04.6	05.5	07.6	10.2	76	31	68	58	NE	1	SW 3
23	737.6	737.1	738.3	13.6	25.8	18.4	19.0	26.1	11.9	09.0	09.6	10.2	09.8	82	41	62	62	NE	1	SW 3
24	740.4	738.7	740.9	17.4	24.8	14.7	17.9	25.0	13.1	07.6	10.6	08.5	11.9	71	36	95	67	NE	1	ENE 2
25	741.1	739.6	740.8	12.4	21.6	14.5	16.0	23.6	11.0	07.4	10.3	08.4	11.5	96	43	91	77	NE	1	SSW 2
26	741.8	739.7	740.6	10.3	21.7	15.6	15.8	22.4	05.1	04.6	05.2	07.0	08.1	98	36	61	65	S	1	N 1
27	740.9	738.5	740.4	12.1	23.4	16.6	17.3	24.0	07.2	02.3	08.2	06.8	05.9	77	31	41	50	SW	1	NE 1
28	740.7	738.3	737.4	11.2	22.6	15.8	16.4	23.8	06.5	01.8	07.4	07.8	08.5	74	38	63	58	NE	1	NE 2
29	736.4	733.3	733.4	12.6	26.0	19.0	19.2	26.6	08.6	03.7	08.4	09.9	10.8	77	39	66	61	NE	1	SE 1
30	734.0	733.6	734.9	15.0	17.4	13.4	14.8	23.6	12.3	07.0	09.1	13.0	10.8	71	87	94	84	S	3	SE 3
31	735.5	734.5	735.5	12.6	23.2	18.4	18.2	25.0	11.4	08.4	10.5	12.1	11.3	96	57	71	75	SW	1	NE 1
MES.																				
RED.	738.1	736.6	737.5	12.0	21.1	15.0	15.8	22.2	05.1	04.8	08.6	08.1	08.8	81	43	68	64	1.4	2.7	1.9

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LJUBLJANA BEŽIGRAD

1	735.5	734.3	734.7	13.5	25.7	20.2	19.5	26.0	12.4	08.7	11.6	11.7	10.3	100	47	58	68	NW	1	SW 4
2	735.5	735.6	736.1	16.4	26.5	20.6	21.0	26.9	12.0	07.2	09.7	11.0	10.1	69	43	55	56	NE	1	W 3
3	737.3	737.4	738.1	17.2	24.3	20.5	20.6	25.4	14.4	10.4	10.7	11.5	12.5	73	51	69	64	E	2	SE 2
4	739.5	741.0	741.5	16.2	16.2	17.0	16.6	20.7	14.7	11.3	11.9	13.0	13.8	86	94	95	92	SE	1	NE 1
5	742.5	741.3	741.4	14.1	24.4	19.6	19.4	25.1	13.5	07.5	11.9	12.0	13.3	99	53	77	76	-	0	NE 1
6	740.6	736.6	737.4	16.6	19.0	15.5	16.6	21.5	15.5	13.0	13.2	15.3	12.8	93	93	97	94	NE	1	NE 2
7	736.1	734.3	735.9	14.4	15.2	11.4	13.1	15.9	11.2	13.6	11.5	11.4	09.2	94	88	91	91	SE	1	N 2
8	734.9	733.8	733.1	11.0	17.2	14.2	14.2	18.4	10.4	09.8	08.9	10.1	11.4	91	68	94	84	N	1	SW 1
9	731.4	730.1	731.3	13.6	19.6	16.4	16.5	21.3	10.8	06.8	09.6	10.8	10.6	82	63	76	74	-	0	SW 2
10	732.8	732.9	734.1	15.4	26.6	19.6	20.4	27.0	12.8	08.2	11.2	08.2	12.1	85	31	70	62	NE	1	SW 1
11	736.3	735.7	737.1	16.5	26.4	15.0	20.2	26.6	14.3	10.5	11.5	11.7	13.3	82	45	81	69	SE	1	ENE 1
12	739.7	738.6	738.7	19.0	24.3	20.8	21.2	25.3	16.2	12.6	13.4	12.5	13.0	81	55	70	69	E	1	NE 3
13	738.9	737.4	737.5	16.8	26.6	22.4	22.0	27.2	15.0	10.8	12.6	15.0	11.8	88	57	58	68	SW	1	NE 1
14	738.2	736.7	740.9	17.7	24.5	15.6	18.4	27.5	14.0	10.0	12.0	14.1	12.8	79	61	95	78	-	0	NE 2
15	743.6	741.3	741.2	14.0	20.2	15.4	16.2	20.9	09.9	05.6	07.8	09.2	09.2	65	52	70	62	NE	1	ENE 2
16	741.1	738.5	739.1	11.8	20.1	16.6	16.3	20.7	08.6	04.9	08.8	08.3	08.9	85	47	63	65	NE	1	E 2
17	738.1	736.1	735.2	14.6	22.3	17.7	18.1	22.6	12.0	08.4	10.1	11.1	11.7	81	55	77	71	NE	1	SSW 2
18	734.0	733.5	734.9	14.4	19.2	18.4	17.6	22.0	13.6	07.2	11.5	13.5	12.7	94	81	80	85	N	1	W 1
19	736.5	733.7	734.9	16.0	24.8	17.6	19.1	25.1	12.1	08.0	10.6	10.5	12.9	78	45	84	69	E	1	E 1
20	736.4	733.5	733.6	16.0	24.6	15.4	15.8	25.2	14.7	11.0	08.2	10.8	09.4	60	47	55	54	E	1	SW 3
21	733.6	735.1	736.1	15.4	18.0	16.6	16.6	20.7	15.2	13.5	12.1	12.1	11.6	92	78	82	84	NE	1	N 1
22	735.7	735.2	733.5	15.0	14.4	14.7	14.7	16.9	14.0	13.6	12.3	11.9	12.0	96	97	96	96	N	1	NE 1
23	735.0	733.0	732.6	13.2	18.8	16.3	16.2	19.8	13.2	08.5	10.5	10.4	09.6	93	64	69	75	W	3	SW 2
24	731.6	732.0	732.1	14.0	16.8	15.6	15.5	19.6	13.0	12.5	10.5	11.4	12.5	88	79	94	87	W	1	SW 3
25	733.6	735.5	737.1	15.1	19.8	18.4	17.9	22.6	13.9	13.6	12.2	13.2	13.7	95	76	86	86	E	1	SE 1
26	740.3	740.6	741.0	16.4	26.1	19.6	20.4	26.9	14.1	10.0	12.0	11.7	13.8	86	46	81	71	NE	1	NE 3
27	741.4	740.0	740.7	15.7	28.0	21.6	21.6	28.5	13.5	10.0	13.0	12.5	13.0	97	44	67	69	NE	1	SW 3
28	740.7	739.2	738.4	18.2	28.6	23.5	23.4	29.0	15.2	11.7	13.1	14.4	12.2	84	49	56	63	NE	1	SW 3
29	736.1	736.5	741.0	19.6	29.3	16.2	20.3	29.6	16.1	12.5	12.4	14.0	12.7	73	46	92	70	E	1	SW 3
30	741.1	739.4	740.1	14.3	25.4	18.5	19.4	26.2	13.3	10.0	11.3	09.0	11.1	93	37	68	66	NW	1	NE 3
MES.																				
RED.	737.3	736.4	737.0	15.4	22.4	18.0	18.4	23.7	13.3	10.0	11.2	11.7	11.8	85	60	77	74	1.0	2.0	1.4

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		7	14	21	Sred Dias				
14	7	7	14	21	Sred Dias	7	7		
1	7	01 ⁰	03 ¹	10 ⁰	C4.7	1C.6	.	.	$\Delta^1 n-10^{1/2}, \infty 12^{1/2}-16^{1/4} \odot$
2	8	01 ⁰	05 ¹	02 ¹	C4.C	1C.5	.	.	$\Delta^0 n-6^{1/2}, 20^{1/2} n-10, \infty 11-10^{1/2}, \nabla^{+0-1} 13^{40} 14^{10} \odot$
3	7	00 ⁰	05 ⁰	04 ¹	C3.C	05.6	04.0	.	$\Delta^0 n-10, \Delta^2 n-10, 100 10-n, \odot$
4	7	04 ¹	08 ⁰	03 ¹	C5.0	10.5	.	.	$\Delta^1 n-9^{1/4}, \Delta^2 n-9^{1/2}, \infty 9^{1/2} n, T^1 16^{24} 17 \odot$
5	7	00 ⁰	05 ⁰	01 ¹	C2.C	1C.5	.	.	$\Delta^2 n-9, \Delta^0 n-7, \Delta^1 n-7, \Delta^2 n-10^{45}, \infty 10^{45} n, \odot$
6	7	06 ¹	01 ⁰	00	C2.3	1C.8	.	.	$\Delta^0 n-5^{1/4}, \Delta^1 n-8, \infty 5^{1/4} n, \odot$
7	7	00 ⁰	10 ¹	09 ¹	C6.3	C3.5	.	.	$\Delta^0 7^{15} 10, \Delta^0 1^{25} 14^{3/4}, \Delta^1 10^{15} 10^{16}, 13^{30} 14^{3/4}-16^{3/4}, \Delta^0 10^{25} 14^{3/4}, \Delta^0 1^{25} 16^{55} \odot$
8	7	10 ¹	05 ⁰	07 ¹	C7.3	1C.0	03.7	.	$\Delta^0 n-10^{45} \odot$
9	7	05 ¹	05 ¹	10 ²	C5.3	C1.4	.	.	$\Delta^0 n-9^{1/2}, \infty 9^{1/2}-15^{1/2}, T^{13-14} 12^{1/2} 14^{1/2}, \Delta^0 19^{80}, \nabla^{+0-1} 15^{42} 19^{1/2}, \Delta^0 1^{19} 12-n, \odot$
10	7	10 ²	10 ⁰	01	C7.C	C1.1	05.9	.	$\Delta^0 n-13^{1/2}, \Delta^0 1^{18} 12-n, \odot$
11	7	10 ¹	04 ⁰	03 ¹	C5.7	C8.7	CC.C	.	$\Delta^0 n-6, \Delta^1 n-9, 20^{1/2} n, \Delta^0 6-7, \Delta^1 7-10, \odot$
12	7	06 ⁰	07 ⁰	00	C4.3	C8.C	.	.	$\Delta^1 n-9^{1/2}, \Delta^0 6^{1/4}-11, \infty 11^{1/2} n, T^{11^{40}} 11^{40}, \Delta^0 11^{40}, \Delta^0 11^{20} \odot$
13	8	10 ¹	05 ⁰	08 ¹	C7.7	C7.C	C5.8	.	$\Delta^0 n-8^{20}, \Delta^0 1^{15} 16^{3/4}, \Delta^1 1^{35} 14^{45}, \Delta^0 1-2, 5-7^{35} \odot$
14	7	10 ⁰	10 ¹	03 ⁰	C7.7	C1.7	CC.1	.	$\Delta^0 n-5^{1/4}, \Delta^1 n-8^{1/4}, \Delta^0 5^{1/4}-6^{1/2}, \Delta^0 6^{1/2}-11^{30}, \Delta^0 11^{35}, 14^{15} 15^{08}, \infty 11^{30} 14^{15} \odot$
15	7	10 ¹	06 ⁰	05 ¹	C7.0	C4.6	CC.5	.	$\Delta^0 n-7^{1/4}, \Delta^0 n-5, \Delta^0 6^{1/2}-9^{1/4}, 18^{45} 18^{45}, \Delta^0 7^{1/4}-11, \infty 11-n, \Delta^0 20^{1/2} n, \odot$
16	7	05 ²	06 ⁰	01 ⁰	05.3	06.7	C1.6	.	$\nabla^{+0-1} 3^{35} 10^{15}, \Delta^0 6^{30} 10^{1/2} \odot$
17	7	01 ⁰	07 ⁰	01 ⁰	C3.C	1C.8	C1.1	.	$\Delta^1 n-8, 20^{40} n, \odot$
18	8	04 ⁰	04 ⁰	09 ²	05.7	12.1	.	.	$\Delta^0 n-8^{1/2}, \Delta^0 1^{18} 14-9, 18^{30} 18^{30}, T^{14^{1/4}} 15, \odot$
19	8	05 ⁰	09 ⁰	08 ¹	07.3	06.8	CC.C	.	$\nabla^{+0-1} 2^{1/4}, 17^{20}, \Delta^0 1-2, 14^{3/4}-11^{30}, \odot$
20	8	09 ²	02 ⁰	04 ¹	C5.0	10.3	<u>25.2</u>	.	$\Delta^0 n-6^{1/2}, \Delta^0 1^{20} 15 n, \odot$
21	7	01 ⁰	04 ⁰	05 ¹	C3.3	12.C	.	.	$\Delta^0 n-9, \Delta^0 4^{1/4}-9^{1/2}, \Delta^0 5^{1/4}-6^{1/4}, \Delta^0 5^{1/2}-5^{1/4}, \infty 9^{1/2}-12^{1/2}, \odot$
22	8	08 ²	05 ⁰	10 ²	07.7	06.5	1C.6	.	$\Delta^0 n-4^{55}, \Delta^0 4^{1/4}-11^{1/2}, \Delta^0 1-2, 15^{55} 6^{1/2}, \Delta^0 15-6^{1/2}, \Delta^0 19^{30} n, \Delta^0 6^{1/2}-7^{35}, T^{19^{27}} 19^{30} \odot$
23	8	05 ⁰	03 ⁰	06 ²	04.7	11.7	17.6	.	$\Delta^0 6^{1/4}-6^{1/4} \odot$
24	7	09 ¹	10 ²	09 ¹	C5.3	C1.2	.	.	$\Delta^0 n-9, T^{09^{45}} 18^{1/4}, \Delta^0 10^{15} 16^{1/2}, \Delta^0 16^{1/2}-18^{1/2}, \odot$
25	8	09 ¹	10 ¹	07 ¹	C6.7	03.5	17.C	.	$\Delta^1 n-6^{1/5}, \Delta^0 n, \Delta^0 6^{1/5} 10^{1/2}, \Delta^0 1^{14} 15^{1/4}, \odot$
26	7	08 ¹	07 ²	02 ⁰	05.7	07.3	CC.1	.	$\Delta^1 n-9^{1/4}, 20^{1/4} n, T^{13^{3/4}} 14-14^{40}, \Delta^0 1^{14} 15^{55} 18^{40} 14^{40} 15^{35} \odot$
27	7	10 ¹	06 ¹	02 ¹	C6.C	05.4	C1.6	.	$\Delta^0 n-9^{1/4}, \Delta^0 4^{1/4}, 8^{3/4}-9^{1/2}, \Delta^0 4^{1/4}-4^{3/4}, \Delta^0 6^{1/4}-8^{3/4}, \Delta^0 4^{3/4}-6^{1/4}, T^{13^{35}} 16^{45}, \Delta^0 1^{13} 16^{35} \odot$
28	8	08 ²	06 ⁰	01 ¹	C5.C	10.4	1C.7	.	$\Delta^1 n-6^{1/2}, \Delta^0 6^{1/2}-6^{30}, \Delta^0 6^{30} 9^{1/4}, \odot$
29	8	08 ¹	06 ⁰	07 ¹	C8.0	C3.8	.	.	$\Delta^1 n-9^{1/2}, \Delta^0 1^{12} 14^{1/4}, \odot$
30	8	10 ¹	06 ⁰	05 ¹	C6.3	C6.3	CC.5	.	$\Delta^0 n-7^{1/4}, \Delta^0 2 n-6, 20^{1/2} n-7, \Delta^0 5^{3/4}-7, \Delta^0 7^{1/4}-8^{3/4}, \Delta^0 8^{3/4}-9^{1/2}, \odot$
31	8	05 ¹	06 ⁰	01 ⁰	05.3	07.3	CC.5	.	$\Delta^0 n-5^{1/4}, 7^{1/2}-10^{1/2}, \Delta^0 5^{1/4}, 17^{1/2}, \Delta^0 5^{50} 7, \odot$
MES. MED.		CC.4	CC.4	CC.8	CC.8	231.8	111.3		

1	7	1C ⁰ ≡	1C ¹ ⊙	C1 ⁰	C4.7	1C.3	.	.	Δ ¹ n-9 ¹ / ₄ , 20 ¹ / ₄ -n; = n-3 ¹ / ₂ , 7 ¹ / ₄ -10 ¹ / ₂ ; ≡ ⁰ -3 ¹ / ₂ -7 ¹ / ₄ ⊙
2	7	0C ⁰ ≡	1C ¹ ⊙	C5 ¹	C5.C	05.7	.	.	= n-4 ³ / ₄ , 7 ¹ / ₄ -9 ¹ / ₂ ; Δ ⁰ -n-9 ¹ / ₄ , 20 ¹ / ₄ -n; ≡ ⁰ -4 ³ / ₄ -7 ¹ / ₄ ⊙ 9 ¹ / ₂ -10 ¹ / ₂ , T ⁰ 4 ¹ / ₄ -15 ¹ / ₄ , Δ ¹ 15 ¹ / ₄
3	7	C8 ¹	1C ⁰ ⊙	C5 ¹	C7.7	C2.6	CC.C	.	= n-11 ¹ / ₂ , Δ ¹ n-9, ∞ 11 ¹ / ₂ -n, T ⁰ 12 ¹ / ₂ -14 ¹ / ₄ , 18 ¹ / ₂ -19, 20 ¹ / ₄ -16 ¹ / ₂ , Δ ¹ 16 ¹ / ₂ -17 ¹ / ₂ ⊙
4	7	10 ¹	08 ⁰ ⊙	02 ¹	C6.7	C6.3	CC.E	.	= n-14 ¹ / ₄ , ≡ ⁰ -2 ¹ / ₂ -5 ¹ / ₂ , ∞ 14 ¹ / ₄ -18, T ⁰ 13 ¹ / ₂ -14 ¹ / ₂ , Δ ¹ 14 ¹ / ₂ -20 ¹ / ₂ -n ⊙ [15 ¹ / ₂ ⊙
5	7	1C ² ≡	03 ⁰ ⊙	0C	C4.3	05.2	CC.1	.	Δ ¹ n-9 ¹ / ₂ , 20 ¹ / ₄ -n; = n-4 ¹ / ₄ , 18 ¹ / ₂ -9 ¹ / ₂ ; ≡ ⁰ -2 ¹ / ₄ -7 ¹ / ₂ ; ≡ ⁰ -2 ¹ / ₂ -7 ¹ / ₂ -8 ¹ / ₂ , ∞ 9 ¹ / ₂ -4 ¹ / ₂ ⊙
6	7	0C ⁰ ≡	02 ¹ ⊙	00	0C.7	11.2	.	.	≡ ⁰ -2n-4 ¹ / ₂ , 6 ¹ / ₂ -8 ¹ / ₄ ; Δ ¹ n-8 ≡ ⁰ -2 ¹ / ₂ -6 ¹ / ₂ ; = 8 ¹ / ₄ -11 ¹ / ₄ , ∞ 11 ¹ / ₄ -n ⊙
7	7	C5 ⁰ ⊙	C1 ⁰ ⊙	C1 ⁰	C2.3	11.6	.	.	= n-8 ³ / ₄ , Δ ¹ n-8 ¹ / ₂ ; ≡ ⁰ -1 ¹ / ₂ -6 ¹ / ₄ , ∞ 8 ³ / ₄ -n ⊙
8	7	10 ²	10 ¹ ⊙	0C	C6.7	C2.3	.	.	= n-10 ¹ / ₂ , Δ ¹ n-7 ³ / ₄ , 20 ¹ / ₄ -n; ≡ ⁰ -1 ¹ / ₂ -7 ³ / ₄ , 13 ¹ / ₄ ⊙
9	6	1C ² ≡	02 ⁰ ⊙	0C	C4.0	10.3	13.4	.	≡ ⁰ -n-8; ≡ ⁰ -n-8; = 8-11, ∞ 11-13 ⊙
10	6	CC ⁰ ⊙	0C ⁰ ⊙	0C	0C.C	12.5	.	.	Δ ⁰ -n-9 ¹ / ₂ , 20 ¹ / ₄ -n; ⊙
11	7	1C ⁰ ≡	0C ⁰ ⊙	C6 ¹	C5.3	C5.2	.	.	= n-4 ¹ / ₄ , 8-9 ¹ / ₄ ; Δ ⁰ -n-9, 20 ¹ / ₄ -n; ≡ ⁰ -4 ¹ / ₄ -4 ³ / ₄ , 7 ¹ / ₄ -8; ≡ ⁰ -2 ¹ / ₄ -7 ¹ / ₄ , ∞ 9 ¹ / ₄ -14 ¹ / ₂ ⊙
12	8	08 ¹	04 ⁰ ⊙	00	C4.C	C7.7	CC.C	.	= n-5 ¹ / ₂ , Δ ¹ n-4 ¹ / ₂ , Δ ¹ 4 ¹ / ₂ -5 ¹ / ₄ ⊙
13	7	C1 ⁰ ⊙	03 ⁰ ⊙	10	C4.7	C5.5	.	.	Δ ¹ n-9 ¹ / ₂ ; = n-8 ³ / ₄ ; ≡ ⁰ -5 ¹ / ₂ -6 ¹ / ₄ , ∞ 8 ³ / ₄ -n, T ⁰ 21 ⁰ ⊙
14	8	07 ⁰ ⊙	02 ¹ ⊙	00	C3.C	11.1	C4.C	.	Δ ¹ n, T ⁰ 17 ⁰ ⊙; Δ ¹ 20 ¹ / ₄ -n ⊙
15	7	CC ⁰ ⊙	02 ⁰ ⊙	02 ⁰ ⊙	01.3	12.3	00.C	.	Δ ⁰ -2n-10, 20 ¹ / ₂ -n; = 4 ¹ / ₂ -9 ³ / ₄ ⊙
16	7	01 ¹ ⊙	03 ¹ ⊙	C5 ¹	C3.C	11.3	.	.	Δ ¹ n-9 ¹ / ₄ ; = n-8 ³ / ₄ , ∞ 8 ³ / ₄ -n ⊙
17	7	C2 ¹ ⊙	C1 ⁰ ⊙	0C	C1.0	11.8	.	.	= n-9 ¹ / ₂ , Δ ⁰ -n-9, 20 ¹ / ₂ -n; ∞ 9 ¹ / ₂ -14 ¹ / ₂ ⊙
18	7	CC ⁰ ⊙	01 ⁰ ⊙	C5 ¹	C2.C	11.2	.	.	= n-9 ¹ / ₄ , Δ ¹ n-9, ∞ 9 ¹ / ₄ -n ⊙
19	7	0C ⁰ ⊙	01 ⁰ ⊙	C2 ¹	C1.C	11.5	.	.	Δ ⁰ -n-9, 20 ¹ / ₄ -n; = n-9 ¹ / ₂ , ∞ 9 ¹ / ₂ -12 ³ / ₄ ⊙
20	7	C1 ⁰ ⊙	C5 ⁰ ⊙	C4 ¹	C4.7	C5.3	.	.	Δ ¹ n-9; = n-11 ¹ / ₂ , ∞ 11 ¹ / ₂ -n, T ⁰ -117 ² / ₄ , 18 ¹ / ₄ , Δ ¹ 17 ⁴ / ₂ -18 ⁰ ⊙
21	7	C8 ² ⊙	02 ⁰ ⊙	C6 ¹ ⊙	C5.3	06.3	CC.C	.	= n-10 ¹ / ₂ , Δ ¹ n-9, ∞ 10 ¹ / ₂ -15 ¹ / ₄ , T ⁰ 15 ⁰ , Δ ¹ 16 ⁰ , T ⁰ 17 ⁰ -21 ⁰ ⊙
22	6	1C ¹	1C ¹	10 ²	1C.C	0C.C	C5.7	.	= n-11 ¹ / ₂ , Δ ¹ 18 ¹ / ₂ -9 ⁰ ⊙
23	7	1C ²	1C ⁰ ⊙	10 ¹	1C.C	C1.5	CC.C	.	= 4 ¹ / ₂ -12 ¹ / ₄ , 20 ¹ / ₄ -n; ∞ 12 ¹ / ₄ -20 ¹ / ₄ ⊙
24	7	C7 ⁰ ⊙	05 ¹ ⊙	0C	C4.C	C8.3	CC.7	.	= n-11 ¹ / ₂ , Δ ¹ 4 ¹ / ₂ -4 ⁰ ⊙
25	7	C5 ¹	05 ¹ ⊙	05 ² ⊙	05.0	04.5	.	.	Δ ¹ n-9 ¹ / ₂ ; = 4 ¹ / ₂ -9 ¹ / ₄ , T ⁰ 13 ⁰ -14 ⁰ , 20 ¹ / ₂ -n; ≡ ⁰ -1 ¹ / ₂ -17 ⁰ , Δ ¹ 17 ⁰ -21 ⁰ ⊙
26	6	1C ² ≡	1C ¹ ⊙	00	C6.7	0C.6	13.2	.	Δ ¹ n, T ⁰ 17 ⁰ ⊙; = n-4 ¹ / ₂ , 8 ¹ / ₂ -12 ¹ / ₄ , 20 ¹ / ₄ -n; ≡ ⁰ -4 ¹ / ₂ -4 ³ / ₄ , 7 ¹ / ₄ -8 ¹ / ₂ ; ≡ ⁰ -4 ³ / ₄ -7 ¹ / ₄ , ∞ 12 ¹ / ₄ -20 ¹ / ₄ ⊙
27	7	C6 ⁰ ⊙	10 ¹	1C ¹	C8.7	C3.3	.	.	= n-11 ¹ / ₂ , Δ ¹ n-10 ¹ / ₂ ; ≡ ⁰ -1 ¹ / ₂ -6 ¹ / ₄ , Δ ¹ 17 ⁰ -17 ⁰ ⊙ [12 ¹ / ₄ -20 ¹ / ₄ -n ⊙
28	6	10 ²	1C ²	1C ²	1C.C	0C.C	CC.C	.	= n-11 ¹ / ₂ , Δ ¹ 10 ¹ / ₂ -3 ¹ / ₂ , 7 ¹ / ₂ -10 ¹ / ₂ , 14 ¹ / ₂ -n
29	6	1C ² ●	1C ² ●	1C ² ●	1C.C	0C.C	27.2	.	= n-11 ¹ / ₂ , Δ ¹ 10 ¹ / ₂ -3 ¹ / ₂ , 7 ¹ / ₂ -10 ¹ / ₂ , 14 ¹ / ₂ -n
30	7	C9 ²	08 ⁰ ⊙	C6 ⁰	C7.7	C7.3	C3.4	.	= n-11 ¹ / ₂ , 19 ¹ / ₂ -n; ⊙
31	7	10 ² ≡	07 ¹ ⊙	10 ² ●	C5.C	04.1	CC.C	.	= n-5 ¹ / ₄ , 9 ¹ / ₄ -12 ¹ / ₂ ; ≡ ⁰ -5 ¹ / ₄ -9 ¹ / ₄ , 6 ¹ / ₂ -9, ∞ 12 ¹ / ₂ -16, T ⁰ 15 ⁰ -16 ⁰ , Δ ¹ 16 ⁰ -17 ⁰ , T ⁰ 16 ⁰ -17 ⁰ ⊙
RES.									
MED.									
		C6.2	C5.4	04.2	05.2	223.8	68.6		

88. ST. 57

 $H_s = 157 \text{ m}$ $H_b = 162.5 \text{ m}$ $h_t = 6.0 \text{ m}$ $h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)				Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies	7	7	
1	4	C8	1C	1C	C5.3	00.0	.	.	$\equiv n-n, \bullet^{tr} 12^{15} 12^{45}$
2	5	C5	1C	1C	C5.7	00.0	CC.0	.	$\equiv^{tr} n, \bullet \equiv n-n$
3	5	1C	1C	1C	1C.0	00.0	.	.	$\equiv n-n$
4	4	10*	1C*	1C*	1C.0	00.0	CC.1	.	$\equiv^{tr-0.1} n-n, \bullet \equiv n-n, \boxtimes$
5	4	1C	05	08	C5.0	00.0	C1.0	.	$\equiv n-n$
6	4	1C	1C	1C	1C.0	00.0	.	.	$\equiv n-n$
7	4	C1	CC	1C	C3.7	05.0	.	.	$\equiv n-n, \bullet \equiv n-14^{45} 19^{30} n, \bullet \equiv 0.2 14^{45} 19^{30}$
8	3	1C	1C	1C	1C.0	00.0	CC.4	.	$\equiv^{tr-2} n, \bullet 14^{40} 17^{10} n, \bullet \equiv 0.1 h-14^{45} \equiv 14^{45} n$
9	5	1C	1C	1C	1C.0	00.0	C1.7	.	$\equiv n-n, \bullet \equiv^{tr-2} n-10^{30} \equiv n-n-10^{30}, \bullet^{tr} 19^{45} n$
10	4	1C	1C	10	1C.0	00.0	CC.6	.	$\equiv^{tr-0.1} n-13^{30} \equiv n-n, \bullet \equiv 0.1 n-n, \bullet^{tr} 15^{15} n$
11	5	1C	C2	1C	C7.3	C1.6	CC.3	.	$\equiv n-n, \bullet \equiv n-9^{45}$
12	4	1C	1C	CC	C6.7	CC.1	.	.	$\equiv n-10^{45} \equiv 8^{15} 9^{45}$
13	4	10	01	CC	C3.7	C5.5	.	.	$\equiv n-8^{15} \equiv 8^{15} 10^{15} \equiv 10^{15} n$
14	3	C1	CC	C1	CC.7	C3.8	.	.	$\equiv n-9^{30} \equiv n-n-14 \equiv 0.9^{30} n$
15	3	1C	1C	CC	C5.3	CC.0	.	.	$\equiv n-19^{30} \equiv n-n, \bullet \equiv n-n, \bullet \equiv 19^{30} n$
16	4	1C	1C	10*	1C.0	CC.0	CC.0	.	$\equiv n-n, \bullet^{tr-1} n-14^{42}, \bullet^{tr-0.1} 14^{42} n$
17	6	C5	10	10	C5.7	CC.0	15.6	12	$\equiv n-n, \bullet^{tr} 18^{30} 19^{30} \equiv^{tr} 19^{30} n, \boxtimes$
18	4	10	1C	10	1C.0	CC.0	CC.0	11	$\equiv n-n, \bullet^{tr} 12^{02} 13^{30} \equiv 18^{15} n, \boxtimes$
19	2	1C	1C	1C	1C.0	CC.0	CC.5	C9	$\equiv n-15^{15} \equiv^{tr-0} 10^{00} 17^{30} \equiv 15^{15} n, \boxtimes$
20	3	1C*	1C	10	1C.0	CC.0	C3.1	06	$\equiv n-15^{15} \equiv n-n, \bullet^{tr} n-8^{15} \equiv^{tr} 8^{15} 13^{30}, \boxtimes$
21	4	10	1C	10	1C.0	CC.0	CC.6	C4	$\equiv n-10^{30} \equiv 0.2 n-12^{30} 17^{30} 18^{50} \equiv 8^{30} 9^{15}, \boxtimes$
22	4	1C	1C	1C	1C.0	CC.0	C1.3	03	$\equiv n-9^{45} \equiv 9^{45} n, \boxtimes$
23	6	10*	1C*	1C	1C.0	CC.0	CC.6	C1	$\equiv n-n, \bullet^{tr} n-14^{20} \equiv 0.1 17^{30} 9^{21} 14^{20} n$
24	5	1C*	1C*	1C*	1C.0	CC.0	C7.2	.	$\equiv n-n, \bullet^{tr-0.1} n-14^{40} 18^{15} n, \triangle 14^{40} 18^{15}$
25	7	1C	08	C1	C6.3	C1.5	CC.5	.	$\equiv n-12^{15} 16^{15} n$
26	6	CC	C3	C5	C2.7	C6.1	.	.	$\equiv n-n$
27	5	C2	1C	1C	C7.3	CC.4	.	.	$\equiv n-n, \bullet \equiv n-n$
28	5	C3	C1	CC	C1.3	C5.4	.	.	$\equiv n-n, \bullet \equiv n-n$
29	4	C2	CC	C1	C1.0	C7.3	.	.	$\equiv n-7^{30} 10^{15} n, \bullet \equiv 7^{30} 10^{15}$
30	4	10	05	10	C5.7	CC.3	.	.	$\equiv n-n, \bullet \equiv 8^{30} 10^{30}$
31	4	1C	C5	1C	C5.7	C4.6	.	.	$\equiv n-7^{30} 11^{30} n, \bullet \equiv 7^{30} 11^{30} \oplus 13^{15} 14^{30}$
MES.									
WRED.		C8.2	C7.8	C7.5	C8.0	42.0	38.1		

1	4	10	1C	1C	1C.0	CC.0	C3.5	.	$\equiv n-n, \bullet^{tr-0.1} n-9^{30} 12^{15} 14^{30}, \bullet^{tr} 9^{45} 12^{15}$
2	5	1C*	1C*	1C*	1C.0	CC.0	CC.1	C1	$\equiv n-n, \bullet^{tr} n-n, \boxtimes$
3	4	10	1C	1C	1C.0	CC.0	10.6	C2	$\equiv n-n, \bullet^{tr-0.1} n-11^{15}, \boxtimes$
4	3	10	1C	1C	1C.0	CC.0	CC.6	C1	$\equiv 0.1 n-n, \boxtimes$
5	5	10	CC	CC	C6.0	C3.4	.	.	$\equiv n-11^{45} \equiv 11^{45} n$
6	3	1C	CC	CC	C3.3	C3.2	.	.	$\equiv n-10^{15} \equiv n-n, \bullet \equiv 10^{25} 14^{30} \equiv 14^{30} n$
7	4	C7	C5	C1	C5.7	C1.6	.	.	$\equiv n-11^{30} \equiv 11^{30} n, \boxtimes$
8	5	C7	CC	CC	C4.3	C4.1	.	.	$\equiv n-n, \bullet \equiv n-8^{30} \equiv 7^{45} 9^{45}$
9	6	10	C5	1C	C5.7	C1.7	.	.	$\equiv n-7^{30} 10^{30} 13^{15} 17-n, \bullet \equiv 7^{30} 10^{30} \oplus 12^{15} 13^{30}$
10	5	C5	1C	1C	C5.7	CC.0	.	.	$\equiv 9^{30} 20^{30}, \bullet^{tr-1} 10^{11} 12^{45} 17^{16} n$
11	8	1C	07	1C	C5.0	C1.2	C5.7	.	$\equiv 7^{15} 9^{15} 16^{30} n, \bullet^{tr-1} n-8^{30} 19^{45} 20^{10} \oplus 20^{30} n$
12	6	CC	01	CC	CC.3	CC.6	.	.	$\equiv n-13^{45}$
13	7	C8	C5	1C	C5.0	CC.5	.	.	$\equiv n-9^{45}$
14	7	1C	1C	1C	1C.0	CC.0	.	.	$\equiv n-7^{45} 15^{30} n, \bullet^{tr-1} 15-n$
15	4	C8	1C	1C	C5.3	C1.3	CC.5	.	$\equiv 9^{15} n$
16	5	1C	1C	1C	1C.0	CC.6	.	.	$\equiv n-n, \bullet^{tr} n-n$
17	6	10	C5	1C	C5.7	CC.7	.	.	$\equiv n-n, \bullet^{tr} 7^{55} 8^{30}$
18	7	C2	C1	C1	C1.3	CC.6	CC.0	.	$\equiv n-10^{30} \equiv n-n-9^{15}$
19	6	CC	CC	CC	CC.0	CC.6	.	.	$\equiv n-n, \bullet \equiv n-10^{30}$
20	6	C2	05	05	C6.7	C2.6	.	.	$\equiv n-n, \bullet \equiv n-n$
21	7	C4	1C	1C	CC.0	CC.2	.	.	$\equiv n-12^{30} 17^{45} n, \bullet^{tr} 8^{45} 8^{50}$
22	5	1C	C5	1C	C5.7	CC.0	CC.0	.	$\equiv n-14^{30}, \bullet^{tr-0} 8^{15} 10^{30}$
23	8	1C	10	1C*	1C.0	C2.7	C3.6	.	$\equiv n-12^{30}, \bullet^{tr} n, 13^{12} 13^{19}, \bullet^{tr} 13^{02} 13^{12}, \bullet^{tr} 10^{30} n$
24	6	C7	C7	1C*	CC.0	C3.3	CC.1	.	$\equiv n-15^{15}, \bullet^{tr} n-n, 13^{01} 17^{10} 19^{30}, \bullet^{tr} 17^{22} 17^{58}, \bullet^{tr} 17^{58} n$
25	7	C1	C1	C6	C2.7	C5.8	C4.7	05	$\equiv 8^{15} 12^{30}, \bullet^{tr} 18^{45} 18^{45}, \boxtimes$
26	6	C1	C6	C1	C2.7	C9.2	CC.0	.	$\equiv n-10^{15}$
27	6	C1	C7	C3	C3.7	C7.2	.	.	$\equiv n-14^{15}$
28	8	C7	CC	CC	C3.0	CC.2	.	.	
MES.									
WRED.		C6.5	C7.1	C6.5	C6.8	64.0	50.2		

BR. ST. 57

$H_s = 157 \text{ m}$ $H_b = 162.5 \text{ m}$ $h_t = 6.0 \text{ m}$ $h_r = 2.0 \text{ m}$

Dan	Vrijest 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokrižak h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	8	C9	02	00	C3.7	C5.3	.	.	
2	8	C5	02	02	03.0	07.2	.	.	$\approx n-10^{45} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
3	8	10	02	00	04.0	C7.1	.	.	$\approx n-11^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
4	6	10	10	10	10.0	C1.3	.	.	$\approx 7^{45} 13^{30}$
5	6	10	09	00	06.3	00.4	.	.	$\approx n-13^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
6	5	00	09	01	03.3	05.6	00.0	.	$\approx n-9^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
7	4	09	10	10	09.7	C1.6	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
8	6	10	10	10	10.0	00.0	C1.3	.	$\approx n-13^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
9	4	10	10*	10	10.0	00.0	00.3	.	$\approx n-15^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
10	6	06	10	10	08.7	02.4	02.8	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
11	6	10	10	00	06.7	C1.8	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
12	6	01	02	01	01.3	09.2	.	.	$\approx n-13^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
13	6	10	10	10*	10.0	00.0	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
14	5	10*	10	10*	10.0	00.0	C2.1	03	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
15	5	10*	09	10	09.7	00.1	C3.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
16	6	10	10	08	09.3	00.0	00.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
17	6	00	06	00	02.0	06.5	00.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
18	6	04	10	09	07.7	C1.7	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
19	7	02	09	00	03.7	05.4	.	.	$\approx n-18^{45} \approx 8^{45} 11^{45}$
20	7	04	09	00	04.3	06.6	.	.	$\approx n-9^{45} \approx 8^{45} 11^{45}$
21	7	C5	08	00	04.3	C8.9	.	.	$\approx n-12^{45}$
22	6	00	00	00	00.0	C9.8	.	.	$\approx n-14^{45}$
23	6	00	00	00	00.0	C9.8	.	.	$\approx n-13^{30} 18^{45}$
24	6	03	08	10	07.0	C7.4	.	.	$\approx n-14^{45} 17^{45}$
25	7	10	08	06	08.0	04.0	.	.	$\approx n-r_j \oplus 10-11$
26	7	10	08	08	06.7	01.2	.	.	$\approx n-12^{30}$
27	7	C1	06	07	04.7	C7.2	.	.	$\approx n-12^{45}$
28	6	C2	10	09	07.0	C5.0	.	.	$\approx n-18^{45}$
29	6	10	10	10	10.0	00.0	00.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
30	7	10	10	10	10.0	00.8	C1.8	.	$\approx n-10^{45} 17^{30}$
31	6	00	02	08	03.3	10.2	.	.	$\approx n-13^{30} 18^{45}$
MES.									
WRED.		06.2	07.4	05.4	06.3	126.5	11.3		

1	5	C9	04	00	04.3	07.6	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
2	7	00	10	00	03.3	05.0	.	.	$\approx n-17^{30} 9^{30} 12^{45} \approx 7^{45} 9^{30} \oplus 10^{30} 13^{30} F_{SW} 15^{30} 16$
3	5	10	10	10	10.0	00.0	00.0	.	$\approx n-15^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
4	8	10	10	10	10.0	00.0	11.3	.	$F_{NNE} n$
5	8	09	01	00	03.3	05.5	.	.	$F_{NNW} 7^{45} 10^{30}$
6	8	01	00	00	00.3	09.7	.	.	$\approx n-8^{45}$
7	8	09	04	02	05.0	09.0	.	.	$\approx n-8^{45} \oplus 8^{30} 13^{30}$
8	6	10	10	10	10.0	00.0	C1.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
9	6	10	10	10	10.0	00.6	03.6	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
10	9	10	02	05	05.7	06.5	00.0	.	$\approx n-9^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
11	8	09	09	03	07.0	01.5	C1.3	.	$\approx n-12^{15} \oplus 6^{45} 12^{45} \oplus 14^{20} 17^{15} n$
12	8	04	10	10	08.0	01.5	C0.3	.	$\approx n-12^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
13	6	10	10	08	09.3	00.6	C7.7	.	$\approx n-12^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
14	7	08	10	10	09.3	00.3	00.3	.	$\approx n-13^{30} 17^{30}$
15	6	08	08	10	08.7	03.1	C1.7	.	$\approx n-13^{30} 17^{30}$
16	6	10	10	01	07.0	00.3	C2.5	.	$\approx n-13^{15} 18^{30} n \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
17	6	00	09	09	06.0	C9.3	00.2	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
18	6	09	09	10	05.3	01.0	.	.	$\approx n-14^{45} 18^{30} n \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
19	7	08	10	10	09.3	03.3	00.0	.	$\approx n-12^{30} 15^{30} n \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
20	6	10	10	10	10.0	00.0	05.5	.	$\approx n-14^{30} \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
21	7	10	10	03	07.7	00.0	12.7	.	$\approx n-11^{45} 18^{30} n \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
22	6	C1	05	01	02.3	08.5	C1.9	.	$\approx n-8^{45} F_{WNN} 12^{30} 12^{50} \oplus 14^{20} 17^{15} n$
23	7	C3	10	10	07.7	06.2	C0.3	.	$\approx n-8^{45} \oplus 9^{30} 13^{30}$
24	5	10	10	10	10.0	00.0	04.2	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
25	5	10	10	10	10.0	00.0	19.6	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
26	5	09	04	00	04.3	07.7	07.2	.	$\approx n-14^{30} 18^{30} n$
27	5	00	03	01	01.3	07.9	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
28	7	C4	04	03	03.7	10.7	.	.	$\approx n-9^{30} F_{WSW} 16-17$
29	7	09	07	04	06.7	02.7	.	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
30	7	C1	08	05	04.7	11.8	00.0	.	$\approx n-r_j \cdot n-r_j \oplus 7^{45} 10^{45} \approx 8^{30} 9^{45}$
MES.									
WRED.		C7.0	07.6	05.8	C6.8	126.9	81.3		

BA. ST. 57

$H_g = 157 \text{ m}$ $H_b = 162.5 \text{ m}$ $h_t = 6.0 \text{ m}$ $h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	7	C1⊙	07⊙	C0	02.7	12.0	.	.	= n-11 ¹⁵
2	7	10	05⊙	C8	05.0	05.1	.	.	F _{WSW} 12 ²⁰ 17 ¹⁵ • tr 20 ²³
3	7	09	05⊙	00	06.0	05.9	00.0	.	• 09 ⁴⁵ 9 ³⁰ F _{WSW} 13 ⁵⁰ 18 ⁴⁰
4	8	C4⊙	10	C6	06.7	07.7	00.1	.	= n-10 ⁴⁵ • 10 ⁴⁵ 13 ³⁰
5	8	09	06⊙	03	06.7	06.9	.	.	.
6	8	05⊙	10	10	06.3	06.9	.	.	• tr 20 ⁴⁵
7	8	01⊙	03⊙	00	01.3	11.9	00.0	.	= n-7 ⁴⁵
8	8	04⊙	C5⊙	C9	06.0	12.1	.	.	.
9	8	10	07⊙	01	06.0	03.6	.	.	• 16 ⁰² 16 ²⁰
10	8	C1⊙	04⊙	C0	01.7	12.5	00.3	.	.
11	8	03⊙	03⊙	10	05.3	09.1	.	.	• tr 19 ⁴³ 20 ³⁰
12	7	10	10	C0	06.7	00.2	00.5	.	• tr 7 ¹⁵ 8 ³⁰ = 13 ³⁰ n
13	8	02⊙	C1⊙	02	01.7	13.0	00.0	.	= n-8
14	8	00⊙	06⊙	C2	03.3	11.8	.	.	= n-9 ³⁰ • 16 ⁴⁵ 18 ⁴⁵
15	8	09⊙	C6⊙	10	06.3	07.2	.	.	= n-8 ³⁰ 13 ¹² 18 ⁴² 19 ²⁰ • tr 19 ⁰² n; • 19 ¹³ 20 ³⁰
16	7	10	10	10	10.0	00.0	15.8	.	= n-10 ⁴⁵ • tr 7 ⁰³
17	7	07⊙	06⊙	C8	07.0	08.9	00.0	.	= n-8 ³⁰
18	7	08⊙	10	C8	06.7	01.4	.	.	= n-12 ³⁰
19	7	00⊙	06⊙	10	05.3	10.1	.	.	= n-10 ⁴⁵ 16 ⁴⁵ n
20	8	C5	C6⊙	C8	07.7	10.2	.	.	.
21	8	07⊙	09⊙	10	06.7	05.0	.	.	F _{WSW} 13-13 ⁴⁵
22	8	C2⊙	03⊙	C4	03.0	12.8	.	.	.
23	8	C8⊙	C5⊙	05	06.0	08.8	.	.	• 10 ³⁰ 11 ¹⁵
24	7	10	09⊙	10	09.7	05.8	.	.	• tr 19 ⁰² n
25	7	10	07	08	06.3	03.6	01.2	.	= n-7 ⁴⁵ • tr 8-10 ⁰⁵ 14 ⁴⁵ 15 ¹⁷ • 10 ⁰⁵ 10 ¹² 13 ²⁷
26	8	C8⊙	09	C0	05.7	06.1	00.1	.	= n-8
27	8	00⊙	03⊙	C3	02.0	12.2	.	.	.
28	7	00⊙	07⊙	00	02.3	11.4	.	.	= n-8 ⁴⁵
29	7	00⊙	C6⊙	C1	02.3	11.6	.	.	= n-8 ³⁰
30	7	09	10	C8	09.0	02.4	.	.	= n-8 ⁴⁵ • tr 13 ¹⁰ • tr 13 ²⁵ 17 ⁴⁰ 18 ⁰⁰ 14 ³⁶ 16 ⁵⁰
31	8	C5⊙	C9⊙	C3	07.0	03.5	01.9	.	= n-7 ⁴⁵ • tr 7 ³⁰
MES.									
MED.		05.6	06.9	05.1	05.9	239.7	24.3		

ZAGREB GRIC

1973 JUN

1	7	C0⊙	04⊙	C2	02.0	09.5	.	.	= n-10 ³⁰ 19 ³⁰ n; • n-9 ¹⁵
2	7	C2⊙	10	C8	06.7	08.0	.	.	.
3	7	08⊙	09⊙	10	09.0	03.2	00.6	.	= 8 ¹⁵ 12 ³⁰ • tr 0-6 ³⁰ 9 ²² 9 ³⁷
4	7	10	10	C7	09.0	00.1	00.0	.	= n-10 ³⁰ • tr 0-13 ⁴² 14 ⁵⁵
5	7	09	C6⊙	C5	07.3	04.3	00.4	.	= n-11 ³⁰
6	6	10	10	10	10.0	00.6	00.0	.	= n-7 ⁴⁵ • tr 1-2 n; 14 ³⁴ n; 15 ¹⁵ • 1-2 14 ⁵⁶ 15 ¹¹
7	7	10	10	10	10.0	00.3	00.1	.	= n-11 ³⁰ 16-17 F _{WSW} 19 ⁵⁷ 20 ⁰² 18 ⁰⁰ 21 ³⁰ 22 ²⁰ • 02 ¹³ 22 ¹⁵
8	7	10	C5⊙	10	09.7	01.4	03.8	.	= 9-10 ¹⁵ 19 ³⁵ n; • tr 0-7 ¹⁵ 8 ²⁰
9	6	C9	09	C8	06.7	00.7	00.1	.	= n-7 ⁴⁵ • tr 0-16 ⁴⁰ n
10	7	C9	07⊙	C1	05.7	06.2	00.5	.	= n-9 ¹⁵
11	7	10	08⊙	C2	06.7	04.6	00.2	.	= n-11 ³⁰ • n
12	6	10	C8⊙	C0	06.0	03.4	.	.	= n-13 ³⁰
13	7	C6	04⊙	C2	04.7	10.6	.	.	= n-9 ⁴⁵ 19 ³⁰ n
14	5	C2	09	10	07.0	02.5	.	.	= n-14 ⁴⁵ 18 ³⁰ n; 18 ⁰⁶ 8 ⁴⁵ 12 ⁴² 16 ³⁰ • 0-12 ⁵² 15 ³⁰ n
15	8	C0⊙	C6⊙	C1	02.3	13.8	00.4	.	.
16	8	C9	C6⊙	C6	07.7	02.3	.	.	.
17	8	C9	08⊙	C5	06.7	07.6	.	.	= n-7 ⁴⁵ 19 ¹⁵ n; • 10 ³⁰ 12 ³⁰
18	6	C8⊙	10	C8	08.7	00.7	.	.	= n-7 ⁴⁵ • tr 0-8 ⁴⁵ 11 ³⁰ 12 ¹² 14 ³⁴
19	8	C0⊙	C9	C8	05.7	09.4	00.0	.	= n-8 ⁴⁵
20	8	C8⊙	C0⊙	C9	04.3	09.8	.	.	= n-9 ⁴⁵
21	5	C9	10	10	09.7	00.0	00.1	.	= n-7 ⁴⁵ • tr 1-2 n; 12 ⁴⁵ 13 ²⁰ 18 ⁰⁰ 8 ²⁰ 9 ³⁰ • 0-18 ⁴⁰ 9 ²⁰ 13 ²⁵ n
22	5	10	10	10	10.0	00.1	04.6	.	= n-7 ⁴⁵ • tr 1-2 n; 12 ⁴⁵ 13 ²⁰ 18 ⁰⁰ 8 ²⁰ 9 ³⁰ • 0-18 ⁴⁰ 9 ²⁰ 13 ²⁵ n
23	8	10	04⊙	C6	07.3	08.8	11.5	.	= n-8 ⁴⁵ • n
24	8	10	10	10	10.0	00.0	03.4	.	• tr 0-1 n; n; 15-17
25	7	C5	09⊙	C8	07.3	05.1	10.9	.	= n-10 ¹⁵ • 11 ¹⁷ 12 ³⁰
26	5	C4⊙	05⊙	C0	03.0	09.5	00.1	.	= n-13 ¹⁵
27	7	C0⊙	C0⊙	C0	00.0	13.2	.	.	= n-10 ¹⁵ 18 ⁴⁵
28	7	C0⊙	03⊙	C1	01.3	10.2	.	.	= n-10 ¹⁵ 18 ⁴⁵ n
29	7	C0⊙	02⊙	C5	02.3	10.0	.	.	= n-12 ³⁰ 18 ³⁰ 19 ¹⁵ F _{WSW} 14 ⁴³ n; 18 ³⁸ 19 ¹⁵ • 0-18 ³⁸ 19 ³⁰ • 2 18 ⁴⁵ 19 ⁰²
30	8	C9	C9	C7	08.3	05.7	07.4	.	F _{WSW} 14 ⁴⁵ • 15 ²⁵ = 18 ³⁰ n
MES.									
MED.		06.6	07.3	06.0	06.6	161.6	74.5		

Dan	Vrijnost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavina R mm	Snežni pokriivač h cm	Razvoj vremena w
		14	7	14	21				
1	6	10	10	10	10.0	02.5	.	.	$= 8^{30} - 18^{30}$
2	6	09	07	04	06.7	06.1	.	.	$= n - 13^{30} - 17^{30} - n$
3	7	02	03	07	04.0	09.1	.	.	$= n - 12^{15}$
4	7	00	07	00	02.3	08.5	.	.	
5	7	09	05	06	06.7	08.6	.	.	$= n - 12^{30}, R^{+2} 21^{40}, n, \nabla 21^{52} - n$
6	6	00	00	04	01.3	08.7	08.0	.	$= n - n$
7	5	02	06	06	04.7	05.6	.	.	$= n - 18^{15}, R^{0-1} 11 - 16^{45}, \nabla tr^{-1} 12^{02} - 12^{20}, 15^{22} - 16^{30},$
8	7	10	04	01	05.0	05.1	00.2	.	$= n - 10^{51}$
9	6	04	04	09	05.7	07.1	.	.	$= n - n$
10	7	10	08	03	07.0	04.2	00.0	.	$= n - n, \bullet tr^{-0} n$
11	6	01	01	04	02.0	11.1	.	.	$= n - 10^{30}$
12	7	07	06	03	05.3	05.4	.	.	$= n - 10^{30}$
13	6	10	10	02	07.3	03.1	01.1	.	$= n - 16^{45}, \bullet tr^{-0-1} n - 13^{40},$
14	7	00	09	02	03.7	06.6	03.7	.	$= n - 12^{15}, 15^{30} - n, \bullet tr^{-0} 18^{38} - 18^{54}, \nabla 18^{54} - 19^{06}$
15	6	01	04	05	03.3	07.4	00.0	.	$= n - 13^{45}, \bullet 0-1 10^{55} - 12^{10}, F 86, 12^{37} - 19^{15},$
16	7	09	03	03	05.0	07.0	00.1	.	$= n - 17^{30} F NE - 6 13^{15} - 19^{45}$
17	8	00	01	00	00.3	13.0	.	.	$\nabla tr^{-1} 16^{02} 17^{15}, R^{0-1} 17 - 17^{15}$
18	8	00	09	06	05.0	09.8	.	.	$= n - 8^{30} 18^{15}, n, R^{0-2} 17^{20} - 20^{15}, \nabla 2 18^{32} - 19^{45}, \bullet tr 19^{45} n$
19	8	07	01	10	06.0	09.1	01.2	.	$= n - 8^{36}$
20	8	00	01	02	01.0	13.4	14.6	.	
21	7	01	01	02	01.3	13.4	.	.	$= n - 9^{30}$
22	7	03	07	09	06.3	08.4	.	.	$= n - 7^{45}, R^{+2} 8^{30} n, \nabla 18^{30} - 8^{45}$
23	6	03	06	00	03.0	11.6	21.3	.	
24	7	00	10	10	06.7	05.6	.	.	$= n - 7^{30} 14^{30} n; \oplus 10^{30} 11^{30}, R^{+2} 12^{42}, 17, \nabla^{+2} 13^{00} - n$
25	8	00	10	10	06.7	07.3	24.3	.	$= n - 12^{15}$
26	6	09	09	03	07.0	04.5	.	.	$= n - 9^{30} 12^{15} 16^{45}, \nabla tr^{-1} 12^{22} 17^{15}, R^{0-1} 12^{42} 17$
27	8	07	10	03	06.7	06.8	00.5	.	$= n - 7^{30} \nabla tr^{-1} 12^{30} 14^{25}, R^{0-1} 13^{00} 14, F 13^{38} - 13^{50}$
28	8	04	08	02	04.7	08.7	00.3	.	$= n - 8^{30},$
29	5	10	10	01	07.0	00.9	.	.	$= 11^{45} 18^{45}, \bullet tr^{-0} 12^{04} 13^{45}$
30	7	09	09	10	05.3	04.5	01.1	.	$= n - 12^{30}, \nabla tr^{-2} 13^{25} - 14^{45}, 18^{16} - 20^{30},$
31	7	03	07	02	04.0	05.3	05.4	.	$= n - 12^{15}, 18^{45} n$
MES.									
VRED.	04.5	06.0	04.5	05.0	229.1	01.8			

1	6	C00	030	0C	C1.C	12.6	.	.	$= n-13^{15} 19^{30} n; \Delta^1 n-rj$
2	6	000	030	C7	C3.3	C8.4	.	.	$= n-16^{18} 19^{30} n; \Delta^1 n-rj; R^2 15^{24} 15^{54} \nabla 0^{15} 32^{15} 55 \bullet +r-0^{15} 55^{18} 15;$
3	6	C9	1C0	1C	C9.7	C2.C	C1.3	.	$= n-n; \bullet +r-0-2^{17} 44^{30} 14^{15} 16^{30} \nabla +r-0-\Delta 12^{30} 14^{15} R^2 0-1^{11} 30-16^{15}$
4	5	10	080	C7	C8.3	03.C	C7.C	.	$= n-n; \nabla +r-1^{17} 27^{9} 15; R^2 0-1^{17} 45^{9} 15 14^{45} 17^{45}; \bullet +r-0^{13} 25^{17} 30$
5	6	000	060	C2	C2.7	C9.3	C1.7	.	$= n-n; \Delta^1 n-rj$
6	6	C00	020	00	0C.7	12.5	.	.	$= n-n; \Delta^0 n-rj$
7	8	CC0	CC0	CC	CC.C	11.6	.	.	$= n-10^{30} \Delta^1 n-rj$
8	8	08	070	00	C5.C	C4.3	.	.	$= n-9^{30} \Delta^0 n-rj$
9	8	CC0	010	00	0C.3	12.8	.	.	$= n-9^{30} \Delta^0 n-rj$
10	7	000	C10	0C	0C.3	12.6	.	.	$= n-14^{45} \Delta^0 n-rj$
11	7	CC0	0C0	CC	CC.C	12.9	.	.	$= n-15^{30} \bullet +r-1^{54} 6^{15} 9^{50} 10$
12	6	10	040	00	04.7	C7.4	CC.C	.	$= n-n$
13	6	000	010	C5	02.C	09.3	CC.C	.	$= n-7^{45}$
14	7	C10	C40	00	C1.7	11.8	.	.	$= n-13^{30} 17^{45} n$
15	6	C00	050	0C	01.7	11.4	.	.	$= n-12^{30} 18^{15} n$
16	7	000	080	0C	C2.7	10.C	.	.	$= n-13^{30}$
17	6	CC0	CC0	0C	CC.0	12.4	.	.	$= n-12^{30}$
18	7	0C0	0C0	C1	CC.3	12.5	.	.	$= n-14^{45} 18^{15} n; R^2 19^{45} 20^{30} \bullet +r-20^{30}$
19	5	CC0	010	01	0C.7	11.7	.	.	$= n-13^{30} 16^{45} n; \bullet 18^{30} 18^{39} n; \nabla 0-2^{20} 05^{20} 55^{15} R^2 120^{42} 20^{50}$
20	7	CC0	050	C2	C4.3	C8.8	.	.	$= n-n$
21	6	CE	C80	1C	C8.7	C3.6	CC.C	.	$= n-n$
22	5	1C	1C	1C	1C.0	0C.1	C2.5	.	$= n-n; R^2 18^{28} 18^{40}; \bullet 0-1-2^{18} 28^{18} 50^{15} \nabla 18^{30} 18^{40}$
23	6	10	1C	1C	1C.0	00.C	.	.	$= n-n$
24	6	CE	0C0	C2	C3.3	C9.2	.	.	$= n-n$
25	6	CE	0C0	09	C7.7	C4.4	C3.7	.	$= n-n$
26	6	10	1C	1C	1C.C	00.C	.	.	$= n-n$
27	7	1C	1C	1C	1C.0	01.5	.	.	$= n-11^{30} R^2 16^{15}$
28	6	10	1C	1C	1C.C	00.C	CC.1	.	$= n-n; \bullet +r-0-1^{11} 14^{45} n$
29	6	10	1C	10	1C.C	00.C	1C.4	.	$= n-n; \bullet 0-1^{11} n$
30	5	1C	C70	C1	C6.C	C3.3	.	.	$= n-n$
31	5	000	C5	1C	06.3	01.8	.	.	$\Delta^1 n-rj; \equiv^0 n-10^{30} = 10^{30} n$

BR. ST. 57

 $H_s = 157 \text{ m}$ $H_b = 162.5 \text{ m}$ $h_t = 6.0 \text{ m}$ $h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	7	10	04	01	05.0	05.7	.	.	.	$\approx n-9^{45}$
2	7	00	03	00	01.0	11.4	.	.	.	$\approx n-11^{45}$
3	7	00	00	00	00.0	11.6	.	.	.	$\approx n-11^{45}$
4	7	00	00	00	00.0	11.8	.	.	.	$\approx n-12^{45}$
5	7	00	00	00	00.0	11.8	.	.	.	$\approx n-12^{45}$
6	7	00	01	00	00.3	11.2	.	.	.	$\approx n-14^{45}$
7	7	01	00	00	00.3	11.0	.	.	.	$\approx n-14^{45}$
8	7	00	00	00	00.0	10.5	.	.	.	$\approx n-15^{45}$
9	6	01	01	01	01.0	10.2	.	.	.	$\approx n-15^{45}$
10	6	01	05	10	06.7	04.6	.	.	.	$\approx n-15^{45}$
11	8	00	06	09	07.7	07.2	06.5	.	.	$\approx n-17^{45}$
12	7	00	03	00	01.0	10.3	.	.	.	$\approx n-17^{45}$
13	6	00	01	01	00.7	09.6	.	.	.	$\approx n-17^{45}$
14	6	00	00	00	00.0	10.1	.	.	.	$\approx n-17^{45}$
15	6	00	10	00	03.3	02.3	.	.	.	$\approx n-17^{45}$
16	5	00	07	05	04.0	08.2	00.0	.	.	$\approx n-17^{45}$
17	3	10	10	10	10.0	00.0	01.9	.	.	$\approx n-17^{45}$
18	6	06	10	10	08.7	01.3	09.6	.	.	$\approx n-17^{45}$
19	6	10	10	10	10.0	00.0	34.9	.	.	$\approx n-17^{45}$
20	6	10	03	00	04.3	03.2	01.3	.	.	$\approx n-17^{45}$
21	7	01	05	00	02.0	06.6	.	.	.	$\approx n-17^{45}$
22	7	10	10	01	07.0	00.0	02.9	.	.	$\approx n-17^{45}$
23	7	10	05	00	06.3	03.1	07.5	.	.	$\approx n-17^{45}$
24	5	10	05	10	05.7	02.0	00.1	.	.	$\approx n-17^{45}$
25	7	10	10	10	10.0	00.0	00.0	.	.	$\approx n-17^{45}$
26	6	10	10	10	10.0	00.0	18.1	.	.	$\approx n-17^{45}$
27	5	10	10	10	10.0	00.0	01.7	.	.	$\approx n-17^{45}$
28	5	06	04	00	03.3	05.1	12.6	.	.	$\approx n-17^{45}$
29	5	10	00	00	03.3	07.8	.	.	.	$\approx n-17^{45}$
30	7	01	04	10	05.0	04.5	.	.	.	$\approx n-17^{45}$
PES.										
WRED.		04.5	05.0	03.6	04.4	181.1	57.1			

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1973 OKTOBAR

1	6	10	10	10	10.0	00.0	01.0	.	.	$\approx n-n$
2	6	10	10	10	10.0	00.0	.	.	.	$\approx n-n$
3	5	10	10	10	10.0	00.0	.	.	.	$\approx n-n$
4	5	10	07	10	05.0	01.1	.	.	.	$\approx n-n$
5	6	00	01	00	00.3	08.9	.	.	.	$\approx n-15^{45}$
6	6	00	01	00	00.3	09.0	.	.	.	$\approx n-14^{45}$
7	5	00	00	01	00.3	08.4	.	.	.	$\approx n-14^{45}$
8	6	10	10	10	10.0	00.2	.	.	.	$\approx n-14^{45}$
9	6	08	01	00	03.0	07.3	03.8	.	.	$\approx n-14^{45}$
10	6	00	00	00	00.0	08.0	.	.	.	$\approx n-14^{45}$
11	5	02	06	00	02.7	05.6	.	.	.	$\approx n-14^{45}$
12	8	10	10	10	10.0	00.2	00.0	.	.	$\approx n-14^{45}$
13	8	10	10	10	10.0	00.0	06.6	.	.	$\approx n-14^{45}$
14	6	10	07	10	05.0	03.0	00.0	.	.	$\approx n-14^{45}$
15	7	10	09	01	06.7	01.3	00.6	.	.	$\approx n-14^{45}$
16	6	09	10	06	09.0	00.3	00.2	.	.	$\approx n-14^{45}$
17	8	00	02	00	00.7	09.0	03.2	.	.	$\approx n-14^{45}$
18	7	09	10	10	09.7	03.6	.	.	.	$\approx n-14^{45}$
19	7	01	00	00	00.3	09.2	.	.	.	$\approx n-14^{45}$
20	5	10	10	10	10.0	00.1	.	.	.	$\approx n-14^{45}$
21	5	10	10	09	09.7	00.1	00.0	.	.	$\approx n-14^{45}$
22	5	07	04	00	03.7	05.0	01.8	.	.	$\approx n-14^{45}$
23	8	03	05	05	05.7	06.2	.	.	.	$\approx n-14^{45}$
24	8	09	04	02	05.0	07.8	00.1	.	.	$\approx n-14^{45}$
25	7	00	00	00	00.0	08.8	.	.	.	$\approx n-14^{45}$
26	6	05	04	00	03.0	06.1	.	.	.	$\approx n-14^{45}$
27	5	10	05	00	05.0	07.6	.	.	.	$\approx n-14^{45}$
28	6	00	00	00	00.0	07.7	.	.	.	$\approx n-14^{45}$
29	5	10	07	02	06.3	06.3	.	.	.	$\approx n-14^{45}$
30	5	08	07	10	06.3	04.0	.	.	.	$\approx n-14^{45}$
31	5	08	07	05	06.0	03.7	.	.	.	$\approx n-14^{45}$
PES.										
WRED.		06.4	05.8	04.7	05.7	138.5	17.6			

BR. ST. 57

$H_s = 157 \text{ m}$ $H_b = 162.5 \text{ m}$ $h_t = 6.0 \text{ m}$ $h_r = 2.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insekcija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21				
1	8	C3	01	00	C1.3	C8.7	.	.	$\equiv n-9^{30}$
2	6	C0	00	C1	C0.3	C8.3	.	.	$\equiv n-n, \angle n-r, \angle$
3	7	C0	01	00	C0.3	C8.1	.	.	$\equiv n-n, \angle n-r, \angle \equiv 07^{45} 9^{45}$
4	5	C1	00	C9	C3.3	C7.6	.	.	$\equiv n-n, \angle n-r, \angle$
5	8	09	03	09	07.0	04.2	.	.	$\equiv n-9^{45}$
6	8	10	10	10	10.0	00.6	.	.	$\equiv n-9^{45}$
7	6	10	10	10	06.7	00.0	26.4	06	$\equiv n-9^{45}$
8	5	10	10	10	10.0	C3.1	C0.2	.	$\equiv n-9^{45}$
9	3	10	09	10	09.7	00.2	.	.	$\equiv n-9^{45}$
10	5	09	00	00	03.0	07.7	C0.7	.	$\equiv n-n$
11	3	10	00	00	C3.3	05.6	.	.	$\equiv n-9^{45}$
12	4	09	07	C0	C5.3	C0.4	.	.	$\equiv n-9^{45}$
13	5	07	09	10	08.7	01.0	.	.	$\equiv n-9^{45}$
14	4	10	10	09	09.7	C0.0	C0.1	.	$\equiv n-9^{45}$
15	5	10	10	01	07.0	00.3	C8.6	.	$\equiv n-9^{45}$
16	6	10	09	01	06.7	00.5	C0.0	.	$\equiv n-9^{45}$
17	7	09	08	01	06.0	01.6	.	.	$\equiv n-9^{45}$
18	7	10	04	C1	C5.0	02.2	.	.	$\equiv n-9^{45}$
19	6	01	01	00	C0.7	07.6	.	.	$\equiv n-9^{45}$
20	6	C8	01	C1	03.3	C5.7	.	.	$\equiv n-9^{45}$
21	6	00	00	00	00.0	07.7	.	.	$\equiv n-9^{45}$
22	6	00	01	02	01.0	C5.5	.	.	$\equiv n-9^{45}$
23	7	00	09	00	C3.0	04.7	.	.	$\equiv n-9^{45}$
24	6	10	06	C1	05.7	C1.5	.	.	$\equiv n-9^{45}$
25	5	10	10	09	09.7	00.0	.	.	$\equiv n-9^{45}$
26	4	10	10	10	10.0	00.0	C1.3	.	$\equiv n-9^{45}$
27	6	10	10	10	10.0	C1.4	16.5	.	$\equiv n-9^{45}$
28	6	10	09	10	09.7	00.5	.	.	$\equiv n-9^{45}$
29	6	10	10	10	10.0	00.0	.	.	$\equiv n-9^{45}$
30	8	00	01	00	00.3	08.4	01.3	04	$\equiv n-9^{45}$
MES.									
WRED.		C6.9	05.6	04.2	05.6	103.5	55.5		

1	6	02	C0	C1	01.0	06.4	.	03	$\equiv n-n$
2	5	00	04	00	C1.3	C3.0	.	03	$\equiv n-n$
3	5	00	C0	00	00.0	07.4	C0.0	03	$\equiv n-n$
4	5	00	08	C8	C5.3	00.1	.	02	$\equiv n-n$
5	4	02	09	09	06.7	C2.2	.	02	$\equiv n-n$
6	5	01	C2	00	C1.0	07.1	.	02	$\equiv n-n$
7	6	01	08	00	C3.0	03.4	.	.	$\equiv n-n$
8	4	10	10	10	10.0	00.5	.	.	$\equiv n-n$
9	8	10	10	01	C7.0	00.0	C8.5	.	$\equiv n-n$
10	6	C7	01	C0	02.7	C7.4	C6.1	.	$\equiv n-n$
11	6	00	C0	C0	02.0	04.0	.	.	$\equiv n-n$
12	6	C3	08	C1	04.0	00.7	.	.	$\equiv n-n$
13	5	10	08	00	C0.0	C1.2	.	.	$\equiv n-n$
14	6	C5	08	10	C7.7	01.3	.	.	$\equiv n-n$
15	8	10	07	00	C5.7	02.6	08.2	.	$\equiv n-n$
16	7	C1	10	C7	C6.0	C1.8	.	.	$\equiv n-n$
17	8	10	10	10	10.0	00.0	.	.	$\equiv n-n$
18	8	10	10	10	10.0	C0.2	02.0	.	$\equiv n-n$
19	3	10	10	08	C5.3	C0.0	C0.0	.	$\equiv n-n$
20	6	10	06	C8	08.0	04.8	C0.3	.	$\equiv n-n$
21	7	03	10	10	07.7	C3.0	.	.	$\equiv n-n$
22	7	10	07	C0	C5.7	03.6	00.1	.	$\equiv n-n$
23	7	08	C5	C2	C6.3	C0.1	C0.0	.	$\equiv n-n$
24	7	10	09	10	09.7	00.9	.	.	$\equiv n-n$
25	6	10	10	10	10.0	C1.1	C0.0	.	$\equiv n-n$
26	6	C5	10	10	09.7	C0.0	13.5	.	$\equiv n-n$
27	5	10	10	10	10.0	C0.2	C3.8	.	$\equiv n-n$
28	5	10	10	10	10.0	C0.0	.	.	$\equiv n-n$
29	5	10	10	10	10.0	C0.0	C0.0	.	$\equiv n-n$
30	5	10	10	10	10.0	C0.0	C0.0	.	$\equiv n-n$
31	5	10	10	10	10.0	00.0	.	.	$\equiv n-n$
MES.									
WRED.		C6.5	C7.7	05.6	C6.6	63.0	42.5		

BR. ST.89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Validnost 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	8	1C●	1C	10●	1C.0	00.0	07.8	.	● 0-16 ³⁰ 17 ³⁰ 15 ³⁰ -24; F E ENE 6 ³⁰ 12 ³⁰ F E ESE 13 ⁵⁵ 17
2	7	1C	1C●	1C	1C.0	00.0	13.1	.	● 0-10-16 ³⁰ F ESE 0-10 ⁴⁵ 17 ⁴⁵ 23 ³⁰
3	8	09	09	10	05.3	00.9	09.1	.	● 0-17 ⁴⁰ 23 ⁵⁵
4	8	10	05	04	07.7	03.1	02.3	.	F NNE 20 ⁰⁵ 23 ⁵⁰
5	8	09	09○	02	06.7	01.1	.	.	F NNE 2-23 ³⁰
6	8	09	06○	00	05.0	06.2	.	.	F NE 19-21 ⁰⁵
7	8	00	01○	00	00.3	08.0	.	.	.
8	8	00	00○	00	00.0	08.4	.	.	.
9	8	00	00○	00	00.0	08.4	.	.	.
10	8	01	00○	00	00.3	07.8	.	.	.
11	8	06	02○	00	02.7	07.6	.	.	F NNE 20 ⁴⁵ 24
12	8	00	00○	00	00.0	08.2	.	.	F NNE 0-10 ⁵⁰ 21 ⁵⁰ 23 ³⁵
13	8	00	00○	00	00.0	08.4	.	.	F NNE-NE 10 ⁵
14	8	00	00○	09	03.0	08.6	.	.	.
15	8	10	05	10	05.7	00.2	.	.	.
16	7	10	1C●	01	07.0	00.0	00.5	.	● 0-13 ³⁰ 14 ³⁰ 9 ⁰⁵ 19 ³⁰ ; F E ESE-E 6 ⁰⁶ 17
17	8	09	09	10	05.3	02.0	18.0	.	● 14 ⁰⁹ 14 ²⁰ 11 ²⁰ F ESE 19 ³⁰ 24
18	6	10●	10●	10	10.0	00.0	04.3	.	F ESE 0-14 ³⁰ ; ● 0-15 ⁴⁵ 15 ⁴⁵ 19 ³⁰ 20 ⁴⁰
19	8	01	05	10	06.7	05.2	14.4	.	● 14 ⁰⁸ 16 ³⁰
20	8	10	10	08	05.3	00.0	09.7	.	● 0-17 ³⁵ 10 ⁵⁰ 14 ⁰² 18 ³⁰ ; F ESE-E 7 ¹² 8 ⁴⁵
21	8	02	06○	00	02.7	06.4	04.8	.	● 0-17 ³⁵ 10 ⁵⁰ 14 ⁰² 18 ³⁰ ; F ESE-E 7 ¹² 8 ⁴⁵
22	8	09	09○	10	05.3	00.8	00.2	.	F E-ESE 12-24; ● 21 ³⁰ 24
23	8	09	10	10●	05.7	00.0	08.2	.	● 0-10-5 ⁴⁵ 11 ³² 12 ⁴⁵ 16 ¹⁵ 24; F NNE 22 ²⁵ 24
24	8	10	05	03	07.3	02.4	08.4	.	● 0-14 ⁵⁵ F E 0-24
25	8	00	00○	00	00.0	08.8	.	.	F NNE 0-24 ¹⁰ 17 ³⁰ 24
26	8	00	00	00	00.0	08.6	.	.	F NNE 0-14 ⁵
27	7	01	10○	10	07.0	06.0	.	.	L 0-17-8 ³⁰ ; ● 21 ¹⁵ 24
28	8	10	03○	00	04.3	07.4	03.6	.	● 0-6; F NNE 8 ⁵⁰ 24; F NNE 0-24
29	9	02	01○	00	01.0	08.2	.	.	F NNE 0-24
30	9	01	06○	00	02.3	08.2	.	.	F ESE 18 ²⁰ 24
31	8	05	09○	10	08.0	05.6	.	.	F ESE 18 ²⁰ 24
MES.									
VR.		05.2	05.7	04.4	05.1	146.5	104.4		

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1	8	09	09	10	05.3	02.6	03.8	.	● 0-17 ³⁵ 10 ⁵⁰ 14 ⁰² 18 ³⁰ ; F ESE-E 7 ¹² 8 ⁴⁵
2	6	10●	10	10	10.0	00.0	07.5	.	● 0-17 ³⁵ 10 ⁵⁰ 14 ⁰² 18 ³⁰ ; F ESE-E 7 ¹² 8 ⁴⁵
3	8	08	09	00	05.7	03.3	04.3	.	T 17 ³⁵ F NNE 14 ¹⁰ 24
4	8	00	01○	00	00.3	09.4	.	.	F NNE 0-24
5	9	02	00○	00	00.7	05.3	.	.	F NNE 0-10
6	8	00	00○	00	00.0	09.3	.	.	F NNE 0-10
7	8	01	02○	00	01.0	09.6	.	.	F NNE 0-10
8	8	00	06○	02	02.7	06.9	.	.	F NNE 0-10
9	6	10	10	03	07.7	01.3	.	.	F NNE 0-10
10	8	10	10	10	10.0	00.0	.	.	F ESE 3 ⁴⁰ 22
11	9	08	03○	10	07.0	06.8	.	.	● 9 ³⁵ 9 ⁴⁵ 15 ³⁵ 17 ³⁰ ; w 20 ³⁰ n
12	8	08	00○	00	02.7	08.9	00.5	.	F NNE 14 ⁰² 13 ²⁷
13	9	06○	05	10	08.3	05.1	.	.	F ESE 14-24
14	8	10	10	10●	10.0	00.0	.	.	F ESE-SE 0-22 ⁴⁵ ; ● 18 ⁵⁰ 24
15	8	10	10●	10	10.0	01.0	18.0	.	● 0-10-5 ³⁰ 11 ³⁰ 17 ¹⁰
16	8	10●	05	10●	05.7	01.6	01.2	.	● 0-11 ¹⁰ 18 ³⁰ 21 ³⁰
17	8	09	08	09	08.7	05.8	04.6	.	F NNE 5 ¹⁰ 24
18	8	01	03○	00	01.3	09.1	.	.	F NNE 13 ³⁰
19	8	10	10●	10	10.0	00.0	.	.	● 13 ³⁰ 18 ¹⁰ ; F ESE 12 ²⁵ 14 ¹⁰
20	8	03	06○	00	03.0	08.9	00.7	.	F NNE 5 ⁰⁵ 24
21	8	02	10	10	07.3	04.2	.	.	F NNE 0-9 ¹⁰ ; ● 12 ³⁰ 14 ³⁰
22	8	10	10	10●	10.0	00.0	00.0	.	● 10 ²⁰ 10 ²⁰ 15 ²⁴ n
23	8	06	03	00	03.0	04.0	06.6	.	● 10 ²⁰ 12 ⁴⁵ 15 ¹⁵ 19 ¹⁵ 12 ³⁰
24	8	02	06○	00	02.7	08.4	.	.	● 10 ²⁰ 12 ⁴⁵ 15 ¹⁵ 19 ¹⁵ 12 ³⁰
25	9	04	10	10	08.0	02.7	08.2	.	● 10 ²⁰ 12 ⁴⁵ 15 ¹⁵ 19 ¹⁵ 12 ³⁰
26	8	01	01○	00	00.7	10.0	.	.	● 10 ²⁰ 12 ⁴⁵ 15 ¹⁵ 19 ¹⁵ 12 ³⁰
27	8	01○	02○	01	01.3	09.5	.	.	F NNE-N 0-16 ⁵⁵
28	8	07	02○	00	03.0	07.7	.	.	L 17-9, 18-17; F N 9 ⁵⁰ 24; F NNE 0-24
MES.									
VR.		05.6	06.0	04.8	05.5	145.8	55.4		

BR. ST-89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8	03	0	06	00	03.0	05.6	.	F _{NNE} 0-6 ⁵⁵ i
2	8	01	0	01	00	00.7	09.6	.	.
3	8	10	0	08	00	06.0	02.7	.	F _N 13 ¹⁵ , 18
4	8	07	0	07	05	06.3	07.0	.	F _N 0-5
5	8	08	0	08	00	05.3	05.3	.	.
6	8	01	0	04	00	01.7	08.5	.	.
7	8	09	0	09	10	05.3	00.2	.	F _{ESE} 7 ¹⁰ 23 ⁴⁰ i
8	8	09	0	10	10	05.7	00.0	06.6	• 0 ¹ 11 ¹⁰ 7 ²⁰ 13 ³⁰ i; 17 ²⁸ , 17 ⁴² i
9	8	10	0	10	09	05.7	00.8	06.6	F _{NNE} 0-5 ²⁰ 16 ¹⁵ 24i
10	8	04	0	07	03	04.7	07.3	.	F _{NNE} 0-11 ²⁴ 16 ⁰² 24
11	8	09	0	05	00	04.7	03.6	.	F - F _{NNE} 0-11
12	8	00	0	00	00	00.0	09.5	.	.
13	8	06	0	10	10	08.7	02.2	.	F - F _{NNE} 7-10 ³⁵ 13-24i; 18 ³⁰ 11
14	8	02	0	09	02	04.3	05.7	.	L 11-9
15	8	05	0	05	00	03.3	05.0	.	F _{NNE} 19-24
16	8	01	0	02	00	01.0	09.5	.	F _{NNE} 0-10, 18-24
17	8	00	0	01	00	00.3	10.0	.	.
18	8	01	0	01	01	01.0	10.3	.	F _{NNE} 20-24
19	8	07	0	08	06	07.0	05.6	.	F _N 15 ⁴⁵ 20 ¹⁵ 23 ²⁰ 24
20	9	01	0	01	00	00.7	10.5	.	F - F _N 0-11 ⁴⁰
21	8	02	0	03	00	01.7	10.6	.	.
22	8	00	0	00	00	00.0	10.6	.	.
23	8	00	0	02	04	02.0	10.0	.	.
24	8	06	0	10	10	08.7	01.2	.	.
25	8	10	0	10	10	10.0	00.0	.	.
26	8	09	0	05	10	05.3	00.8	00.0	• 0 ¹ 11 ²⁰ 20-23 ⁴⁵
27	8	10	0	03	03	05.3	06.5	07.0	• 0 ¹ 11 ¹⁰ 8 ³⁵ i
28	8	09	0	10	10	05.7	00.0	00.0	• 9 ³⁰ 10 ²⁰ 11 ¹⁰ 15 ³² 11
29	8	10	0	09	01	06.7	01.8	04.5	• 0 ¹ 11 ²⁰ 6 ³⁰ 11 ¹⁰ F _{NNE} 17-11i
30	8	10	0	05	07	08.7	01.3	.	• 0 ¹ 17 ²⁰ 17 ²⁵
31	8	09	0	10	00	06.3	07.1	00.4	• 11-8
MES.									
VRED.		05.4	06.0	03.6	05.0	174.0	25.5		

SPLIT MARJAN

1973 APRIL

1	8	10	0	03	00	04.3	08.8	00.1	• 0 ¹ 11-7
2	8	00	0	06	00	02.0	10.6	.	.
3	7	10	0	05	10	05.7	00.4	.	F _{ESE} 2 ¹⁰ 18 ³⁰ F _{NNE} 20 ⁵⁰ 24i; 0 ¹ 19 ³² 9 ⁴⁰ 16 ³⁰ 18 ²⁰ i
4	8	10	0	10	10	10.0	00.0	00.4	F - F _{NNE} 0-24i; 0 ¹ 0 ³⁰ 1
5	8	09	0	09	09	09.0	00.0	.	F _{NNE} 0-23 ⁵⁰
6	8	01	0	02	00	01.0	11.3	.	.
7	8	06	0	02	00	02.7	10.5	.	.
8	8	00	0	05	07	04.0	09.3	.	F - F _{ESE} 6 ⁰⁵ 24
9	7	10	0	10	10	10.0	00.0	.	F - F _N 0-24i; 0 ¹ 13 ³⁰ 14 ¹⁰ 18 ²⁸
10	8	10	0	08	02	06.7	03.7	00.0	F - F _{ESE} 18 ²³
11	8	06	0	05	00	03.7	08.9	01.6	• 1 ¹ 11 ¹⁰ 9 ¹⁰ 10 ⁰⁵ i; 8 ⁵⁰ 9 ¹⁵ i; 1 ¹ 9 ¹⁵ 9 ¹⁸ i
12	8	10	0	10	10	10.0	01.2	06.0	• 1 ¹ 11 ³⁰ i
13	8	07	0	08	00	05.0	07.5	04.2	• 11
14	8	06	0	08	00	04.7	09.4	.	F _{NNE} 18 ⁵² 24i
15	8	04	0	04	00	02.7	11.5	.	F _{NNE} 0-18 ⁴⁰ i
16	8	02	0	05	09	06.7	07.4	.	.
17	8	02	0	02	00	01.3	11.4	.	• 11-8
18	8	08	0	01	00	03.0	11.7	.	.
19	8	09	0	10	08	05.0	03.2	.	.
20	7	10	0	10	10	10.0	00.0	02.3	• 0 ¹ 11 ⁴⁰ 13 ³⁰ 14 ³⁰ F - F _{E-ESE} 3 ³⁰ 4 ³⁵ 7 ³⁰ 13 ¹⁵
21	6	09	0	10	10	05.7	02.2	18.5	T ¹ 11 ⁴⁵ 7 ¹⁵ 10 ¹⁵ 10 ²⁰ ; 0 ¹ 10 ²⁰ 16 ¹⁰ i; F _S 18 ³⁰ 20
22	8	00	0	02	00	00.7	11.4	07.8	.
23	6	02	0	10	10	07.3	02.6	.	• 16 ³² 19 ¹⁵ F _{NNE} 16 ⁴⁰ 22i
24	7	10	0	10	10	10.0	00.0	01.8	• 0 ¹ 12 ²⁰ 14 ¹⁰ 14 ¹⁵ 12 ³⁰
25	7	10	0	10	10	10.0	00.9	12.0	• 0 ¹ 11-8 ¹⁰
26	8	10	0	10	02	07.3	03.7	00.9	.
27	7	09	0	01	00	03.3	05.5	.	• 11-9 ³⁰ 9 ³⁰ 13 ³⁰
28	8	08	0	05	08	07.0	09.8	.	• 11-8 ¹⁰ F _{ESE} 22 ⁴⁰ 24
29	7	06	0	09	09	08.0	07.1	.	F _{ESE} 0-18
30	8	00	0	02	00	00.7	12.4	.	.
MES.									
VRED.		06.5	06.7	04.8	06.0	187.2	55.6		

BR. ST. 89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inozlacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8 01	0	06	04	03.7	12.5	.	.	$\Delta^1 n-8^{30}$
2	8 09	10	00	00	06.3	09.6	.	.	$\Delta^1 n-9$
3	8 07	09	10	00	06.7	04.3	.	.	$F_{ESE} 12^{30} 22^i$
4	8 05	10	03	00	06.0	04.8	.	.	.
5	8 06	07	09	00	07.3	10.2	.	.	.
6	8 05	09	10	00	08.0	08.1	.	.	$F_{ESE} 18^{35} 24^i$
7	8 09	02	00	00	03.7	09.0	.	.	$F_{ESE} 0-4^{20} i$
8	8 00	06	01	00	02.3	12.9	.	.	.
9	8 09	09	08	00	06.7	04.3	.	.	$\bullet^{tr} 13, F_{NNE} 15^{42} 22^{50} i$
10	8 04	08	00	00	04.0	07.6	00.0	.	.
11	8 04	02	00	00	02.0	11.5	.	.	.
12	8 10	08	06	00	08.0	06.3	.	.	$\bullet^{09^{15} 9^{25}} F_{NNE} 20^{55} 24^i$
13	8 04	04	00	00	02.7	11.7	00.0	.	$F_{NNE} 0-6^{20}$
14	8 00	00	00	00	00.0	13.0	.	.	.
15	8 04	03	03	00	03.3	12.5	.	.	$\Delta^1 n-9$
16	8 02	01	00	00	01.0	12.6	.	.	$= n-8^{30}$
17	8 09	10	07	00	08.7	00.3	.	.	$\bullet^{01^{20} 13^{45}}$
18	8 10	07	00	00	05.7	05.0	01.5	.	$\bullet^{02^{30} 5^{20}}$
19	6 02	05	10	00	07.0	06.1	.	.	$F-F 5^{35} 24^i \bullet^{tr} 17^{09} 17^{15}$
20	8 10	01	00	00	03.7	09.5	00.0	.	$F_{ESE} 0-3^{30}$
21	8 02	06	00	00	02.7	12.6	.	.	$= n-9^{30}$
22	8 00	05	00	00	01.7	12.5	.	.	$= n-8^{30}$
23	8 02	07	02	00	03.7	05.8	.	.	$= n-9^{30} = 9^{30} 11, 18-24$
24	8 00	03	00	00	01.0	13.3	.	.	$= 0-9$
25	8 01	08	00	00	03.0	11.7	.	.	$F_{NNE} 19^{30} 23^i$
26	8 00	05	00	00	01.7	12.7	.	.	$F-F_{NNE-N} 15^{50} 23^{15} i$
27	8 00	01	00	00	00.3	13.4	.	.	$F_{NNE} 17^{18} 21$
28	8 01	03	00	00	01.3	12.5	.	.	.
29	8 00	10	00	00	00.7	13.7	.	.	.
30	8 01	02	00	00	03.7	11.9	.	.	$\Phi 13^{30} 14^{30}$
31	7 01	04	00	00	01.7	12.9	.	.	$= n-6^{30} = 6^{30} 12^{30}$
MES.									
VRED.		03.8	05.6	02.4	03.9	305.6	01.5		

SPLIT MARJAN

1973 JUN

1	8 00	00	00	00.0	13.1	.	.	.	$= n-9$
2	8 00	07	00	02.3	12.9	.	.	.	.
3	8 09	10	10	05.7	06.8	.	.	.	$F_{ESE} 0-0^{30} 3^{50} 12^{40}$
4	8 10	05	00	06.3	03.3	06.1	.	.	$\bullet^{0-14-13}$
5	8 02	05	00	02.3	11.9	06.7	.	.	.
6	8 08	10	10	05.3	05.1	.	.	.	$\bullet^{018^{30} 21^{20} T^1 20^{40} 21^{45}}$
7	8 07	01	03	03.7	12.8	00.2	.	.	$F_{ESE} 8^{20} 6^{20} 18^{40} 24^i$
8	7 09	07	10	08.7	09.8	.	.	.	$F_{ESE} 0-11^{10} 14^{19} 02, 15^{15}, 15^{19} 45, 20^{30} 7^1 20^{05} 20^{25} 4^1 20^{30} n$
9	8 09	08	09	06.7	04.5	12.7	.	.	$\bullet^{07^{08} 10^{45} 18^{50} 20^{30} 17^{30} 19^{35} 10^{00} 16^{45} n}$
10	8 09	09	06	08.0	03.6	03.1	.	.	.
11	8 00	06	00	02.0	12.8	.	.	.	.
12	8 01	04	00	01.7	13.1	.	.	.	.
13	8 00	01	00	00.3	13.9	.	.	.	.
14	8 05	08	06	06.3	08.1	.	.	.	$\Delta^1 r_j - 9, = r_j - 12, T^1 M-14^{20}, F_N 23^{35} 24^i$
15	8 01	02	00	01.0	13.8	.	.	.	$F-F_{NNE} 0-24$
16	8 00	02	00	00.7	14.3	.	.	.	$F-F_{NNE} 0-9^{12}, 13^{20} 20$
17	8 00	09	10	06.3	11.7	.	.	.	$\bullet^{018^{35} 22^{20} i}$
18	7 09	09	10	05.3	01.3	.	.	.	.
19	8 00	03	00	01.0	13.5	03.9	.	.	.
20	8 02	00	00	00.7	13.1	.	.	.	.
21	8 06	09	02	05.7	05.9	.	.	.	$F_{ESE} 9-11^{30}$
22	8 03	04	07	04.7	06.5	.	.	.	$F_{ESE} 11^{09} 14^{30}$
23	5 10	01	09	06.7	08.9	01.6	.	.	$T^1_{kv} - n, \bullet^{0-13^{30} 6^{15} 19^{15} 22^{20}}$
24	8 08	06	09	07.7	09.0	05.2	.	.	.
25	8 09	08	00	05.7	08.8	.	.	.	$\bullet^{0-113^{30} 13^{56}}$
26	8 04	03	00	02.3	10.4	00.5	.	.	.
27	8 00	01	00	00.3	13.9	.	.	.	.
28	8 00	00	00	00.0	11.7	.	.	.	.
29	8 00	03	00	01.0	13.6	.	.	.	.
30	8 00	02	00	00.7	11.5	.	.	.	$F_{NNE} 19^{45} 24^i$
MES.									
VRED.		04.0	04.9	03.4	04.1	300.4	40.4		

BR. ST.89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8 010	050	02	02.7	11.4	.	.	.	$F_{NNE} 0-9, 17-19$
2	8 020	05	03	04.7	10.2	.	.	.	$F_{NNE} 16^{20} 20^{30}$
3	8 07	050	02	04.7	05.1	.	.	.	$F_{NNE} 12^{20} 17^{30} 16^{20} 23^{10}$; $07^{55} 8^{40}$
4	8 000	020	00	00.7	13.8	00.0	.	.	$F_{NNE} 9^{30} 22^{35}$
5	8 000	09	00	03.0	10.1	.	.	.	$013^{40} 14^{50}$
6	8 000	000	00	00.0	12.3	00.1	.	.	.
7	8 020	010	00	01.0	13.0	.	.	.	.
8	7 000	010	00	00.3	12.8	.	.	.	.
9	8 000	010	09	03.3	12.2	.	.	.	$\pi-8^{30} F_{NNE} 18^{25} 19^{20} 0-1 19^{05} 19^{25} 18^{20} 19^{06} 19^{20}$
10	8 040	09	06	06.3	05.8	00.5	.	.	$\pi 11^{10} 12^{05} F_{NNE} 21^{35} 24$
11	8 040	030	00	02.3	13.3	.	.	.	$F_{NNE} 0-12^{30} i, 18-20^{45}$
12	7 000	010	01	00.7	13.2	.	.	.	.
13	8 10	07	03	06.7	08.5	00.0	.	.	$06^{30} 8^{45} i$
14	7 000	060	00	02.0	10.3	00.0	.	.	.
15	8 03	10	06	06.3	10.6	.	.	.	.
16	8 000	010	00	00.3	13.2	.	.	.	.
17	8 000	000	03	01.0	12.3	.	.	.	$F_{ESE} 19^{10} 24 i$
18	8 020	070	00	03.0	11.1	.	.	.	$F_{ESE} 0-5^{10}$
19	9 000	000	04	01.3	12.5	.	.	.	$00 \pi-8^{15} 8^{20} \pi$
20	9 000	010	00	00.3	13.6	.	.	.	$F_{SW} 13^{25} 16^{25}$
21	8 000	010	00	00.3	13.5	.	.	.	.
22	8 000	000	00	00.0	13.0	.	.	.	$F_{ESE} 22^{40} 24$
23	8 000	010	02	01.0	12.7	.	.	.	$F_{ESE} 0-0^{40} 13^{40} 14^{40} 23^{55} 24^{15} \pi$
24	8 010	05	09	06.3	05.7	02.1	.	.	$0-2 0-0^{45} 22^{45} 23^{10} 24^{15} 22^{45}$
25	8 080	10	10	09.3	01.0	10.5	.	.	$011^{45} 20^{50} i$
26	8 010	050	10	05.3	11.1	05.1	.	.	$0-1 20^{29} 21^{40} 13^{10} 20^{32} 20^{42}$
27	8 020	08	01	03.7	10.4	01.7	.	.	$014^{35} 14^{35} i, T_w 14^{35} 14^{40} 16^{46} = 17^{30}$
28	8 010	05	00	03.3	07.5	00.2	.	.	010^{57}
29	8 000	030	01	01.3	13.0	00.0	.	.	.
30	8 09	05	02	05.3	09.1	.	.	.	$F_{NNE} 0-7^{50}$
31	8 060	040	03	04.3	12.8	.	.	.	.
MES.									
WRED.		02.0	04.3	02.5	02.9	335.1	20.2		

SPLIT MARJAN

1973 AUGUST

1	8 000	020	00	00.7	12.0	.	.	.	$tr 17$
2	8 080	060	10	08.0	08.1	.	.	.	.
3	8 10	060	03	06.3	05.2	00.0	.	.	$T_{NW-NE} 11^{42} 16^{30} i, 013^{04} 13^{40}$
4	8 030	08	00	03.7	04.4	.	.	.	.
5	8 000	020	00	00.7	12.5	00.0	.	.	.
6	8 000	010	00	00.3	12.7	.	.	.	.
7	8 000	010	00	00.3	12.8	.	.	.	$\pi-11$
8	8 000	05	00	01.7	10.3	.	.	.	$\pi-10^{30}$
9	8 000	000	00	00.0	12.6	.	.	.	$F_{NNE} 21^{15} 24$
10	8 000	000	00	00.0	13.2	.	.	.	$F_{NNE} 0-9^{45} i$
11	8 000	000	00	00.0	13.0	.	.	.	.
12	8 000	000	00	00.0	12.8	.	.	.	.
13	8 000	030	00	01.0	12.6	.	.	.	$F_{NNE} 19^{50} 24 i$
14	8 000	010	00	00.3	12.5	.	.	.	$F_{NNE} 0-3^{10} 6^{45} 11^{30} 15^{30} 24$
15	8 000	000	00	00.0	12.1	.	.	.	$F_{NNE} 0-1$
16	8 000	010	00	00.3	12.2	.	.	.	.
17	8 000	010	00	00.3	12.0	.	.	.	.
18	8 000	060	03	03.0	11.5	.	.	.	.
19	8 020	050	02	03.0	11.1	.	.	.	.
20	8 000	020	00	00.7	11.0	.	.	.	$\pi-11$
21	7 010	010	06	02.7	10.7	.	.	.	$\pi-9^{30}$
22	7 030	020	00	01.7	11.4	.	.	.	$\pi-11$
23	8 000	010	00	00.3	11.2	.	.	.	.
24	8 09	05	10	09.3	07.3	.	.	.	$017^{45} 18^{40}$
25	7 000	040	00	01.3	09.2	00.0	.	.	.
26	7 10	10	10	10.0	00.0	00.0	.	.	$tr 6, 11^{50} 18^{30} i, 012^{45} 13^{25} i, 13^{42} 13-18^{15}$
27	7 090	10	06	08.3	00.6	14.8	.	.	$0-2 13^{30} 15^{40} i, 21^{40} 24$
28	7 09	10	03	07.3	01.7	13.5	.	.	$0-1 1^{40} 2^{10} 8^{15} 17^{45} = 14-17, 19^{30} 20^{30}$
29	6 08	10	10	05.3	02.0	27.3	.	.	$7-2 10^{50} 14^{42} i, 13^{42} 14^{42} i, 014^{42} 14^{42} i, 14^{50} 18^{20} 20$
30	9 09	040	01	04.7	05.7	32.5	.	.	.
31	8 010	06	07	04.7	08.7	.	.	.	$T 14^{02} 14^{15} i, 014^{45} 14 i$
MES.									
WRED.		02.6	03.8	02.3	02.9	293.5	22.5		

BR. ST. 89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	9	C60	050	00	03.7	C6.2	CC.1	.	$F_{N-NNE} 6^{50} 17^{50} 14^{02} 24$
2	8	C10	010	00	00.7	11.9	.	.	$F_{N-NNE} 0-10^{54}$
3	8	000	000	00	00.0	12.1	.	.	.
4	8	000	010	00	00.3	12.1	.	.	.
5	8	000	000	00	00.0	11.9	.	.	.
6	8	000	000	00	00.0	11.5	.	.	.
7	8	000	000	00	00.0	11.6	.	.	.
8	7	000	000	00	00.0	10.9	.	.	.
9	6	000	000	00	00.0	11.0	.	.	$= n-17$
10	7	010	050	09	05.0	07.6	.	.	$= n-9^{30} \rightarrow n-9^{30} \rightarrow 21^{45}$
11	8	070	010	00	02.7	09.1	00.0	.	$F_{NNE} 4^{30} 14^{30} 20^{10} 24$
12	8	000	010	00	00.3	10.9	.	.	$F_{NNE} 0-9^{45}$
13	8	000	000	00	00.0	11.1	.	.	.
14	8	010	000	00	00.3	10.5	.	.	.
15	6	07	070	10	08.0	08.7	.	.	$= n-11$
16	7	C10	010	00	00.7	09.2	.	.	$= n-12$
17	2	10	10	03	07.7	00.2	00.0	.	$\rightarrow n-17, 13^{05} 17^{30}, T 9^{45} 9^{30} 13^{55} 14^{35} \rightarrow 13^{54} 14^{15} R 14^{35} 17$
18	8	070	10	10	05.0	00.5	20.1	.	$\rightarrow 9^{05} 10 F_{ESE} 9^{05} 19^{20} T 9^{45} 10^{22}$
19	8	060	10	03	06.3	02.3	02.4	.	$F_{ESE} 11-12^{15} R 11^{05} 12^{35} \rightarrow 2 11^{15} 11^{50}$
20	8	C10	010	00	00.7	10.5	09.6	.	.
21	8	C60	050	00	03.7	10.3	.	.	$F_{ESE} 3-10^{30} \rightarrow 16^{20} 18^{10}$
22	8	C8	09	10	05.0	02.6	.	.	$\rightarrow 17$
23	8	040	07	00	03.7	08.4	04.8	.	$F_{ESE} 2^{22} 24$
24	8	10	05	10	05.7	00.5	.	.	$F_{ESE} 0-24$
25	8	10	10	10	10.0	01.8	.	.	.
26	8	10	09	10	05.7	08.4	.	.	$F_{ESE} 0-15^{54} 19^{05} 23^{40} \rightarrow 18^{37} n, 13^{17} n, 19^{20} n$
27	8	10	10	10	10.0	08.5	34.4	.	$\rightarrow 0^{05} 0^{15} \rightarrow 14^{40} 14^{44}, F_{NNE} 3^{25} 3^{50} 11^{10} 24, R 11^{45} 12$
28	8	C9	010	00	03.3	08.6	01.1	.	$F_{NNE} 0-18^{21}$
29	8	C10	00	00	00.3	10.4	.	.	.
30	8	C20	040	00	02.0	09.8	.	.	$\rightarrow n-9$
MES.									
WRED.		03.9	03.9	02.8	03.6	249.1	72.5		

SPLIT MARJAN

1973 OKTOBAR

1	8	000	040	00	C1.3	10.3	.	.	$= n-9$
2	8	010	010	00	00.7	C5.8	.	.	.
3	8	000	000	00	00.0	09.9	.	.	.
4	8	020	000	00	00.7	09.9	.	.	.
5	8	010	000	00	00.3	10.0	.	.	.
6	8	000	000	00	00.0	09.7	.	.	.
7	8	000	060	10	C5.3	C8.9	.	.	.
8	5	10	10	10	10.0	02.0	19.0	.	$\rightarrow 0-1 R 15^{10} \rightarrow 14^{40} 15^{20}$
9	8	10	10	05	C6.3	00.0	23.2	.	$\rightarrow 0-1 13^{00} 13^{20} 11 F_{NNE} 9^{30} 24$
10	8	000	010	00	CC.3	09.3	00.0	.	$F_{NNE} 0-24^{45}$
11	7	000	020	00	00.7	09.0	.	.	$= 8^{30} 12$
12	8	010	07	07	05.0	08.0	.	.	$\rightarrow n-9^{30} = n-12$
13	8	020	060	04	C4.0	C7.9	.	.	$R 21^{10} n, F_{ESE} 20^{50} n$
14	8	09	10	09	09.3	02.0	01.1	.	$\rightarrow 0-1 F_{ESE} 2^{25} 17^{02}$
15	8	09	08	C8	C6.3	02.1	00.2	.	$\rightarrow 0-1 3^{20} 3^{40} 6^{50} 18^{26} \rightarrow 18^{45} 18^{40}$
16	8	09	08	C7	08.0	00.4	00.5	.	$F_{ESE} 10^{45} 18^{25} \rightarrow 17^{06} 18^{10}$
17	8	05	09	02	05.3	C2.2	00.0	.	$\rightarrow 17^{37} 17^{52}$
18	8	10	10	07	09.0	00.4	00.0	.	.
19	9	070	020	03	C4.0	C8.1	.	.	.
20	8	C8	10	10	05.3	00.5	.	.	$\rightarrow 16^{06} n$
21	7	10	10	08	05.3	00.0	00.0	.	$\rightarrow 19^{45} n$
22	7	C7	10	00	05.7	00.6	.	.	$T 9^{45} 10^{32} \rightarrow 19^{12} 15^{50}, F_{NNE} 11^{20} 24$
23	9	C20	060	02	03.3	09.7	06.3	.	$F_{NNE} 0-9$
24	8	040	070	00	03.7	03.2	.	.	$F_{ESE} 10^{05} 24$
25	8	C10	010	CC	CC.7	09.5	.	.	$F_{NNE} 0-n$
26	8	010	000	00	00.3	09.5	.	.	.
27	8	020	010	00	01.0	09.2	.	.	.
28	8	000	000	00	00.0	09.3	.	.	.
29	8	000	000	00	00.0	09.3	.	.	.
30	8	010	040	00	C1.7	C9.4	.	.	.
31	8	C20	000	00	00.7	08.9	.	.	$F_{NNE} 1^{10} 24$
MES.									
WRED.		03.7	04.6	03.0	03.7	198.9	51.3		

BR. ST. 89

 $H_s = 122 \text{ m}$ $H_b = 128 \text{ m}$ $h_t = 6.5 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Intencija brj. sek	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8	01	04	00	01.7	08.9	.	.	.
2	9	00	00	00	00.0	09.5	.	.	.
3	8	01	00	00	00.3	09.4	.	.	.
4	8	07	09	04	06.7	04.9	.	.	.
5	8	04	08	07	06.3	01.3	.	.	.
6	8	07	08	10	08.3	02.4	.	.	F _{ESE} 15-24; $\bullet^0$ p-n
7	8	10	10	10	10.0	00.0	00.0	.	F _{ESE-NNE} 0-24; $\bullet^0$ n-14 ⁵⁰ ; $\bullet^0$ 14 ³⁰ n; T 20 ³⁰ n
8	8	10	10	10	10.0	00.0	04.4	.	F _{NNE} 0-5 ⁰⁰ ; $\bullet^0$ 11-13 ⁵⁰ ; 14 ³⁰ -20 ⁰⁰
9	8	01	01	01	01.0	08.9	00.5	.	.
10	8	00	00	00	00.0	09.1	.	.	.
11	8	00	00	00	00.0	09.4	.	.	.
12	8	01	08	01	03.3	05.4	.	.	⊕ 12 ³⁰ -13 ³⁰
13	8	05	07	02	04.7	05.6	.	.	.
14	8	09	07	01	05.7	01.2	.	.	.
15	8	06	02	03	03.7	06.5	.	.	.
16	8	08	07	01	05.3	03.4	.	.	.
17	8	08	02	03	04.3	07.6	.	.	.
18	8	03	01	00	01.3	08.2	.	.	.
19	8	07	10	09	08.7	00.0	.	.	.
20	7	10	09	00	06.3	01.7	00.1	.	• 0-16 ⁴⁰ 17 ¹⁵
21	8	01	01	00	00.7	08.8	00.1	.	.
22	9	03	03	02	02.7	07.7	.	.	.
23	7	02	05	09	05.3	05.5	.	.	.
24	6	10	10	10	10.0	00.0	.	.	• 6 ³⁰ n; • 8 ⁵⁵ 9 ⁰⁶ ; • 11 ²⁰ -13 ⁵⁰
25	7	10	10	10	10.0	00.0	00.2	.	.
26	8	09	09	10	09.3	01.7	.	.	• 19 ⁴⁰ 20 ¹⁵ n; F _{NNE} 20 ⁴⁵ 24; 17 ¹⁵ 21 ⁵⁰ n
27	8	04	01	00	01.7	07.8	04.1	.	F _{NNE} 0-10 ³⁰
28	8	01	02	08	03.7	07.4	.	.	.
29	8	03	10	10	07.7	00.6	.	.	• 19 ⁴⁰ 20 ¹⁵ n; • 10 ³⁵ 13 ³⁰ i; F _{NNE} 14 ⁵⁰ -24
30	8	09	01	01	03.7	08.4	23.8	.	• 0-1; F _{NNE} 0-11 ¹⁵
MES.									
MRED.		05.0	05.2	04.1	04.7	151.3	33.2		

SPLIT MARJAN

1973 DECEMBAR

1	2	10*	10*	03	07.7	00.0	04.4	03	Δ* 1 n-6 ³⁰ ; * 6 ³⁰ 17 ⁴⁰ ; [X]
2	8	10	10	10	10.0	00.0	05.5	14	F _{NNE} 6-24; [X]
3	8	05	10	02	05.7	00.0	.	09	F _{NNE} 0-11; 17 ³⁰ 22; ⊕ 13 ¹⁵ 13 ⁴⁰ ; [X]
4	7	01	02	02	01.7	07.8	.	03	• 10-24; [X]
5	7	01	03	00	01.3	08.0	.	.	• 0-24
6	8	01	00	00	00.3	08.4	.	.	• 0-24
7	8	07	09	09	08.3	01.2	.	.	.
8	8	09	03	05	05.7	05.1	.	.	F _{ESE} 13 ²⁰ 20 ³⁰
9	8	04	09	10	07.7	00.8	.	.	• 17 ³⁰ 19 ⁴⁰ ; 13 ⁰⁰ 19 ²⁰ i; F _{NNW} 12 ⁰⁰ -15 ⁰⁰ 15 ⁵⁰ -24
10	8	02	02	01	01.7	07.0	02.3	.	F _{NNE} 0-13 ²⁰
11	8	00	00	04	01.3	07.5	.	.	.
12	7	10	09	07	08.7	00.6	.	.	.
13	8	10	10	10	10.0	00.0	.	.	• 0-18 ⁴⁰ 10 ⁴⁰
14	8	09	09	10	05.3	02.8	01.0	.	.
15	8	10	04	00	04.7	02.0	00.3	.	• 0-2; 6 ³⁵ 8 ⁰⁰ ; * 8 ⁰⁰ 8 ²⁵ ; * 17 ²⁵ 10 ⁴⁵ i; F _{NNE-NNW} 6 ⁵⁰ 16 ⁴⁰ 17 ⁰⁷ 10
16	8	04	00	00	01.3	07.2	03.8	.	F _{NNW} 0-5 ⁰⁰
17	8	09	10	10	09.7	00.0	.	.	• 0-1 17 ³⁵ 21 ³⁵ i
18	6	10	10	10	10.0	00.4	02.1	.	• 15 ²⁰ 15 ³⁰
19	8	09	08	09	08.7	02.5	00.2	.	• 0-1 6 ⁵⁰ 7 ⁵⁰
20	8	10	04	01	05.0	03.3	00.4	.	• 0-1 6 ²⁵ 7 ⁴⁵
21	7	08	10	10	09.3	00.1	00.6	.	F _{SE} 9 ²⁰ 16 ²⁰ ; • 0-1 12 ³⁰ n
22	8	10	07	00	05.7	01.9	27.8	.	• 0-2 6-12 ³⁵ 16-8 ³⁵
23	8	07	07	08	07.3	05.9	39.3	.	.
24	8	06	10	10	08.7	00.6	.	.	F _{SE} n-24; • 17 ⁴⁰ 9 ⁴⁵ 12 ²⁵ -20 ⁴⁵ i
25	6	07	09	09	08.3	00.0	00.5	.	F _{SE} 0-24; • 0 8 ³⁰ 13 ³⁰ i
26	7	10	09	10	09.7	00.0	04.8	.	• 0-2 6 ³⁰ 16 ⁵⁰ i; • 13 ²⁰ -13 ³⁰ T 9 ⁴⁵ 9 ⁴⁷ F _{SE} 0-11; 13 ⁵⁰ -16
27	8	01	00	00	00.3	08.0	26.5	.	• 0 n-11
28	8	06	05	06	05.7	03.8	.	.	• 0 n-10
29	7	01	00	00	00.3	07.8	.	.	• 0 n-11
30	8	04	09	10	07.7	04.2	.	.	• 0 n-10
31	8	10	10	10	10.0	00.0	.	.	• 0 7 ²⁵ 7 ⁵⁰
MES.									
MRED.		06.5	06.4	05.7	06.2	97.6	119.5		

[illegible]

1	C	1C	1C	1C	1C.0	00.0	C1.2	48	$\equiv 0-24, V0-24, F_{\text{FSSW}} 0-24, * 3^{10} 6^{30} 12^{30} 15^{10} \text{ and } 3^{10} 24, *$
2	C	10	10	10*	1C.0	00.0	01.7	54	$\equiv 0-24, V0-24, F_{\text{FSSW}} 0-24, \text{ and } 0-24, * 0^{10} 6^{15} 11^{30} 18, *$
3	C	10	10	10	1C.0	01.3	C4.1	62	$V0-24, \equiv 0-0^{10} 3^{30} 24, \text{ and } 0-11, F_{\text{FSSW}} 0-3, 8-11^{30} \text{ and } 100^{30} 3^{30}, *$
4	8	10	00	03	04.3	06.6	.	61	$V0-24, \equiv 0-10^{45} F_{\text{FSSW}} 0-24, * 10^{10} 3^{30} 24, *$
5	9	10	00	00	03.3	09.6	.	60	$V0-24, F_{\text{FSSW}} 0-14^{45}, \equiv 0^{30} 7^{20} \text{ and } 200^{70} 24, *$
6	9	00	00	00	00.0	09.6	.	57	$V0-24, * 200^{70} 24, F_{\text{FSSW}} 8^{45} 24, *$
7	9	00	03	00	01.0	09.7	.	54	$V0-24, * 800^{70} 24, F_{\text{FSSW}} 0-16^{15}, *$
8	9	03	01	10	04.7	09.7	.	52	$V0-24, * 800^{70} 24, F_{\text{FSSW}} 0-15, F_{\text{FSSW}} 5^{45} 12, \equiv 10^{30} 24, *$
9	C	10	10	10	1C.0	00.0	.	52	$V0-24, \equiv 0-24, F_{\text{FSSW}} 0-24, *$
10	0	10	10	10*	1C.0	00.0	.	50	$V0-24, \equiv 0-24, F_{\text{FSSW}} 0-24, * 13^{30} 24, \text{ and } 13^{30} 24, *$
11	C	10	10*	10	1C.0	00.2	06.3	55	$V0-24, \equiv 0-24, F_{\text{FSSW}} 0-16^{30}, * 0-8^{15} 17^{30} 19^{30} \text{ and } 0-16^{30}, * 600^{70} 14^{25} 16^{05}, *$
12	0	10	10*	10	1C.0	01.1	03.4	58	$V0-24, \equiv 0-15^{10} F_{\text{FSSW}} 5^{15} 14^{15} \text{ and } 6^{15} 13^{40}, *$
13	8	00	07	04	03.7	06.7	08.1	67	$V0-24, F_{\text{FSSW}} 9^{15} 24, \equiv 23^{15} 24, *$
14	0	10	10*	10*	1C.0	00.0	04.8	72	$V0-24, F_{\text{FSSW}} 0-24, \equiv 6-24, * 4^{10} 24, \text{ and } 4^{10} 24, *$
15	C	10	10*	10	1C.0	00.0	13.2	81	$\equiv 0-24, F_{\text{FSSW}} 0-24, \text{ and } 0-24, V0-24, * 0-6^{15} 13^{15} 18, *$
16	0	10	10	10*	1C.0	00.0	01.8	85	$\equiv 0-24, F_{\text{FSSW}} 0-13^{15} V0-24, \text{ and } 0-13^{15} * 15-23^{15}, *$
17	C	10	10	10*	1C.0	00.0	07.2	95	$\equiv 0-24, V0-24, * 7^{45} 24, F_{\text{FSSW}} 15-24, \text{ and } 15-24, *$
18	C	10	10	10	1C.0	00.0	06.1	106	$\equiv 0-24^{15} F_{\text{FSSW}} 0-18, V0-24, \text{ and } 0-18, * 0-4^{45} \text{ and } 21^{45}, *$
19	9	02	05	10	05.7	06.8	.	106	$F_{\text{FSSW}} 0^{15} 11^{45}, \equiv 0^{15} 6^{45} 19^{15} 24, \text{ and } 0^{15} 6^{45}, * 400^{65} 19^{15}, * 21^{15} 22, *$
20	C	10	10	10	1C.0	00.0	00.2	107	$\equiv 0-24, V0-24, F_{\text{FSSW}} 8^{45} 24, *$
21	0	10	10	10	1C.0	00.0	.	107	$\equiv 0-24, V0-24, F_{\text{FSSW}} 0-24, *$
22	0	10	10*	10*	1C.0	00.0	.	107	$\equiv 0-24, V0-24, F_{\text{FSSW}} 0-10^{30}, * 10^{30} 22^{10}, *$
23	0	10	10	10	1C.0	00.0	.	120	$V0-24, \equiv 0-24, * 14^{30} 18, *$
24	8	10	06	00	08.7	08.1	C4.0	127	$V0-24, \equiv 0-7^{10} 800^{70} 11^{10} \text{ and } 7^{30} 11^{20} 24, F_{\text{FSSW}} 20^{30} 24, *$
25	0	10	10*	10	1C.0	00.0	02.4	131	$V0-24, \text{ and } F_{\text{FSSW}} 0-3, 9-24, * 3-7^{15}, \equiv 3^{30} 24, *$
26	0	10	10	10	1C.0	00.0	00.0	130	$V0-24, \text{ and } 0-24, \equiv 0-24, F_{\text{FSSW}} 0-24, *$
27	C	10	10	10	10.0	00.0	00.0	128	$V0-24, \equiv 0-24, \text{ and } 0-24, F_{\text{FSSW}} 0-24, * 3^{30} 4^{10}, *$
28	0	10	10	10	1C.0	00.0	.	128	$V0-24, \equiv 0-24, \text{ and } 0-24, F_{\text{FSSW}} 0-24, * 16^{15} 18, *$

BR. ST. 140

H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokrivac h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	8	01	04	00	01.7	.	.	146	F _{sw} 20 ³⁰ 22 ³⁰ ○, ⊗
2	9	01	05	00	02.0	.	.	142	F _{sw} 18 ¹⁵ 21 ³⁰ ○, ⊗
3	8	01	10	10	07.0	.	.	135	F _{sw} 0 ¹⁵ 24 ¹⁵ ○, ⊗
4	8	05	08	06	06.3	.	.	130	F _{sw} 0 ¹⁵ 13 ¹⁵ ○, ⊗
5	8	04	06	00	03.3	.	.	123	F _{sw} 0 ¹⁵ 5 ³⁰ ⊕ 12 ¹⁵ 13 ³⁰ ○, ⊗
6	8	08	07	10	08.3	.	.	118	F _{sw} 6 ¹⁵ 24 ¹⁵ ○, ⊗
7	8	02	04	08	04.7	.	.	111	F _{sw} 0-24 ¹⁵ ○, ⊗
8	8	04	01	00	01.7	.	.	102	F _{sw} 0-13 ¹⁵ ○, ⊗
9	0	10	10	10	10.0	.	.	90	≡ 6 ²⁰ 24 V 14-24 * 14 ⁰⁵ 23 ¹⁵ * 14 ⁰⁵ 24 F _N 18 ³⁰ 24
10	0	10	10	10	10.0	.	03.6	94	V 0-24, ≡ 0-21, * 0-12 ³⁰ F _N 0-23 ³⁰ ⊗
11	8	04	05	00	03.0	.	.	90	V 0-14 ³⁰ ≡ 3-4 ⁵⁵ ○, ⊗
12	0	10	10	10	10.0	.	.	85	≡ 2 ³⁰ 24 V 22 ³⁰ 24, ⊗
13	0	10	10	10	10.0	.	.	80	≡ 0-24 V 0-24 ⊗
14	8	10	06	03	06.3	.	.	78	V 0-11 ≡ 0-7 ⁴⁰ ○, ⊗
15	8	03	06	00	03.0	.	.	67	F _N 2 ³⁰ 11, ○, ⊗
16	0	06	10	10	08.7	.	.	56	≡ 5 ⁵⁰ 24 * 19 ¹⁵ 19 ³⁰ ○, ⊗
17	0	10	10	10	10.0	.	01.6	46	≡ 0-24 V 2 ¹⁵ 24, * 3 ³⁰ 4 ¹⁵ ⊗
18	0	10	10	04	08.0	.	.	40	≡ 0-0 ³⁰ 4 ²⁵ 18 V 0-3 F _{sw} 3 ³⁰ 24, * 7 ²⁰ 11, * 10 ⁰⁰ 21-24, ⊗
19	8	00	05	07	05.3	.	01.8	30	F _{sw} 0-24 * 10 ⁰⁰ 0-12, ⊗
20	8	10	04	00	04.7	.	.	24	F _{sw} 0-23 ³⁰ ≡ 3 ³⁰ 12, ○, ⊗
21	8	01	05	00	02.0	.	.	20	F _{sw} 21 ¹⁵ 24, ○, ⊗
22	8	02	02	00	01.3	.	.	15	F _{sw} 0-24, ○, ⊗
23	8	01	06	05	04.0	.	.	11	F _{sw} 0-10 ³⁰ ○, ⊗
24	8	04	06	10	06.7	.	.	06	≡ 19 ¹⁵ 24, ○, ⊗
25	8	10	07	10	05.0	.	.	02	≡ 0-8 ³⁰ 18 ²⁵ 21 ⁰⁵ F _N 0 ³⁰ 12, 19 ³⁰ 24, ○, ⊗
26	0	10	10	10	10.0	.	.	.	F _{sw} 0-24, ≡ 0 ¹⁵ 24
27	8	10	07	10	05.0	.	.	.	F _{sw} 0-24, ≡ 0-8 ¹⁵ 16 ⁵⁵ 24 V 2-8, 22 ³⁰ 24, ○
28	0	10	10	10	10.0	.	.	.	≡ 0-24 F _N 0-24 V 0-5 ³⁰
29	8	10	08	04	07.3	.	.	.	≡ 0-10 ⁴⁵ 17 ³⁰ 20 ³⁰ F _N 0-8 ¹⁵ 15 ¹⁵ 16 ⁴⁵ , * 17 ²⁰ 17 ³⁵ ○
30	8	03	05	10	06.0	.	00.6	.	* 10 ⁰⁰ 19 ³⁰ 24 * 20 ⁰⁰ 12 ⁵⁰ ○
31	8	08	10	04	07.3	.	03.5	.	* 10 ⁰⁰ 0-10 ³⁰ , * 19 ¹⁵ 19 ¹⁵ ○
MES.						.			
WRED.		06.1	07.1	05.8	06.3	.	11.5		

1	8	10	05	04	07.7	02.0	00.0	.	○
2	8	03	02	02	02.3	13.6	.	.	* 6 ⁰⁰ 2 ³⁰ 6, F _{sw} 3-5, 20 ³⁰ 24, ○
3	8	06	10	10	08.7	03.9	.	.	F _{sw} 0-22 ³⁰ ○
4	0	10	10	07	09.0	00.0	00.7	.	● 2-2 ³⁰ ≡ 4 ⁰⁵ 14 ¹⁰ ● 4 ¹⁵ 13 ³⁰ F _S 5 ³⁰ 20
5	8	00	10	03	04.3	05.6	01.4	.	F _{sw} 0 ¹⁵ 5, * 10 ⁰⁰ 3-11, ○
6	8	04	10	06	06.7	07.0	.	.	* 8 ⁰⁰ -20 ⁰⁰ 4 ²⁰ 11, F _{sw} 15 ³⁰ 24, ○
7	8	06	05	10	07.0	08.4	.	.	F _{sw} 0-24 ≡ 20 ³⁰ 23 ¹⁵ ○
8	8	04	05	10	06.3	10.0	.	.	F _{sw} 0-23 ≡ 2 ³⁰ 4 ⁴⁵ * 21 ¹⁵ 24, ○
9	0	05	10	05	06.7	04.7	.	.	≡ 0-10 ³⁰ * 20 ⁰⁰ 1 ¹⁵ 9 ¹⁵ 18-12 ¹⁵ 30, * 9-14, 22 ³⁰ -23 ³⁰ ≡ 9 ¹⁵ 14, 21 ³⁰ 24, 17 ¹⁰ 14, ○
10	0	10	10	10	10.0	00.0	14.4	.	≡ 0-24, * 1 ³⁰ 3 ²⁰ 14 ¹⁰ 19 ¹⁵ F _N 3-24
11	0	10	10	10	10.0	00.0	11.2	.	≡ 0-24, F _N 0-24, * 0 ¹⁵ 3 ³⁰
12	8	10	08	10	05.3	03.1	.	.	≡ 0-12, 19-23, F _N 0-18, ○
13	8	00	05	02	02.3	13.3	.	.	≡ 19 ³⁰ 20 ⁰⁵ ○
14	7	06	09	10	08.3	06.4	.	.	≡ 19 ³⁰ 14 ³⁰ * 13 ²² 13 ⁴² * 13 ⁴² 14 ¹⁵ F _N 14 ¹⁵ 24, ≡ 15-24, ○
15	0	10	10	10	10.0	00.0	03.1	.	F _N 0-24, ≡ 0-24 V 5 ³⁰ -10 ³⁰
16	8	10	02	10	07.3	02.6	.	.	≡ 0-13 ³⁰ 18 ³⁰ 24, F _N 0-24 V 1 ¹⁵ 12 ³⁰ 23-24, ○
17	8	10	05	00	05.0	06.0	.	.	≡ 0-9 ³⁰ F _N 0-14 ¹⁵ 21 ¹⁵ 24 V 0-7 ¹⁵ ○
18	8	04	07	10	07.0	03.3	.	.	F _N 0-2 ¹⁵ * 13 ³⁰ 24, ≡ 14-24, ○
19	8	10	08	05	07.7	00.0	10.4	.	● 0-5 ³⁰ ≡ 0-11, F _N 0 ¹⁵ 24
20	8	01	05	00	02.0	11.8	.	.	F _N 0-6, ○
21	8	09	08	05	07.3	04.4	.	.	F _S 9 ¹⁵ 24, ○
22	8	08	01	03	04.0	11.4	.	.	F _{sw} 0-24, ○
23	0	10	10	04	08.0	02.9	00.0	.	F _S 0-24 ≡ 1 ³⁰ 14 ³⁰ 22 ³⁰ 24, * 7 ²⁰ 10 ⁴⁵ ○
24	1	10	10	10	10.0	00.9	06.0	.	F _{sw} 0-16 ³⁰ ≡ 0-24, * 8 ³⁰ 10 ⁴⁰ 14 ³⁰ 17 ⁰⁵ 17 ¹⁵ 10, * 6 ⁰⁰ 13 ³⁰ 19 ³⁰
25	0	10	10	10	10.0	01.0	06.2	.	≡ 0-24, * 10 ⁴⁵ 12 ¹⁰ F _N 12 ¹⁵ 24, * 18-18 ²⁰ ○
26	8	10	07	10	05.0	01.5	03.0	.	≡ 0-21 ³⁰ F _N 0-21 ¹⁵ * 3 ¹⁰ 5 ¹⁵ 8-9 ¹⁵ ○
27	8	00	02	00	00.7	14.4	00.8	.	* 3 ⁰⁰ 3 ³⁰ * 3 ³⁰ 7 ³⁰ 21 ¹⁵ 24, ○
28	8	00	01	00	00.3	14.9	.	.	○ 0-6, F _N 12-15 ³⁰ ○
29	8	00	01	04	01.7	12.5	.	.	≡ 20 ³⁰ 23, ○
30	0	10	10	10	10.0	00.0	.	.	≡ 2-24
MES.									
WRED.		06.5	07.0	06.3	06.6	166.0	57.2		

BR. ST. 140

$$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijnost 0-9	Oblačnost N (0—10)				Inzolacija broj sati	Padavina R mm	Snežni pokrižak h cm	Razvoj vremena w
		14	7	14	21				
1	C	10≡	10≡	10≡	10.0	00.0	08.0	.	≡ n-n, Fw 8-n, 10-13 ³⁰
2	C	10≡	10≡	10≡	10.0	00.0	02.2	.	≡ n-n, Fw n-n
3	B	0C ⊙	01 ⊙	00	00.3	12.5	.	.	≡ n, ⊙
4	B	00 ⊙	01 ⊙	00	00.3	12.7	.	.	⊙
5	B	0C ⊙	00 ⊙	00	00.0	12.5	.	.	≡ 1000 n-8 ³⁰ ⊙
6	B	0C ⊙	00 ⊙	00	00.0	12.4	.	.	⊙
7	B	06	03 ⊙	00	03.0	10.5	.	.	Δ n, ≡ 1000 n-8 ³⁰ ⊙
8	B	0C ⊙	02 ⊙	00	00.7	11.1	.	.	Δ n, ≡ 200-100 n-8 ³⁰ ⊙
9	B	02 ⊙	03 ⊙	00	01.7	10.0	.	.	≡ 100 n-9 ⊙
10	B	00 ⊙	04 ⊙	05	04.3	08.5	.	.	≡ 1000 n-8 ⁴⁵ , T 16 ¹⁰ -16 ²⁰ , 16 ⁵⁰ -17, Fsw 18 ³⁰ n, 19 ⁴⁰ n, ⊙
11	B	1C ≡ ●	01 ⊙	10 ≡	07.0	06.5	00.8	.	≡ n-9 ⁴⁰ 17 ⁰⁵ n, F-Fw n-n, 6 ⁰⁵ 7 ⁰⁵ ≡ 200 9 ⁴⁰ 12, ⊙
12	B	10 ≡	01 ⊙	00	03.7	09.5	00.1	.	≡ n-7 ³⁰ Fw n-12 V n-8, ⊙
13	B	0C ⊙	01 ⊙	10 ≡	03.7	11.4	.	.	≡ 600-300 n-11, 17-18, Fw n-n, ≡ 18-n, ⊙
14	B	0C ⊙	01 ⊙	00	00.3	11.7	.	.	≡ n, F-Fw n-8 ³⁰ 11 ⁴⁰ n-11, ⊙
15	B	06	07	1C ≡ ●	07.7	03.3	.	.	≡ 19 ⁵⁰ 20 ⁵⁵ , 20-n, R 20 ¹⁵ -21 ⁰² , Fsw 20 ¹⁵ 21 ²⁰ ⊙
16	C	10 ≡	06 ⊙	00 ≡	05.3	06.8	05.0	.	≡ n-7 ³⁰ ≡ 7 ³⁰ 15 ≡ 20 ⁴⁰ n, ⊙
17	C	05	10 ≡	10 ≡	08.3	01.0	.	.	≡ n-6 ³⁰ 7 ³⁰ ≡ 200 6 ³⁰ 7 ⁵⁰ ≡ 7 ⁵⁰ n, 14 ⁰⁵ 18 ³⁰ Fsw 15 ¹⁵ 19 ³⁰ ⊙
18	B	01 ≡ ⊙	08 ⊙	10 ≡	06.3	03.2	03.8	.	≡ 300 n-8 ¹³⁰ ≡ 8 ²⁵ n, Fsw sw-8 ³⁰ n, 12 ⁰⁵ 12 ³⁰ 16 ¹⁵ n, ⊙
19	0	05 ⊙	10 ≡	04	06.3	02.1	08.4	.	≡ n, 7 ⁵⁰ 20 ³⁰ Fsw n-19 ³⁰ , 9 ¹⁰ 18, ⊙
20	B	1C ≡	08	00	06.0	02.7	12.3	.	≡ n-13 ³⁰ ⊙
21	B	10 ≡	06	10 ≡	08.7	03.6	.	.	≡ n-11, 17 ⁴⁰ n, F-Fsw 8 ⁰⁰ n, ⊙
22	C	10 ≡	10 ● ≡	10 ≡	10.0	00.0	.	.	≡ n-n, F-Fsw 1 ssw n-n, 10 ⁴⁰ 17
23	B	10 ≡	08	00	06.0	02.1	14.9	.	≡ n-8 ⁵⁰ 18 ⁴⁵ 20 ³⁰ , F-Fsw n-n, ≡ 300 7 ⁰⁵ 9, ⊙
24	B	06	08	00	04.7	01.7	.	.	F-Fsw n-n, ≡ h, ⊙
25	B	09	06 ⊙	02	05.7	02.5	.	.	Fsw-s n-n, ⊙
26	B	06 ⊙	08	06	06.7	04.8	.	.	Fs n-n, ≡ 800 n-n, ⊙
27	1	10 ≡	10 ● ≡	10 ●	10.0	00.0	.	.	≡ n-10 ³⁰ 13 ³⁰ n, F-NE-SE 8-11, 7 ¹⁰ 10 ¹⁰ 13 ²⁰ n, 18-9 ⁵⁰ ≡ 600-100 10 ³⁰ 13 ³⁰
28	C	10 ≡	1C ≡	1C ≡	10.0	00.0	23.3	.	≡ n-n
29	B	05 ⊙	01 ⊙	00	02.0	11.4	00.5	.	≡ n, ≡ 800 n-11 ³⁰ ⊙
30	9	02 ⊙	02 ⊙	10 ≡	04.7	11.5	.	.	≡ 800 n-11, Fsw 18-n, ≡ 19 ⁴⁰ n, ⊙
MES.									
VRED.		05.4	05.2	04.7	05.1	186.6	79.3		

1	9	000	020	00	00.7	.	.	.	800-11 ⁵⁰ n-11 ⁵⁰ ⊙
2	8	C40	C10	00	C1.7	.	.	.	800-14 ⁵⁰ n-14 ⁵⁰ ⊙
3	8	000	000	00	00.0	.	.	.	800-600 n-11 ⁵⁰ ⊙
4	8	000	000	00	00.0	.	.	.	800-200 n-11 ⁵⁰ ⊙
5	8	000	000	00	00.0	.	.	.	800-200 n-11 ⁵⁰ ⊙
6	8	000	000	00	00.0	.	.	.	1000-800 n-11 ⁵⁰ ⊙
7	8	000	000	00	00.0	.	.	.	100-10 ³⁰ F _{sw} 18 ¹⁵ n ₁ ≡ 20 ³⁵ n ₁ ⊙
8	0	09	10	10	05.7	.	.	.	≡ 8 ⁰⁵ n ₁ ⊙ 9 ⁰⁵ 10 ¹⁵ ≡ 800 10 ²⁷ 12 ²⁷ F _{sw} 11 ⁴⁵ 13 ²⁰
9	C	10	10	10	10.0	.	.	.	≡ n-n, F _{sw} NNE n-n
10	1	10	10	10	06.7	.	.	.	≡ n-15 ⁴⁰ F _{sw} NNE n-12 ¹⁵ ≡ 800 17 ²⁰ n ₁ ⊙
11	8	000	010	10	03.7	.	.	.	F _{sw} 15-n ₁ ≡ 19 ¹⁰ n ₁ ⊙
12	8	10	040	10	08.0	.	.	.	F _{sw} n-13 ³⁰ ≡ n-6 ²⁰ 20 ³⁰ n ₁ ≡ 600-300 7 ³⁵ 12, 18-20 ³⁰ ⊙
13	0	10	10	10	10.0	.	.	.	≡ n-n, F _{sw} 8 ³⁰ 12 ³⁰ ⊙
14	0	10	10	10	10.0	.	.	.	≡ n-n, F _{sw} 8-n ₁ ⊙ 19 ¹⁰ n ₁
15	C	10	10	10	10.0	.	.	.	≡ n-21 ¹⁰ F _{sw} n-n ₁ ⊙ n ₁ 10 ³⁰ 20 ³⁰
16	0	10	10	10	10.0	.	.	.	≡ n-n, F _{sw} n-n ₁ ⊙ 17 ¹⁵ 20
17	8	10	10	10	08.3	.	.	.	≡ n-n, F _{sw} n-n ₁ ⊙
18	8	10	10	10	10.0	.	.	.	≡ n-8 ³⁰ F _{sw} n-20 ³⁰ ≡ 12 ³⁰ n ₁ ⊙ 19 ¹⁵ n ₁ ⊙
19	8	C8	030	10	07.0	.	.	.	≡ n ₁ 20 ²⁵ n ₁ V n-9 F _{sw} 18 ³⁰ n ₁ ⊙
20	8	10	10	10	10.0	.	.	.	F _{sw} n-24 V n-9 F _{sw} 18 ³⁰ n ₁ ⊙ 10 ¹⁰ 11 ³⁰ 18 ¹⁵ 24, 12 ⁵⁵ 17 ¹⁰ 17 ⁵⁰ ≡ 1000-300 13 ¹⁰ 15
21	8	10	10	10	10.0	.	.	.	≡ n-13 ¹⁵ 18 ¹⁵ 24, F _{sw} n-24 13 ¹⁹ 24, 19 ¹⁰ 24, 19 ¹⁰ 24, 19 ¹⁰ 24
22	C	10	10	10	10.0	.	.	.	10-3, 11 ³⁰ 12 ³⁰ F _{sw} n-24 ≡ 0-7 ³⁵ 9 ⁴⁰ 24, 0-3 ³⁰ ⊙ 0 ¹⁵ 255 n ₁ 11 ³⁰ 12 ¹⁵ 12
23	C	10	10	10	10.0	.	.	.	≡ n-2 ¹⁰ V n-24, F _{sw} n-24 ≡ 11 ³⁰ 20 ³⁰ 24, n-2 ¹⁰ 24, 19 ¹⁰ 24, 19 ¹⁰ 24, 19 ¹⁰ 24
24	0	10	10	10	10.0	.	.	.	F _{sw} n-24 V n-24, 2 ¹⁵ 24, 11 ³⁰ 24, 11 ³⁰ 24, 11 ³⁰ 24, 11 ³⁰ 24
25	C	10	10	10	10.0	.	.	.	V n-24, ≡ 0-24, F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
26	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
27	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
28	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
29	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
30	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵ 24
31	8	10	10	10	10.0	.	.	.	V n-24, ≡ 0-10 ³⁰ F _{sw} n-24, 10 ¹⁵ 24, 10 ¹⁵ 24, 10 ¹⁵

BR. ST. 140

$H_s = 2067 \text{ m}$ $H_b = 2070.4 \text{ m}$ $h_t = 3.0 \text{ m}$ $h_r = 1.5 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dies	7	7	
1	8	10	00	00	00	03.3	05.2	02	F-FNO-24, V0-11 ³⁰ = 0-10 ⁰⁵ ○, ☒
2	9	00	00	00	00	00.0	10.1	02	F-FNO-10 ³⁰ ○, ☒
3	9	00	00	00	00	00.0	09.6	.	○
4	9	04	00	00	00	01.3	10.0	.	Fsw 19 ⁰⁵ 24, ○
5	9	01	06	10	05	05.7	06.2	.	F-Fsw 0-24, 800-5-10 ³⁰ = 15 ⁴⁵ 24, ○, ☒
6	C	10	10	10	10	00.0	00.0	.	F-Fsw-ssw 0-24, = 0-24
7	C	10	10	10	10	00.0	07.0	.	F-Fsw-ssw 0-8, 18 ³⁰ 24, = 0-24, 11 ³⁰ 17 ³⁰ 23 ³⁰ V 9 ¹⁵ 24, 17-24, ☒
8	1	08	00	00	00	02.7	00.0	18	V0-24, = 0-5 ³⁰ 10 ³⁰ 24, F-FNE 0-24, 10-24, 11 ³⁰ 15 ³⁰ 18 ³⁰ 24, ☒
9	C	10	10	10	10	00.0	00.0	26	V0-24, = 0-24, F-FNUE-N 0-24, 10-5 ³⁰ 10-24, ☒
10	9	00	00	00	00	00.0	10.1	26	= 0-24, F-FNE-N 0-11 ³⁰ 10-11 ³⁰ 11 ³⁰ 4 ³⁰ 24, ○, ☒
11	9	00	00	00	00	00.0	10.1	25	800-300 0-24, V 1-8 ³⁰ F-FSE 20 ³⁵ 24, ○, ☒
12	8	00	04	00	01	01.3	04.1	22	Fsw-ssw 0-2, 12 ¹⁵ 24, 800 0-24, = 10 ²⁰ 13 ⁵⁵ ○, ☒
13	8	00	06	04	03	03.3	07.6	21	F-Fsw-sw 0-24, 800 0-17 ³⁰ = 23 ⁵⁵ 24, ○, ☒
14	C	10	10	10	10	00.0	00.0	20	Fsw 0-24, = 0-1 ³⁰ = 13 ⁰⁵ 24, V 7 ⁰⁰ 24, ☒
15	C	05	10	10	08	08.3	04.3	21	V0-20, = 0-3 ¹⁰ 11 ⁴⁵ 24, 11 ⁴⁵ 15 ⁴⁵ 12 ⁰⁰ 3 ¹⁰ 11 ⁴⁰ F-Fsw 9 ³⁰ 24, ○, ☒
16	8	00	05	00	01	01.7	04.8	18	= 0-11 ⁴⁵ F-Fsw-w 0-24, = 16 ⁴⁵ 24, ○, ☒
17	0	10	10	10	10	00.0	00.0	17	= 0-24, F-Fsw 0-8 ⁴⁵ 11 ³⁰ 11 ⁴⁵ ☒
18	8	10	01	00	03	03.7	05.5	15	= 0-12 ⁰⁰ V 1 ³⁰ 11 ⁴⁵ 12 ⁴⁵ 17 ⁵⁰ ○, ☒
19	9	01	02	10	04	04.3	08.8	13	F-Fsw-ssw 3 ⁴⁵ 24, 800 5 ³⁰ 13 ⁵⁵ = 15 ⁵⁰ 15 ⁵⁰ = 15 ⁵⁰ 24, V 18 ³⁰ 24, ○, ☒
20	8	10	10	10	10	00.0	00.0	13	= 0-12 ⁰⁰ 15-24, F-Fsw 0-10 ³⁰ 20 ³⁰ 24, V0-13 ³⁰ ☒
21	8	00	08	10	06	06.0	06.1	12	V0-24, = 0-10 ³⁰ 20 ³⁵ 24, F-Fw 6 ³⁰ 24, = 10 ²⁰ 12 ²⁵ ○, ☒
22	9	02	02	00	01	01.3	04.7	11	= 0-8 ³⁰ F-FN 0-20, V0-10, 800 5 ³⁰ 17 ³⁰ ○, ☒
23	9	00	00	01	00	00.3	10.4	11	800 17 ³⁰ ○, ☒
24	0	06	10	10	08	08.7	00.0	06	800 4 ³⁰ 8 ³⁰ = 8 ³⁰ 24, V 11-24, F-Fsw 11-24, ☒
25	C	10	10	10	10	00.0	00.0	05	= 0-24, V0-24, F-Fsw 0-24, ☒
26	C	10	10	10	10	00.0	01.4	07	= 0-24, V0-24, F-Fsw-N 0-24, 1 ³⁰ 24, 1 ³⁰ 24, 18 ¹⁹ 24, ☒
27	1	10	10	00	06	06.7	00.0	16	= 0-18 ³⁰ 23 ³⁰ 24, V0-24, F-FN 0-17, 1 ³⁰ 17 ³⁰ 10 ⁰⁵ 15, ☒
28	8	10	04	00	04	04.7	00.0	19	V0-24, = 0-18 ³⁰ F-FN 12 ²⁴ ☒
29	0	00	10	10	06	06.7	03.7	19	V0-24, F-Fsw-N 0-24, 800 4 ³⁰ 13 ¹⁵ 10-10 ³⁰ 24, = 13 ⁴⁵ 24, ☒
30	1	10	10	00	06	06.7	00.3	22	V0-24, F-Fsw-N 0-24, = 0-18 ²⁰ 1 ³⁰ 24, 4-11, ○, ☒
MES.									
WRED.		05.2	05.6	04.8	05.2	121.6	46.9		

1	0	09	10	10	09	09.7	00.0	CC.4	23	V0-24, F-FNW 0-4 ³⁰ 18 ³⁰ 22 ⁰⁰ 10-10 ³⁰ 18-23, 8 ³⁰ 21 ⁴⁵ = 8 ⁴⁵ 24, ☒
2	8	10	10	10	10	10.0	00.0	05.8	32	V0-24, = 0-3 ³⁰ 18 ³⁰ 14 ³⁰ 24, 800 3-14 ³⁰ F-FN 15-24, 15 ³⁰ 24, ☒
3	C	10	10	10	10	10.0	00.0	.	32	V0-24, = 0-16 ⁰⁵ 19 ⁴⁵ 24, F-FNE 0-15 ³⁰ 10-15 ³⁰ ☒
4	C	10	10	10	10	10.0	01.2	.	32	V0-24, = 0-10 ³⁰ F-Fsw 0 ⁴⁵ 17 ⁴⁵ = 10 ⁰⁰ -800 10 ⁰⁵ 20 ⁰⁵ = 20 ⁰⁵ 24, ○, ☒
5	8	00	01	01	00	00.7	09.3	.	32	V0-24, = 0-2 ⁴⁵ 800-300 2 ⁴⁵ 21 ²⁰ = 21 ²⁰ 24, F-FN 21 ³⁰ 24, ○, ☒
6	8	00	00	00	00	00.0	09.2	.	32	V0-24, = 0-5 ⁰⁵ F-FN-sw 0-17 ⁴⁵ 23 ⁴⁵ 24, 800 5 ⁰⁵ 12 ³⁰ ○, ☒
7	C	03	10	10	07	07.7	02.5	.	32	V0-24, Fsw 0-21 ⁴⁵ = 10 ³⁵ 24, ○, ☒
8	C	05	10	10	08	08.3	02.1	.	31	V0-24, = 0-1 ³⁰ 11 ⁴⁵ 24, F-Fsw 6 ⁴⁵ 24, 23 ⁴⁵ 24, 22 ⁴⁵ 24, ☒
9	C	10	10	10	10	00.0	00.0	00.4	31	V0-24, = 0-24, F-Fsw-N 0-24, 10-24, 10-2 ⁵⁵ 8 ⁵⁵ 24, ☒
10	8	03	03	00	02	02.0	07.2	15.8	53	V0-24, F-FN-E 0-24, = 0-1 ²⁵ 10-0 ⁰⁵ 10-11 ³⁰ 600 5 ⁰⁵ 23 ³⁰ ☒
11	8	00	00	00	00	00.0	09.1	.	53	V0-24, F-FNE 0-20, 800-600 10 ⁴⁵ 24, ○, ☒
12	9	00	01	02	01	01.0	09.2	.	50	V0-24, 800 0-24, Fsw-E-SE 3-8, 18-24, ○, ☒
13	C	10	10	10	10	10.0	00.0	.	44	V0-24, 800 0-250 F-FSE-SSW-sw 0-24, = 4 ¹⁰ 24, 1 ³⁰ 8 ²⁰ 24, ☒
14	8	01	01	10	04	04.0	08.2	.	44	V0-24, = 0-4 ²⁰ 17 ⁴⁰ 24, F-Fsw-SSE 0-24, 10-24, ○, ☒
15	C	10	10	10	10	10.0	00.0	05.0	50	V0-24, = 0-24, F-Fsw-S-N 0-24, 10-24, 10-2 ⁴⁰ 24, ☒
16	C	10	10	01	07	07.0	00.0	24.0	73	V0-24, 10-2 ³⁰ F-FN-NW 0-24, = 0-15 ⁴⁵ 10-13 ¹⁷ ☒
17	C	10	10	10	10	10.0	00.0	.	71	V0-24, F-FNW-sw-S 0-24, = 2 ⁵⁵ 24, 1 ³⁰ 3-24, ☒
18	C	10	10	03	07	07.7	00.0	.	68	V0-24, = 0-24, F-Fs-sw 0-16 ³⁰ 10-17, ☒
19	C	10	10	10	10	10.0	00.0	.	64	V0-24, = 0-24, 10-8-24, F-Fsw-sw 9-24, 10-9 ³⁰ 10 ¹⁵ ☒
20	C	10	10	10	10	10.0	00.0	00.0	62	V0-24, = 0-24, F-Fsw 0-24, 10-24, 10-8-13 ¹⁵ ☒
21	C	10	10	10	10	10.0	00.0	01.4	65	V0-24, = 0-24, F-Fsw 0-24, 10-24, ☒
22	C	10	10	10	10	10.0	00.0	.	64	V0-24, = 0-23, 10-17, F-Fsw 0-16 ³⁰ 10-14 ³⁰ ☒
23	1	00	10	10	06	06.7	01.4	03.2	70	V0-24, F-Fsw 0 ³⁰ 24, 800-100 1 ³⁰ 13 ³⁰ = 7-24, 10-18-24, ○, ☒
24	C	10	10	10	10	10.0	00.0	.	63	V0-24, = 0-24, F-Fsw 0-24, 10-24, 10-22 ³⁰ ☒
25	C	10	10	10	10	10.0	00.0	.	62	V0-24, = 0-24, F-Fsw 0-24, 10-11 ⁴⁵ 13, 10-11 ⁴⁵ 16, ☒
26	C	10	10	10	10	10.0	00.0	00.6	62	V0-24, = 0-24, F-Fs-ssw 0-23 ⁴⁵ 10-6 ⁵⁵ 17 ¹⁵ 10-6 ⁵⁵ 24, 7 ¹⁵ 24, 18 ⁵⁵ 13, ☒
27	8	10	00	00	03	03.3	08.7	13.7	78	V0-24, = 0-7 ⁴⁵ 10-11 ⁴⁵ 10-7 ³⁰ 13 ³⁰ 13 ³⁰ 13 ³⁰ 13 ³⁰ 14 ⁴⁵ ○, ☒
28	8	03	02	00	01	01.7	07.9	.	78	V0-24, 800 5 ³⁰ 24, F-FNW 6 ¹⁵ 8 ³⁰ ○, ☒
29	8	01	01	00	00	00.7	08.9	.	76	V0-24, 800 5 ³⁰ 24, F-FNW 6 ¹⁵ 8 ³⁰ ○, ☒
30	8	05	07	10	07	07.3	03.2	.	76	V0-24, 800-600 0-19 ⁰⁵ F-Fsw-ssw 9 ³⁰ 24, = 19 ⁰⁵ 24, ☒
31	C	10	10	10	10	10.0	00.0	.	72	V0-24, = 0-24, F-Fsw 0-24, ☒
MES.										
WRED.		06.8	07.3	07.0	07.0	88.1	74.3			

BR. ST. 142

 $H_s = 630 \text{ m}$ $H_b = 637.0 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21				
1	4	10≡	10	10	10.0	00.0	.	.	$\equiv n-10, \sim 9^{25} 10^{40} \equiv 10-n$
2	4	10	10*	10	10.0	00.0	00.1	.	$\equiv n-n, * 10^{45} 14^{30} \equiv$
3	2	10≡	08≡	10≡	09.3	00.0	00.5	00	$\equiv n-11, \equiv 11-n$
4	1	10≡	10≡	10*	10.0	00.0	00.1	.	$\bullet n-10, \equiv n-9, \Delta 10-18^{30}, * 18^{30} n, \boxtimes$
5	4	10*	10	10	10.0	00.0	03.0	04	$* n-17^{30}, \Delta 7^{30} n, \boxtimes$
6	5	10≡	10*	10	10.0	00.0	01.1	05	$\equiv n-9, = 9-n, * 10^{30} n, \boxtimes$
7	7	10	10	10	10.0	00.0	00.0	04	$\boxtimes$
8	5	10	10	10	10.0	00.0	.	03	$\equiv 12-n, \boxtimes$
9	5	10	10	10	10.0	00.0	.	03	$\equiv rj-n, \boxtimes$
10	5	10	10	10	10.0	00.0	.	03	$\equiv n-n, \boxtimes$
11	5	10	10	10	10.0	00.0	.	03	$\equiv n-n, \boxtimes$
12	5	10	10	10	10.0	00.0	.	03	$\equiv n-n, \boxtimes$
13	7	10	07	00	05.7	01.6	.	03	$\boxtimes$
14	4	00	00	00	00.0	07.7	.	03	$\equiv 9^{30} 17^{35} \boxtimes$
15	8	05	01	10	05.3	05.9	.	01	$\equiv n-11, \Delta 8-10, \bullet pp, \boxtimes$
16	8	10	06	10	08.7	00.3	00.4	.	$\equiv 9-12, \bullet 17-n, F_{ESE} 20^{45}$
17	8	08	04	10	07.3	05.8	00.8	.	$\equiv n-8, \equiv 9-11$
18	8	09	10	08	09.0	00.0	.	.	$\bullet 8^{30} 9^{30}, 11^{30} 12^{30}, 18^{45} 19^{35}, 13^{30} 18^{30}$
19	3	05	09	09	07.7	04.8	07.0	.	$\equiv n-j-8, \equiv 9-16$
20	5	10	09	10	09.7	00.0	00.1	.	$\bullet n, \equiv n-9, = n-8, 11^{30} n, \equiv 8-11^{30} \equiv pp-n$
21	5	10	09	00	06.3	00.4	00.2	.	$\bullet n-n, \equiv rj-12, = 12-n$
22	4	09	10	10	09.7	00.0	00.1	.	$\equiv n-10, 12^{30} n, \equiv 7^{30} 12^{30}, 7^{40} 10^{30}, \bullet 23^{10} 24$
23	4	10	10	10*	10.0	00.0	00.9	.	$\bullet 0-0^{30} 14^{30} 18^{40}, \equiv n-12, \bullet 10^{50} 14^{30}, = 12-n, * 18^{40} 24$
24	5	10	10	10	10.0	00.0	03.6	02	$* 0-5^{30} = n-n, \Delta 6^{30} n, \boxtimes$
25	7	10	10	04	08.0	00.5	00.5	02	$F_{SE} 12^{40} 13^{05} \boxtimes$
26	6	06	00	00	02.0	07.6	.	01	$\equiv n-n, \boxtimes$
27	5	10	07	00	05.7	06.1	.	.	$\equiv n-n$
28	6	10	10	10	10.0	00.0	00.7	02	$\equiv n-n, * 2^{45} 5^{30} 23-24, = rj-n, \boxtimes$
29	5	10*	10*	10	10.0	00.0	00.6	01	$* 0-17^{30} = n-n, \boxtimes$
30	5	10	00	09	06.3	03.6	02.1	04	$\equiv n-n, \boxtimes$
31	6	10	09	10	09.7	05.4	.	01	$\equiv n-n, \boxtimes$
MES.									
WRED.		09.1	08.0	08.1	08.4	49.7	21.8		

SARAJEVO

1973 FEBRUAR

1	3	10	08	02	06.7	01.7	00.1	.	$\equiv n-n, \bullet rj-7^{20} 23^{20} 24, \bullet 12^{30} 13^{30} \equiv 13-14^{10}$
2	4	10	10	10	10.0	00.4	03.2	.	$\bullet 0-2^{40} 4^{45} 6^{20}, \bullet 2^{40} 4^{45} 6^{20} 9^{10}, F_{ESE} 8^{45}, = 11-n$
3	5	10	10	10	10.0	00.0	00.7	.	$\bullet n-12^{30} \equiv n-9 \equiv 9-11, = 11-n$
4	6	10	06	00	05.3	03.7	00.1	.	$\equiv n-rj, = rj-n$
5	3	10	10	00	06.7	00.0	00.0	.	$\equiv n-n, \bullet 5^{45} 6^{50} = pp-n$
6	4	10	10	00	06.7	00.7	.	.	$\equiv n-9, 19^{30} n, = n-n$
7	3	10	08	00	06.0	04.1	.	.	$\equiv n-10, 19^{30} n, = n-11, \vee n-9, \equiv 11-n$
8	6	08	02	00	03.3	08.0	.	.	$\equiv n-9, \equiv n-10 = 10-15$
9	7	04	08	00	04.0	02.1	.	.	$\equiv rj-8, = n-12$
10	8	10	10	09	09.7	01.2	.	.	$F_s 2^{35} 7^{10} 9^{10}, 12^{45}, 19^{10}, 23^{15} 24$
11	7	10*	06	10*	08.7	01.5	02.7	02	$F_s 0^{50} 1^{30}, \bullet n, * 6^{15} 10^{20} 20^{45} n, \boxtimes$
12	7	10*	02	00	04.0	05.0	05.1	01	$* n-7^{40}, \boxtimes$
13	6	04	09	04	05.7	06.5	00.1	00	$\equiv n-9, = n-n, \equiv 22-n, F_s 23^{05} 24$
14	8	08	08	10	08.7	01.3	.	.	$F_s 0-4^{50}, 7^{10}, 8^{25} 13^{45}, 15^{45} 20^{25} 22, \bullet 15^{20} n$
15	4	10	10*	10	10.0	00.0	23.5	.	$\bullet n-8^{45}, F_{sw} 12^{20}, * 8^{15} n, * 16^{25} 16^{40} = pp-n$
16	4	10*	10	10*	10.0	00.2	25.0	02	$* n-9, 11^{50} n, \equiv n-rj, = rj-n, \Delta 11^{20} 11^{50}, \boxtimes$
17	5	10*	10*	10	10.0	00.0	13.2	06	$* n-n, = n-n, \boxtimes$
18	6	10*	09	10	05.7	00.2	00.7	07	$* n-12, = n-n, \boxtimes$
19	6	05	08	04	05.7	07.4	00.7	03	$\equiv n-n, \boxtimes$
20	6	08	10	10	05.3	01.9	.	01	$\equiv n-n, \boxtimes$
21	6	10	09	10	05.7	00.0	00.0	00	$\equiv n-n, \Delta rj-10, pp-n$
22	4	10	10	10	10.0	00.0	01.6	00	$\bullet n-n, \equiv n-11, * 17^{20} n, 11-n, \boxtimes$
23	4	10	10*	10*	10.0	00.5	05.6	.	$\equiv n-11, = 11-n, * 13^{45} 14^{20}, * 14^{20} n, \boxtimes$
24	7	00	02	00	00.7	06.3	10.0	11	$\equiv n-rj, \boxtimes$
25	6	10*	10	10	10.0	00.0	07.4	12	$\equiv n-n, * n-rj, \boxtimes$
26	5	10*	10*	10*	10.0	00.1	01.6	11	$* n-n, \boxtimes$
27	7	10*	10	10*	10.0	01.8	03.2	13	$* n-10^{30} 15-n, \boxtimes$
28	7	10*	09*	10*	09.7	00.0	03.1	12	$* n-n, \boxtimes$
MES.									
WRED.		08.8	08.4	06.4	07.9	54.6	111.6		

BR. ST. 142

 $H_s = 630 \text{ m}$ $H_b = 637.0 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R - mm	Snežni pokrivak h - cm	Razvoj vremena w
		14	7	14	21	Sred Dias			
1	4	10*	10*	10*	10.0	00.0	01.5	15	*n-ni, *
2	7	09	08	00	05.7	03.0	02.1	12	=n-7 ³⁰ = 7 ³⁰ 11 *
3	5	10*	10	10*	10.0	00.0	00.0	07	=n-n, * 6 ⁴⁵ ni, *
4	5	10*	10	10	10.0	00.0	00.2	07	*n-n, = n-pp, *
5	6	10*	10	10	10.0	00.0	01.5	07	*n-10, = n-n, Δ 13-ni, *
6	7	09	03	00	04.0	07.5	02.8	04	=n-11, *
7	6	09	10	10	05.7	00.1	.	.	=n-pp, Δ nj-8, • 22 ⁴⁰ ni
8	3	10*	10*	10*	10.0	00.0	03.1	00	*n-n, *
9	4	10*	10*	10*	10.0	00.0	21.0	20	=n-n, *
10	6	08	10	10	05.3	01.0	04.0	18	=n-n, *
11	6	10	10	10	10.0	00.2	.	12	=n-n, *
12	7	10*	09	00	06.3	01.7	00.8	10	*n-8, = n-12, *
13	6	10	10*	10	10.0	00.0	00.0	07	Δ nj-7 ⁴⁰ = nj-pp, * 7 ⁴⁰ ni, *
14	6	10*	10	10	10.0	00.0	00.4	07	*n-10, = n-n, *
15	7	09	10	10	05.7	01.1	00.0	06	=n-11, *
16	6	10*	10*	10	10.0	00.1	00.1	02	=n-n, * nj-pp, *
17	8	10	10	00	06.7	03.6	00.0	00	=n-10
18	5	05	10	05	06.7	01.3	.	.	=n-n
19	6	10*	10	10	10.0	00.7	00.6	01	=n-pp, * 2 ⁴⁰ -9, 13 ⁰⁵ -17i, * 13-13 ⁰⁵ , *
20	8	09	06	10	08.3	04.6	02.9	00	* 7 ²⁰ 8
21	7	09	05	08	07.3	08.4	00.0	00	=n-11
22	7	08	01	00	03.0	08.1	.	.	=n-10
23	8	00	00	00	00.0	10.9	.	.	=n-8 ¹⁰ , 19 ⁴⁵ ni, Δ nj-7 ³⁰ = 8 ⁴⁰ 10
24	7	08	10	00	06.0	04.4	.	.	.
25	7	10	10	10	10.0	00.0	.	.	.
26	7	10	10	10	10.0	00.0	00.1	.	• n-5, 7 ²⁰ ni, = n-9
27	7	07	07	00	04.7	08.8	06.0	.	=n-10, • 2 ⁴⁵ 4 ⁴⁵
28	7	09	10	08	09.0	00.7	.	.	Δ n-9 = n-7 ³⁰ = 7 ³⁰ 10, F _{ESE} 19 ²⁵ 20 ³⁰
29	7	10	10	08	09.3	00.1	00.0	.	• 5 ⁴⁵ 5 ⁴⁵
30	8	10	10	10	10.0	00.7	00.0	.	=n-10, • nj-5 ³⁰
31	7	00	10	07	05.7	03.2	.	.	=n-9 ³⁰ , Δ nj-11, = 9 ³⁰ 12 ³⁰
MES.									
VRED.		08.7	08.7	07.0	08.1	70.2	57.1		

SARAJEVO

1973 APRIL

1	7	05	07	00	04.0	03.8	.	.	
2	7	07	08	00	05.0	09.3	.	.	=n-10, Δ nj-9, F _S 21 ⁰⁰ 22 ²⁰
3	7	10	10	10	10.0	00.0	.	.	=n-9, F _S 0 ⁴⁵ 2 ¹⁰ , • 11 ⁴⁵ 21 ⁴⁵ , * 21 ⁴⁵ n
4	3	10*	10*	10*	10.0	00.0	19.0	08	*n-n, *
5	5	10*	10*	10*	10.0	00.0	26.1	30	*n-n, *
6	6	10*	10	00	06.7	03.2	07.6	27	*n-7 ³⁰ = n-10, = 10-pp, *
7	7	07	04	00	03.7	11.0	00.0	10	=n-n, *
8	7	10	08	04	07.3	07.1	.	.	=n-n, F _S 20 ⁴⁵ 22
9	7	10	10	05	08.3	00.6	.	.	F _S 9 ⁴⁵ 10 ⁴⁵
10	8	07	09	10	08.7	03.1	00.0	.	F _S 2 ⁴⁵ 19 ⁴⁰ , • nj-ni, F _S 21 ⁰⁰ 22
11	8	07	09	08	08.0	04.5	02.9	.	• 7 ²⁰ 15i, * 8 ⁵⁰ 15i, F _S -w 10 ⁴⁵ 10 ⁴⁵ , 13 ⁴⁵ , 16 ²⁵ 16 ³⁵
12	8	04	10	10	08.0	02.3	00.5	.	Δ n-8, = n-9, • 13 ⁴⁰ 14 ¹⁰
13	7	10*	10	10	10.0	00.0	05.4	01	• 1 ⁴⁰ 5 ⁴⁰ , 14 ⁵⁰ 17 ⁴⁰ , * 5 ⁴⁰ 11, 17 ⁵⁰ ni, * 17 ⁴⁰ 17 ⁵⁰ , *
14	6	10	05	10	05.7	06.5	11.9	02	=n-n, *
15	5	10*	10	10	10.0	00.0	01.2	01	*n-pp, = n-n, *
16	6	10	10	10	10.0	00.0	01.0	00	=n-n, • n-10 ³⁰ 13 ³⁰ ni
17	8	10	04	03	05.7	08.0	00.8	.	=n-10
18	8	00	01	02	01.0	11.5	.	.	=n-10, Δ n-9
19	8	06	10	08	08.0	03.4	.	.	=n-11, Δ n-9
20	8	10	10	05	08.3	03.4	.	.	=7 ³⁰ 10, • 8 ⁰⁵ 17 ¹⁰ , F _S 10 ³⁰ 15 ⁵⁵
21	7	02	10	09	07.0	05.5	04.1	.	F _S 11 ⁵⁰ • 12 ²⁰ 13 ⁵⁰ 23 ²⁰ 24
22	7	05	07	10	07.3	08.5	05.7	02	• 0-1 ⁴⁰ = n-n, * 1 ⁴⁰ 4 ⁴⁵ , *
23	8	00	10	10	06.7	03.7	.	.	Δ n-8 = n-9, • 18 ¹⁰ 23i
24	5	10	05	10	09.7	00.3	01.2	.	=n-n, • 5 ⁵⁰ 14 ⁴⁰ , 11 ¹⁰ 22 ³⁰ i
25	8	10	10	10	10.0	00.5	06.2	.	• 3 ⁴⁰ 5 ⁴⁰
26	6	10	10	07	09.0	01.2	01.3	.	=n-n, • 0 ²⁰ 7 ¹⁰ , • 7 ¹⁰ 11 ²⁰
27	8	00	03	00	01.0	09.4	00.6	.	=n-10, Δ n-8 ³⁰
28	8	04	01	00	01.7	12.3	.	.	
29	8	10	08	00	06.0	04.4	.	.	F _S 8 ²⁵ 11-20 ²⁰ i
30	8	04	05	00	03.0	12.3	.	.	Δ n-8
MES.									
VRED.		07.3	08.1	06.0	07.1	135.8	95.5		

BR. ST. 142

 $H_s = 630 \text{ m}$ $H_b = 637.0 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8	000	010	00	00.3	12.5	.	.	$\Delta n-8^{30}$
2	8	010	070	03	03.7	10.0	.	.	$\Delta n-8$
3	8	020	10	04	05.3	03.2	.	.	$\Delta n-8, \bullet n-j-pip$
4	8	070	05	10	08.7	03.3	00.0	.	.
5	8	060	060	00	04.0	09.5	.	.	$\Delta n-j-8$
6	8	10	080	00	06.0	06.3	.	.	$\Delta n-j-8^{30}$
7	7	080	030	10	07.0	11.0	.	.	$\Delta n-j-8^{30}$
8	8	030	010	00	01.3	12.7	.	.	.
9	7	10	10	10	10.0	00.0	.	.	$\bullet H^{24} = n-p-n$
10	6	10	10	10	10.0	00.2	15.5	.	$= n-n, \bullet 0-12^{30}, 12^{30}-15^{30}$
11	7	040	060	00	03.3	08.2	03.0	.	.
12	7	10	10	10	10.0	00.0	.	.	$\bullet 20^{15}-21^{15}$
13	7	10	10	10	10.0	00.0	00.0	.	$= n-n$
14	7	000	050	00	01.7	11.4	.	.	$\Delta n-9^{30}$
15	8	020	10	01	04.3	11.0	.	.	$\Delta n-9$
16	6	040	10	10	06.0	02.6	.	.	$= n-j-n, \bullet 18^{50}-21^{10}$
17	6	10	10	05	08.3	00.0	06.8	.	$= n-n, \bullet 20^{30}-5^{10}$
18	5	10	10	00	06.7	00.0	.	.	$= n-j-n, \bullet 7^{10}-11^{20}$
19	8	000	010	10	03.7	07.5	03.4	.	$F_{0.125} 19^{30}$
20	8	030	030	00	02.0	11.6	.	.	$F_{0.5} 19^{30}$
21	8	020	020	00	01.3	13.5	.	.	$\Delta n-8$
22	8	010	010	00	00.7	13.3	.	.	$\Delta n-8$
23	8	000	09	07	05.3	09.0	.	.	$\Delta n-8, F_w 17^{40}$
24	8	08	040	05	05.7	09.8	.	.	$\Delta n-8$
25	8	050	07	09	07.0	06.5	.	.	.
26	6	08	09	09	08.7	05.0	00.3	.	$= n-n, \bullet 2^{10}-2^{40}, 15^{10}-15^{20}, 19^{30}-19^{50}$
27	7	070	08	08	07.7	08.0	00.3	.	.
28	7	10	09	07	08.7	05.1	00.0	.	$= n-10, \bullet 7-7^{10}$
29	7	030	09	01	04.3	07.5	00.6	.	$= n-11, \bullet 1^{30}-1^{50}, 4-13^{50}, 16^{55}-17^{10}, 18^{11} 11^{55} 14$
30	8	010	020	10	04.3	12.4	00.0	.	$\Delta n-8, \bullet 22^{15}-23^{30}$
31	8	05	09	09	05.0	06.0	00.1	.	$= n-10$
MES.									
RED.		05.3	06.7	05.1	05.7	217.5	30.0		

SARAJEVO

1973 JUN

1	8	08	060	00	04.7	03.2	.	.	.
2	8	010	010	00	00.7	13.8	.	.	.
3	8	020	10	05	05.7	05.2	.	.	.
4	7	10	10	10	10.0	00.0	00.4	.	$\bullet 1^{10}-7^{10}$
5	8	000	10	09	06.3	07.0	00.1	.	$\Delta n-8^{30} = n-10$
6	8	000	10	09	06.3	06.6	.	.	$\Delta n-8$
7	8	070	030	07	05.7	08.6	.	.	.
8	8	010	07	10	06.0	05.9	.	.	$\bullet 20^{50}-22, 16^{21} 21^{55}, 22^{20}, 22^{30}-n$
9	7	020	05	08	06.3	05.8	01.1	.	$16^{10}-13^{30}, 19^{30} n, 10^{30}, 13^{30}, 19^{50}, 19^{55}$
10	6	10	10	10	10.0	00.0	16.1	.	$= n-n, \bullet 14^{10}-18^{10}, 13^{10}-18^{20}, 22^{55}-23^{20}$
11	7	10	09	09	05.3	05.4	02.8	.	$= n-11, \bullet 0^{20}-0^{30}$
12	8	020	07	00	03.0	08.1	.	.	$\Delta n-8, = n-10$
13	8	000	010	05	02.0	13.7	.	.	$\Delta n-8^{30} = n-10, 20^{30}-n$
14	7	040	10	08	07.3	06.6	.	.	$\Delta n-8^{30} = n-10, 18^{10} 15, 11^{55} 14^{05}, 23^{25} 24, 20^{30}-n$
15	8	10	080	08	08.7	03.7	06.1	.	$\bullet 0^{20}-1^{30}$
16	7	10	050	02	05.7	02.9	.	.	.
17	7	010	040	01	02.0	09.9	.	.	$\Delta n-8^{30}$
18	8	08	050	10	07.7	04.4	.	.	$\Delta n-8^{30} = n-10, 14^{15} 14^{30}, F_w 14^{20} 14^{35}, 14^{30} 24^{10}$
19	8	07	09	10	08.7	05.3	06.6	.	$\bullet 0-3^{50}$
20	8	000	010	00	00.3	13.8	.	.	$\Delta n-8$
21	8	10	08	07	08.3	04.6	.	.	$\Delta n-8$
22	8	030	030	07	04.3	08.9	.	.	$\Delta n-8$
23	7	09	08	04	07.0	08.0	.	.	$\bullet 9-14$
24	8	060	07	10	07.7	03.2	02.3	.	$13^{10}-10, \bullet 9^{10} 10^{50}, 15^{20} 20^{50}, F_w 9^{10} 9^{15}$
25	8	10	10	09	09.7	02.4	09.3	.	$\bullet 18-18^{30}$
26	8	10	050	00	05.0	05.4	02.6	.	$= n-10, \bullet 2^{30}-5, 7^{10} 7^{20}$
27	8	000	020	00	00.7	14.0	00.0	.	$\Delta n-9$
28	8	000	010	00	00.3	14.0	.	.	$\Delta n-8^{30}$
29	7	000	040	08	04.0	12.0	.	.	$\Delta n-8, 20^{30}-n$
30	6	10	08	09	09.0	02.3	.	.	$= n-p-p$
MES.									
RED.		05.0	06.4	05.8	05.7	204.7	47.4		

BR. ST. 142

 $H_s = 630 \text{ m}$ $H_b = 637.0 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21				
1	7	08	04	10	07.3	06.5	.	.	= n-p
2	6	10	10	10	10.0	00.2	.	.	= n-p, 11 ³⁵ 14 ⁵⁰ 16-18 ⁴⁰
3	6	10	05	09	05.3	00.3	06.9	.	= n-p, 5-5 ⁵⁰ 17 ⁴⁰ 11 ³⁰
4	6	02	08	07	05.7	07.4	06.6	.	13 ⁴⁰ 13 ⁴⁰ 13 ⁴⁰ 14 ⁴⁰
5	8	05	04	06	05.0	09.2	02.0	.	= n-10, 12 ²⁰ 12 ²⁵
6	8	03	01	00	01.3	10.2	00.6	.	Δ n-9 16-17, 16 ⁴⁵ 17, 21-n
7	8	00	09	05	04.7	06.1	00.6	.	Δ n-8 13-16 ³⁰ 20 ³⁰ 13 ⁴⁵ 16 ⁵⁰
8	7	10	07	04	07.0	08.2	01.4	.	= n-rj
9	7	00	09	05	04.7	07.2	.	.	Δ n-rj, 13 14 ⁴⁵ 17, 15 ⁵⁰ 16, FNE 16-16 ⁴⁰ 22 ⁴⁵ n
10	7	10	08	10	05.3	01.5	00.1	.	● 7 ³⁵ 10 ⁵⁰
11	6	04	09	09	07.3	01.5	04.7	.	= n-p, Δ n-8
12	7	10	05	07	06.7	05.3	.	.	.
13	7	02	08	05	05.0	07.4	.	.	Δ n-rj, 13 14 ⁴⁵ 14 ⁵⁰ 15 ²⁰
14	7	04	10	00	04.7	08.2	05.8	.	Δ n-8, = n-rj
15	7	00	08	03	03.7	09.4	.	.	Δ n-rj, Fsw 9 ⁵⁰
16	8	00	02	05	02.3	13.5	.	.	Δ n-rj
17	8	00	00	00	00.0	13.8	.	.	Fsw 3 ²⁰ 3 ⁴⁰ 6 ³⁵ 8 ¹⁰ 10 ²⁰ 13 ³⁵
18	7	02	03	00	01.7	12.6	.	.	Δ 21 ⁴⁵ n
19	8	00	01	09	03.3	12.0	.	.	.
20	8	04	03	00	02.3	12.6	.	.	.
21	8	00	00	00	00.0	13.8	.	.	Δ n-8
22	8	00	01	00	00.3	13.5	.	.	.
23	8	02	05	00	02.3	12.5	.	.	.
24	7	07	09	10	06.7	06.4	01.1	.	13 ⁴⁰ 1 ⁵⁰ 2 ⁵⁰ 23 ⁴⁰ 24, Fw 12 ³⁰ 15 ⁴⁵
25	7	10	10	10	10.0	00.0	09.6	.	● 0-2 ³⁰ 14 ⁵⁰ 18 ³⁰
26	8	04	05	10	06.3	06.7	02.1	.	Δ n-8 ³⁰ , = n-10, 13 14 ⁴⁵ 17 ⁴⁰ 18-18 ²⁵
27	6	10	07	04	07.0	01.4	00.5	.	= n-p, 16 ²⁵ 18, 13 17 ⁵⁰ 18 ³⁰ 17 ⁵⁵ 17 ⁵⁰ 23 ³⁵ 24
28	6	10	06	07	07.7	05.1	14.3	.	● 0-0 ²⁰ 6 ³⁵ 7 ²⁵ 14 ⁴⁰ 15 ³⁰ , = n-p, Fw 14 ⁴⁵ 14 ⁵⁵
29	6	10	10	10	10.0	00.0	01.5	.	= n-p, 13 ⁴⁰ 16 ³⁰
30	7	10	08	02	06.7	00.8	01.2	.	= n-11
31	8	06	08	01	05.0	05.7	.	.	.
PES.									
RED.		04.9	06.2	05.1	05.4	220.6	59.4		

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1973 AUGUST

1	8	05	06	00	05.0	05.8	.	.	= n-11, 11 ¹⁵ 11 ²⁰
2	8	00	08	03	03.7	07.9	00.2	.	Δ n-8, = n-10, 13 13 ⁵⁰ 18, 15 ²⁰ 18
3	7	09	10	10	09.7	01.1	02.1	.	Δ n-8 ³⁰ , = n-11, 9 ³⁰ 19 ⁴⁵ n
4	7	09	09	07	08.3	05.2	00.0	.	Δ n-8 ³⁰ , = n-rj, 13 ⁴⁵ 13 ⁵⁰
5	7	10	10	04	08.0	04.1	01.3	.	= n-rj
6	7	02	02	00	01.3	12.5	.	.	Δ n-8 ³⁰ , = n-11
7	8	00	01	00	00.3	13.1	.	.	Δ n-8
8	7	04	09	06	06.3	07.1	.	.	Δ n-8, = n-11
9	8	04	01	05	03.3	11.5	.	.	Δ n-8
10	8	00	00	00	00.0	13.2	.	.	Δ n-8
11	8	00	00	00	00.0	13.2	.	.	Δ n-8
12	8	00	00	00	00.0	13.2	.	.	Δ n-8
13	8	00	05	01	02.0	08.2	.	.	Δ n-8
14	8	02	02	00	01.3	10.1	.	.	Δ n-8, = n-11
15	8	00	04	01	01.7	10.3	.	.	Δ n-8, = 7 ³⁰ 11
16	8	00	06	04	03.3	11.1	.	.	Δ n-8, = 7 ²⁰ 10
17	7	00	06	03	03.0	09.7	.	.	Δ n-8, = 7 ³⁰ 11
18	8	06	08	00	04.7	09.1	.	.	Δ n-8
19	7	00	09	00	03.0	08.3	.	.	Δ n-rj, 13 ⁰⁵ 13 ⁴⁵ 18-18 ²⁰ 13 ⁴⁰ 15, 17 ⁴⁵ 18 ⁴⁵
20	8	00	04	00	01.3	12.3	00.3	.	Δ n-8 ³⁰
21	8	02	03	00	01.7	11.1	.	.	.
22	8	10	07	10	05.0	03.5	.	.	13 14, 16 ²⁰ 16 ³⁰
23	7	10	02	00	04.0	08.0	00.1	.	= n-12, 13 14 ²⁵
24	7	04	10	10	08.0	04.6	.	.	= n-10, 13 12 ⁴⁵ 15 ⁴⁵ 20-n, 15-16 ³⁵ 20 ⁰⁵ 22 ⁴⁰
25	7	08	09	06	07.7	06.0	09.6	.	13 14 ⁴⁵ 18, 17 ²⁵ 18 ⁴⁰
26	6	04	10	10	08.0	03.5	00.5	.	= n-p, 11 ⁴⁰ 24
27	6	10	10	10	10.0	00.0	12.4	.	= n-p, 0-10 ⁴⁵ 10 ¹⁵ 19
28	7	10	10	05	08.3	02.3	03.2	.	● 2 ⁴⁰ 5 ⁴⁵ 13 ⁴⁵ 14 ⁴⁰ 23-24, = n-11, 7 ⁵⁰ 7 ⁵⁰ 13
29	8	10	06	10	08.7	02.7	04.4	.	= n-11, 0-2 ⁴⁰ 5 ⁴⁰ 5 ⁴⁰ 13 16 ²⁵ 17, 16 ⁴⁵ 19 ³⁰ 19 ³⁰ n
30	6	10	10	10	10.0	00.0	10.8	.	● 8 ³⁰ 14 ⁴⁰ 19-22 ⁴⁰ = 20 ³⁰ n
31	7	08	07	10	08.3	08.1	01.1	.	= n-p, 18 ³⁰ 19 ³⁰
PES.									
RED.		04.5	05.9	04.0	04.8	236.8	46.0		

BA. ST. 142

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Validnost 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokriivač h cm	Razvoj vremena w
		7	14	21	Sred Dies				
1	7	10	10	C5	08.3	00.0	00.7	.	.
2	6	10	C30	00	04.3	04.5	.	.	= n-n
3	8	000	010	00	00.3	11.8	.	.	Δ n-8 = n-12
4	8	000	010	00	00.3	12.1	.	.	Δ n-8 = n-12
5	6	000	000	00	00.0	12.0	.	.	Δ n-9 = n-12
6	8	000	C10	00	00.3	11.6	.	.	Δ n-9 = n-11 ³⁰
7	7	000	040	00	01.3	10.4	.	.	Δ n-8 = n-n
8	8	000	C30	00	C1.0	10.3	.	.	Δ n-8 ³⁰
9	7	020	010	00	C1.0	10.7	.	.	Δ n-9 = n-13 ³⁰
10	8	000	010	10	C3.7	09.4	.	.	Δ n-9, 18, 16, 19 ³⁰ , 20 ⁴⁰ , 19 ⁵⁰ , 20, 20-21 ⁴⁰ , 20 ³⁰ n.
11	8	10●	010	03	04.7	06.6	05.5	.	= n-9, 5 ¹⁵ 8 ²⁰
12	8	000	010	00	00.3	11.1	00.4	.	Δ n-9
13	8	000	020	C2	C1.3	09.5	.	.	Δ n-9
14	8	000	000	00	00.0	10.9	.	.	Δ n-9 = n-11
15	7	000	030	10●	04.3	10.3	.	.	Δ n-9 = 13-18, 18, 19 ⁵⁰ , 20 ³⁰ , 20 ³⁰ n, 19 ⁵⁰ , 23 ³⁰
16	7	10●	010	00	03.7	C8.2	C7.5	.	= n-n, Δ 19 ³⁰ n
17	7	020	0918	C7	06.0	05.2	.	.	Δ n-9 = 7 ²⁰ , 11, 13, 14-18 ³⁰ , 15 ¹⁰ , 19 ⁵⁰
18	8	C30	C8	10	07.0	05.2	13.9	.	= n-10, 12 ⁵⁰ , 13 ⁰⁵ , 17 ³⁰ , 22 ⁵⁰ , 23 ⁵⁰ i k.v.
19	8	C8	09	08	08.3	02.6	05.4	.	● 3 ¹⁰ , 4 ⁴⁰ , 10 ³⁰ , 10 ¹⁰ , 13, 11 ⁰⁵ , 11 ⁴⁰
20	8	10	030	00	04.3	08.2	08.8	.	= n-10
21	8	C20	07	00	03.0	C8.8	.	.	Δ n-9, 12-14 ³⁰ , 17 ⁴⁰ , 18 ⁴⁰
22	7	C40	10●	10	08.0	03.9	.	.	= n-10
23	7	C9	07	C0	C5.3	06.4	C7.6	.	Δ n-9, F sse 13, 15 ³⁵ , 16 ⁵⁵
24	8	C5	10	C0	05.0	04.7	.	.	Δ n-8
25	8	10	060	04	C6.7	C2.5	.	.	
26	6	C9	09	10	05.3	01.9	.	.	Δ n-9 = n-n
27	7	10●	10●	10●	10.0	00.0	00.0	.	● 6 ⁴⁵ , 7 ⁵⁰ , 7 ⁵⁰ , 10 ²⁰ , 15 ¹⁰ , 24, 13, 7 ⁵⁰ , 10
28	5	10●	10●	10●	10.0	00.0	23.0	.	= n-n, 2 ¹⁵ , 9 ⁴⁰ , 13 ³⁰ n
29	7	10	000	00	C3.3	07.2	C1.0	.	= n-n
30	8	000	000	00	00.0	10.6	.	.	Δ n-9
MES.									
VRED.	C4.5	C4.4	C3.3	04.0	217.0	78.4			

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1	8	0C0	0C0	00	0C.0	10.5	.	.	$\Delta n-9 = 7^{20} M$
2	6	10	0C0	0C	03.3	03.7	.	.	$\Delta n-9, 20-n = n-n$
3	5	10	C30	1C	07.7	03.5	.	.	$\Delta n-10 = n-n, \bullet 21^{15} n$
4	7	1C	010	0C	03.7	05.0	00.1	.	$= n-12 \bullet 1-1^{40}, \Delta 19-n$
5	8	0C0	010	0C	0C.3	08.4	.	.	$\Delta n-10, 19-n; = n-11, \equiv 7^{20} 8^{20}, \equiv 8^{20} 9$
6	6	0C0	000	00	0C.0	09.8	.	.	$\Delta n-11^{30} = 7^{20} n$
7	7	0G0	0C0	0C	0C.0	08.0	.	.	$\Delta n-10 = n-12$
8	7	1C	050	1C	05.7	00.3	.	.	$\Delta n-7^{50} = n-9, \bullet 7^{50} 10^{40} 20^{40} 24$
9	6	10	1C	10	1C.0	00.0	11.7	.	$\bullet 0-0^{50} 20^{20} 8^{10}, = n-n$
10	4	10	08	00	06.0	01.2	00.5	.	$= n-n$
11	5	040	000	03	02.3	08.6	.	.	$\Delta n-10, 19-n = n-n$
12	8	0C0	010	10	03.7	09.5	.	.	$\Delta n-10 = n-1^{40} \equiv 7^{40} 11, \bullet 21^{10} 24$
13	6	10	10	01	07.0	04.7	00.3	.	$= n-n, \Delta 19-n$
14	7	07	09	10	08.7	03.4	.	.	$\Delta n-9 = 19^{20} 21^{10}$
15	8	09	10	1C	05.7	03.1	04.7	.	$\bullet 0^{50} 3^{50} 13^{40} 13^{30} 19^{30} 20^{40}$
16	8	07	090	C7	07.7	04.6	01.6	.	$F_5 8^{30} 11^{50} 15^{45} 16^{05} 19 22^{50} 24$
17	8	06	010	C1	02.7	09.1	.	.	$F_8 -sw 0^{05} 3^{55} 8^{40} 16^{50} 11^{30} 14^{05}$
18	7	040	09	1C	07.7	05.2	.	.	$F_5 10^{15} 15^{55} 20^{55} 24, \bullet 18^{40} 21^{00}$
19	8	06	020	0C	02.7	08.6	02.9	.	
20	6	10	07	10	05.0	00.0	.	.	$\Delta n-10, = 9-n, \bullet 12^{10} 12^{30}$
21	7	0C	09	10	06.3	00.5	00.0	.	$\Delta n-10, \equiv 6^{45} 9 = 9-12, F_5 12^{10} 13^{25} 16^{20} 17^{50}, R 18^{50} n, \bullet 18^{50} 19^{30}, \bullet 19^{15} 19^{30}$
22	5	10	10	10	10.0	00.0	05.9	.	$= n-n, \bullet 25 5^{50} 9^{10} 19^{45}, R 12-bp, \bullet 17^{20} 17^{25}, \bullet 17^{25} 19^{20}$
23	8	020	08	09	06.3	09.0	22.0	00	$\Delta n-10^{50} = 7^{30} 10, \Delta 19-n$
24	4	09	10	10*	09.7	00.0	.	.	$\Delta n-9 = n-19, \bullet 9^{20} 13^{30} 18^{30} n, \Delta 13^{30} 14^{10}, \bullet 14^{10} 18^{30}$
25	7	10*	10	09	09.7	00.0	01.9	00	$\bullet 6^{55} 8, F 13^{30}$
26	8	10	010	07	06.0	06.1	00.0	00	$= 7^{30} 11$
27	7	0C0	000	00	00.0	09.1	.	.	$\Delta n-8$
28	6	000	000	00	0C.0	06.6	.	.	$\Delta n-9 = n-n$
29	3	10	0C	10	06.7	01.6	.	.	$\Delta n-9, \equiv 6^{10} 11^{30} 18-n, \equiv 11^{30} 18, \Delta 19-n$
30	2	10	10	10	1C.0	00.0	.	.	$\Delta n-11, 19-n = n-9 \equiv 9-n$
31	8	1C	000	02	04.0	07.7	00.2	.	$\bullet 9 n, \equiv n-10^{30} = 10^{30} 12$
MES.									
WED.	06.2	04.8	05.4	05.5	147.8	51.8			

Dan	Valjivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavina R mm	Snežni pokriivač h cm	Razvoj vremena w
		14	7	14	21				
1	8	06	000	00	02.0	08.4	.	.	$\angle 20-n$
2	7	00	000	00	00.0	08.9	.	.	$\angle n-9, 19 \approx n; = 7^{20}n$
3	8	00	000	00	00.0	08.2	.	.	$\angle n-9$
4	8	00	000	00	00.0	08.7	.	.	$\angle n-9$
5	8	00	000	06	02.0	09.2	.	.	$\angle n-8, = 7^{20}9, \equiv 9-11^{30}, F_{ssw} 20^{15} 21^{30}$
6	8	07	09	10	02.7	02.0	.	.	$F_{ssw} 10^{05} 17^{20} 19^{40} 22^{25}, 21^{25}n$
7	4	10*	10*	10*	10.0	00.0	05.0	00	$\bullet 3-5^{45} F_{mw} 3^{30} 3^{40} 5^{45} 6^{20} * 6^{20}n, \boxed{\times}$
8	4	10	10*	10*	10.0	00.0	22.8	15	$\equiv n-12, = 12-n, * 13-n, \boxed{\times}$
9	2	10	10	10	10.0	00.0	05.0	14	$\Delta n-10^{20} \equiv n-12, \equiv 12-16^{30}, = 16^{30}n, \boxed{\times}$
10	6	08	10	10	05.3	00.6	00.7	06	$\equiv n-n, \boxed{\times}$
11	6	10	10	10	10.0	00.0	.	.	$\equiv n-p, \equiv p-p-n$
12	3	10	10	07	05.0	00.0	.	.	$\equiv n-9, 19-n, \equiv 9-19, 9^{10} 9^{50}$
13	3	10	10	05	02.3	02.8	00.0	.	$\equiv n-8, \equiv 8-19, \equiv 19-2n$
14	4	10	07	10	05.0	01.5	.	.	$\equiv n-n, \equiv 11^{30} 12^{30}$
15	7	02	030	09	04.7	07.2	00.3	.	$\bullet n, = 4^{20} 15$
16	8	09	050	00	04.7	03.8	.	.	.
17	7	06	10	10	02.7	00.6	.	.	$\bullet 11-12, F_{ssw} 12^{55}$
18	7	10	050	00	05.0	04.7	01.0	.	.
19	4	00	000	02	02.7	06.7	.	.	$\angle n-10, \equiv n-12, \equiv 7^{30} 8^{40}, = 12-17, \Delta 18-n$
20	8	02	08	01	03.7	02.4	.	.	$\Delta n-9, = 7^{20} 10$
21	8	00	010	08	03.0	08.5	.	.	$\equiv 18-n$
22	6	02	010	05	02.7	06.7	.	.	$\angle n-11, 19-n, = 7^{20} n, \equiv 9^{30} 11$
23	3	00	00	00	00.0	07.7	.	.	$\angle n-11, 20^{40} n, \equiv 7^{20} 10, = 19-n$
24	7	06	09	00	05.0	03.0	.	.	$\angle n-9^{15}, \equiv 11-12^{30}, \equiv 11-12^{30}$
25	8	07	09	10	08.7	05.2	.	.	$F_{ssw} 10^{45} 12^{55}, 23^{50} 24$
26	8	10	09	10*	05.7	02.1	00.1	.	$F_{ssw} 8^{40} 10^{45} 17^{45}, \bullet 13-17^{20}, * 17^{20} 17^{50}, * 17^{50} 24, 19-n, \boxed{\times}$
27	7	10*	070	07	08.0	02.1	09.9	14	$* 0-7^{05} \equiv n-10, \boxed{\times}$
28	6	10*	040	00	04.7	05.1	00.0	05	$\equiv n-n, * n-8, \boxed{\times}$
29	6	00	10	10	06.7	05.9	00.0	05	$\equiv 7^{30} 9^{12}, 12^{30} 14^{15}, \equiv 9-12^{30}, F_{ssw} 14^{40} 20^{20}, * 15^{30} 16^{30}, \boxed{\times}$
30	8	10*	050	04	06.3	02.8	09.4	15	$* n-11^{15}, \boxed{\times}$
MES.									
WED.	05.8	05.5	05.5	05.6	124.8	54.2			

1	4	10	1C*	C9	C9.7	00.C	C0.8	12	$\equiv 7^{30}n, *M-20^{30}, \boxtimes$
2	5	10	1C	10	10.0	00.C	C2.5	12	$\equiv 7^{30}n, \boxtimes$
3	7	10*	1C	1C	10.0	00.C	00.7	11	$*n-7^{30}21^{30}n; \equiv n-11, 19-n; \boxtimes$
4	4	10	01 $\odot$	08	06.3	04.5	C1.C	11	$\equiv n-n, \boxtimes$
5	3	C1	04 $\odot \equiv$	10 $\equiv$	05.0	C3.6	.	10	$\equiv n-7^{30} \equiv 7^{30}n, \boxtimes$
6	3	00	00 $\odot \equiv$	0C	0C.0	C6.C	.	C9	$\equiv 7^{20}17^{45} \equiv 17^{45}n, \boxtimes$
7	7	01	05	C9	06.3	04.9	.	08	$\equiv 7^{20}10 \equiv 14^{20}n, \boxtimes$
8	8	01	01 $\odot$	C4	02.0	04.8	.	04	$F_s 16^{30}21^{25} \boxtimes$
9	7	1C	10	10*	10.0	00.2	.	.	$F_s 0^{20} \bullet 9-15i, *15-n, \boxtimes$
10	8	01	05*	C7	05.7	C4.C	11.5	04	$*12^{30}pp, \boxtimes$
11	3	0C	0C $\equiv \odot$	CC	00.0	C4.3	00.0	03	$\equiv 7^{20}15 \equiv 15-n, \boxtimes$
12	3	0C	0C $\equiv \odot$	CC $\equiv$	0C.0	C2.6	.	03	$\equiv nj-7^{30} \equiv 7^{30}n, \boxtimes$
13	3	C1	07 $\equiv$	04 $\equiv$	C4.0	00.0	.	03	$\equiv n-21^{15} \equiv 6^{45}8, \equiv 21^{15}n, \boxtimes$
14	7	0C	01 $\odot$	1C	03.7	C7.4	.	03	$\equiv 9-n, \boxtimes$
15	5	10*	10*	10*	1C.0	00.C	01.3	01	$F_{N-S} 1^{20}2^{15}5^{15}7^{10}, \bullet nj-6^{35}, *6^{35}n, R_6 6^{35}6^{50}, \boxtimes$
16	5	10*	1C	0C	06.7	C0.2	15.C	24	$*n-10 \equiv n-n, \boxtimes$
17	8	10	10	10	10.0	00.2	00.C	15	$F_s 11^{35}16^{20}19^{25}, \bullet 15-17, \boxtimes$
18	8	1C	05	1C	05.7	C0.3	00.C	05	$\equiv 7^{20}11, 15-n; \boxtimes$
19	4	09	10	C3	07.3	C0.7	.	02	$\equiv 11^{30}n, \boxtimes$
20	8	C3	01 $\odot$	07	C3.7	01.8	.	01	$\equiv n-10, \bullet 8^{25}8^{30}F_s 22^{25}, \boxtimes$
21	8	C9	09	03	07.0	C3.4	00.0	.	$F_s-wsw 3^{10}3^{20}6^{10}24; \bullet 13^{20}13^{30}$
22	7	C7	10	1C	05.0	CC.9	CC.2	.	$F_s-sw 0-1^{05}3^{46}, 6^{10}7^{30}, \bullet 9-18$
23	7	00 $\equiv$	03 $\odot$	02	C1.7	06.2	17.C	.	$\sqcup n-9 \equiv 6^{40}7^{10}, F_s 21^{40}22^{15}$
24	8	C8	04 $\odot$	1C	07.3	02.C	.	.	$F_s-sw 0^{30}8^{05}, 10^{25}15^{10}, 17^{20}20^{05}, \bullet 18-n$
25	8	C8	09	08	08.3	C1.1	.	.	$F_s 2^{05}2^{15}4^{45}11, \bullet nj-n, R_6 12^{25}$
26	7	1C	1C	1C	10.C	00.2	CC.3	.	$\sqcup n-10 \equiv n-12, 15-n; \equiv 12^{30}15$
27	7	10	01 $\odot$	00	03.7	06.1	14.8	.	$\sqcup n-12, 19-n; \equiv n-8, \equiv 8-n$
28	2	1C $\equiv$	02 $\equiv \odot$	10 $\equiv$	07.3	01.3	.	.	$\sqcup n-n, \equiv n-n, \vee n-n$
29	1	00 $\equiv$	10 $\equiv$	10 $\equiv$	06.7	C0.C	.	.	$\sqcup n-10, \vee n-10, \equiv n-n, \bullet 10^{05}10^{50}, \bullet 10^{50}16^{30}$
30	2	10 $\equiv$	10 $\equiv$	10 $\equiv$	1C.0	00.0	.	.	
31	1	10 $\equiv$	10 $\equiv$	10 $\equiv$	1C.0	C0.C	.	.	
MES.									
RED.	C6.1	C6.4	06.9	C6.5	66.9	65.7			

EK. ST. 172

 $H_s = 132 \text{ m}$ $H_b = 131.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	8	C3	C6	C2	C3.7	C4.3	.	.	.	$F_{ESE} 0-24$; $F_{ESE} 0^{15} 125$ $5^{35} 12^{39}$
2	8	C6	09	08	C7.7	C1.0	.	.	.	$F_{ESE} 0-24$; $\star 14^{45} 15^{45}$
3	6	1C	1C	C5	C5.7	00.0	00.0	.	.	$\bullet 0^{30} 9^{30}$; $11^{45} 12^{45}$; $\bullet 0-2^{30} 17^{30} 21^{30} 24$
4	3	1C	1C	1C*	1C.0	C0.0	C0.0	.	.	$\bullet 20-17^{30} 15^{45} 24$; $\bullet 0-7^{30} 15^{45}$; $\bullet 0^{15} 18^{45}$; $\star 18^{45} 24$; $\star 0-10-0^{15}$; $\bullet 11^{20} 24$; $\star$
5	4	1C*	1C	10	1C.0	C0.0	C2.7	03	.	$\bullet 1-20-2^{30} 7^{30} 24$; $\bullet 1-2^{30} 7^{30}$; $\bullet 0-2^{30} 5^{45}$; $\star$
6	5	1C	1C	1C	1C.0	C0.0	C0.2	C1	.	$\bullet 0^{14} 15$; $17^{45} 22^{30} 24$; $\star$
7	7	1C	1C	1C	1C.0	00.0	.	01	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
8	5	1C	1C	1C	1C.0	C0.0	00.0	C1	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
9	6	1C	1C	10	1C.0	C0.0	00.0	01	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
10	6	10	1C	1C	1C.0	C0.0	00.7	01	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
11	6	1C	1C*	1C	1C.0	C0.0	00.2	01	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
12	6	10	05	1C	C5.7	C0.0	00.0	C1	.	$\bullet 0-24$; $\bullet 0^{14} 15$; $\bullet 10-14^{30} 14^{30}$; $\Delta 11^{45} 13$; $\star$
13	7	0C	0C	00	C5.0	C7.5	.	.	.	$\bullet 0-6^{45}$; $\bullet 0^{30} 8^{30}$; $\bullet 20^{45} 24$
14	7	0C	0C	0C	C0.0	C7.6	.	.	.	$\bullet 0-20-10^{30} 20^{30} 24$
15	7	06	07	10	C7.7	C2.9	.	.	.	$\bullet 1-20-10^{45}$; $F_{ESE} 20^{06} 24$
16	6	10*	1C*	10*	1C.0	C0.0	C0.0	.	.	$F_{ESE} 0-24$; $\star 14^{45} 16$; $20-24$; $\bullet 10-24$; $\star$
17	7	1C	0C	08	06.0	C5.0	04.8	03	.	$\star 0-10-1^{30}$; $\bullet 0-0^{30}$; $F_{ESE} 0-5^{45}$; $18^{45} 24$; $F_{ESE} 5^{44} 18^{26}$; $\star$
18	8	05	05	1C	C6.0	C0.7	.	01	.	$F_{ESE} 0-25$; $F_{ESE} 5-12$; $\bullet 0^{14} 13^{45} 22^{45}$; $\star$
19	5	10	1C	10	1C.0	C0.0	04.5	.	.	$\bullet 0-24$; $5^{45} 9^{30}$; $19^{30} 21^{45} 24$; $\bullet 25^{45} 9^{30}$; $\bullet 16^{30} 8^{30}$; $\bullet 19^{30} 21^{45}$
20	6	10	05	C3	C7.3	C1.2	00.3	.	.	$\bullet 0-20-10^{30}$; $F_{ESE} 8^{30} 12^{45}$; $\bullet 12^{30} 24$
21	8	06	06	1C	C7.3	C2.7	.	.	.	$\bullet 0-6^{45}$; $F_{ESE} 0-24$
22	8	05	02	04	C2.7	C6.2	.	.	.	$F_{ESE} 0-24$; $F_{ESE} 21^{29}$
23	8	1C	1C	1C	1C.0	00.0	.	.	.	$F_{ESE} 0-7^{45}$; $F_{ESE} 0^{30} 0^{37}$
24	7	1C	1C	C6	C6.7	C0.0	00.0	.	.	$\star 0^{20} 4^{30}$; $F_{ESE} 5^{12} 21^{30}$; $F_{ESE} 2^{30} 24$
25	8	04	03	00	C2.3	C8.3	.	.	.	$F_{ESE} 0-4^{12}$; $8^{28} 18^{45}$; $F_{ESE} 4^{29} 24$
26	8	04	0C	0C	C1.2	C8.2	.	.	.	$F_{ESE} 0-15^{28}$; $\bullet 0-12^{15}$
27	7	0C	0C	C2	C6.7	C6.5	.	.	.	$\bullet 0^{20} 10^{45}$; $10^{30} 24$
28	6	1C	C5	10	C8.3	C2.2	.	.	.	$\bullet 0-5^{45}$; $\bullet 0-15^{45} 18^{45}$
29	6	1C	05	09	C5.3	C0.0	.	.	.	$\Delta 8^{45} 10^{15}$; $\bullet 10^{45} 22^{45}$
30	7	1C	C3	10	C7.7	C0.0	C0.0	.	.	$\bullet 0^{20} 10^{30}$; $\Delta 4^{50} 5^{45}$; $\star 9^{40} 10^{15}$; $\bullet 18^{30} 24$
31	6	10	04	1C	C8.0	C5.7	C1.7	.	.	$\bullet 0-1^{45}$; $\bullet 0-6^{30} 17^{30}$
MES. VREC.		07.7	06.8	07.4	07.3	70.8	15.1			

BEOGRAD

1973 FEBRUAR

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	7	1C	C7	09	C6.7	C1.2	.	.	.	$\bullet 0-7^{45}$; $F_{ESE} 3^{57}$; $8^{30} 14^{59}$; $\bullet 17^{45} 10^{15}$
2	7	1C	1C	0C	C6.7	C0.0	C0.5	.	.	$\bullet 0-14^{30} 8^{45}$; $F_{ESE-ESE} 8-10$; $13^{13} 16^{21} 21^{25}$
3	7	06	1C	1C	C6.7	C1.5	00.5	.	.	$\bullet 0-10^{30} 6^{45}$; $\bullet 19^{30} 24$
4	5	1C	1C	1C	1C.0	C0.0	.	.	.	$\bullet 1-20-24$; $\bullet 0-24$
5	6	10	1C	1C	1C.0	C0.0	.	.	.	$\bullet 0-24$
6	6	1C	1C	C2	C7.3	C1.2	.	.	.	$\bullet 0-21^{45}$
7	7	05	C5	C2	C6.3	C1.2	.	.	.	$\bullet 0-12^{45} 8^{30}$
8	7	05	C4	C2	C6.7	C5.5	.	.	.	$\bullet 0^{30} 7^{15}$
9	8	04	0C	09	C4.3	C5.0	.	.	.	.
10	8	06	08	09	C7.7	C2.0	.	.	.	.
11	6	10	1C	C7	C9.0	C0.0	C0.5	.	.	$F_{S-W} 0^{17} 6^{40}$; 12^{48} ; $\bullet 5^{40} 8^{35}$; $11^{45} 13^{15} 15^{45} 18^{45}$; $\Delta 7^{45} 8^{15}$; $\star 0-29^{35} 11^{30}$; $\bullet 13^{15} 19^{45}$
12	6	10	04	C0	C4.7	C5.6	C3.6	.	.	$\bullet 0^{20} 8^{30}$; $21^{30} 24$; $\bullet 0-20^{15} 15^{15}$
13	8	02	03	C7	C4.0	C7.1	.	.	.	$\bullet 0-10-9^{30}$; $F_{ESE} 9^{09}$; $12^{25} 19^{45} 24$
14	8	03	05	1C	C7.3	C2.1	.	.	.	$F_{ESE} 0-24$; $F_{ESE} 15^{25} 19^{01} 20^{25}$
15	6	09	08	C9	C6.7	C0.4	.	.	.	$F_{ESE} 0-22^{45}$; $F_{ESE} 0^{42} 24$; $3^{46} 5^{12} 11^{44} 14^{18}$; $\bullet 15^{50} 16^{20}$
16	7	1C	05	1C	C5.7	C1.4	C5.4	.	.	$\bullet 0-17^{45} 6^{20}$; $18^{45} 24$
17	6	10	10	1C	1C.0	C0.0	C6.4	.	.	$\bullet 0-10-6^{30}$; $10^{45} 15^{45}$; $\bullet 0-6^{45} 24$; $\bullet 15^{45} 16^{30}$
18	5	1C*	1C*	C8	C5.3	C0.0	00.1	.	.	$\bullet 0-18^{45}$; $\bullet 15^{45} 5^{45}$; $10^{30} 15^{30}$; $15^{30} 16^{30}$; $F_{W} 6^{12} 11^{50} 12^{12}$; $\star 6^{30} 13^{45}$; $\Delta 9^{30} 10^{30}$
19	7	0C	05	C0	C1.7	C7.2	C0.6	.	.	$\bullet 0^{30} 8^{30}$; $12^{45} 24$
20	6	C2	1C	1C	C7.3	C2.2	.	.	.	$\bullet 0-20-9^{45}$; $\bullet 5^{45} 24$; $\bullet 16^{45} 18^{30}$
21	6	C9	1C	1C	C5.7	C0.0	C0.0	.	.	$\bullet 0-24$; $\bullet 0^{11} 15$; 24
22	7	1C	1C	00	C6.7	C0.0	C3.1	.	.	$\bullet 0-5^{45}$; $14^{45} 15^{30}$; $\bullet 0-10^{30}$; $F_{NW} 13^{24}$
23	6	C3	05	1C	C7.3	C1.5	C0.2	.	.	$\bullet 12^{45} 24$; $\bullet 0-12^{30} 18^{30}$; $\bullet 22^{05} 23^{15}$; $\star 23^{15} 23^{30}$; $F_{NW} 23^{45} 23^{25}$; $\star 0-23^{30} 24$
24	8	C6	05	00	C3.7	C6.9	C4.2	01	.	$\star 0-11^{30}$; $\bullet 0-10-6^{30}$; $\star$
25	7	1C	10	10	1C.0	C0.0	C0.0	.	.	$\bullet 0^{30} 12^{30}$; $\star 6^{40} 12^{35}$; $\star$
26	6	10	10	10	1C.0	C0.0	C4.9	02	.	$\bullet 0-17^{45}$; $F_{NW} 7^{55} 24$; $\star 0-24^{20} 17^{30}$; $\star$
27	7	C8	10	10	C5.3	C1.2	C0.6	02	.	$F_{NW} 0-10^{45} 12^{59}$; 12^{59} ; $\bullet 0^{50} 13^{45}$; $\star 11^{20} 12^{50}$; $\star$
28	6	10*	10*	10	1C.0	C0.0	00.1	02	.	$\star 0-14^{10} 16^{30}$; $F_{NW} 9^{15} 14^{27}$; $\bullet 0^{45} 17^{30}$; $\star$
MES. VREC.		07.5	08.2	06.9	07.6	53.2	31.5			

BR. ST. 172

$H_s = 132 \text{ m}$ $H_b = 131.6 \text{ m}$ $h_l = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	6	08	10	10	05.3	02.8	00.0	.	.	$\approx 06^30-17^45; *15^50, 21^40-22^45, *$
2	7	05	10	05	06.0	02.6	00.0	.	.	.
3	6	05	10	10	06.3	00.9	.	.	.	$\bullet 11^55-19^45; F_{NW} 16^54-16^57$
4	6	10*	10	07	05.0	00.0	00.3	.	.	$*06^45-08^30, 10^30-09^30, 10^45-10^45, 18^15-22^45-24; \bullet 13^30-16^30$
5	6	10	07	02	06.3	06.0	01.2	.	.	$\approx 02^0-03^0, 17^15-14^30, \approx 10^30-17^45; \approx 15^15-16^15$
6	5	10	07	01	06.0	02.0	.	.	.	$\approx 00^30-17^45 \approx 01^20-09^30 \approx 19^30-12^45 \approx 12^15-24; F_{SE} 21^57$
7	7	02	10	04	05.3	00.3	.	.	.	$\approx 00^30-05^30, F_{SE-ESE} 02^20-11^34; 17^24-24; F_{SE} 15^59$
8	6	08	10*	10*	05.3	00.0	.	.	.	$F_{SE} 15^59 \approx 06^15-24; \bullet 11^40-13^15, \bullet 13^15-14^00, 19^15-24; *14^00-19^15$
9	5	10*	10	10	10.0	02.0	01.7	04	.	$*00^20-02^30, *02^30-11^30, 21^30-18^30, \bullet 13^15-16^45; *$
10	7	10	10	10	10.0	02.6	01.7	.	.	$*04^05-14^10, 17^20-18^30; \bullet 16^45-18^45$
11	5	10	10*	10	10.0	00.0	00.1	.	.	$\approx 04^30-24; *08^45-11^30, *11^30-15^15; 21^45-23^30; \bullet 15^15-21^45$
12	7	05	05	06	06.7	07.4	03.3	.	.	$\approx 05^15-10^45$
13	7	10	10	10*	10.0	01.0	00.0	.	.	$\approx 05^30-10^15, \bullet 06^45-09^15; F_{SE} 06^50-09^40; 16^15-24; *08^45-09^40; 14^30-24; F_{SE} 16^20$
14	6	10*	10*	10*	10.0	00.0	00.9	03	.	$F_{SE} 00^15-15^15; *00^10-17^30; \bullet 03^15-14^45; \bullet 17^30-18^30; *18^30-24; *$
15	6	10*	10	10	10.0	00.0	08.0	.	.	$*00^10-17^15 \approx 01^17-24; \bullet 16^45-18^15$
16	6	10	10	10	10.0	00.0	00.0	.	.	$\approx 01^10-24; \bullet 11^27-11^56, \bullet 11^56-12^03; \bullet 13^30-24$
17	7	10	08	00	06.0	05.2	01.3	.	.	$\bullet 00^14-14^15; \bullet 00^10-10^30; \bullet 12^03-24$
18	7	00	09	09	06.0	03.2	.	.	.	$\approx 00^10-24; \approx 01^20-17^30$
19	6	10	08	10	05.3	01.1	00.3	.	.	$\bullet 03^30-5^30; 12^52-23^45; \approx 05^30-22^30; F_{N-NW} 08^10-15^55; 22^36; \Delta 12^50-12^52; \nabla 01^14$
20	8	08	06	07	07.0	06.7	04.8	.	.	$[14^45]$
21	7	10	10	10	10.0	00.0	.	.	.	$F_{NW} 12^08-12^29$
22	8	01	04	04	02.0	07.0	.	.	.	$\approx 02^45-17^30, \Delta 02^30-24$
23	6	00	00	00	00.0	10.2	.	.	.	$\approx 00^30-17^30; \bullet 03^35-06^30; F_{SE} 14^27$
24	8	02	08	06	05.3	07.8	.	.	.	$F_{SE} 33^59; 16^30-16^35$
25	6	05	09	04	06.0	06.0	.	.	.	$\approx 04^45-17^45, 23^30-24; \bullet 13^30-15^45-17^15$
26	8	03	10	05	07.3	01.8	.	.	.	$\approx 00^10-17^45; F_{SE} 05^52-24$
27	7	03	04	00	02.3	07.6	00.1	.	.	$F_{SE} 00^10-08^54, 19^24; F_{SE} 02^54-19$
28	7	06	06	10	07.3	05.1	.	.	.	$F_{SE} 00^35-03^57, F_{SE} 21^35-21^35; \bullet 08^35-09^20$
29	7	10	10	10	10.0	00.0	.	.	.	$F_{SE} 11^10-16^49$
30	8	06	06	05	07.0	06.5	00.1	.	.	$\approx 01^19-24$
31	8	00	03	00	01.0	10.3	.	.	.	
MES.										
WRED.		06.9	08.1	06.5	07.3	104.1	30.8			

BEGRAD

1973 APRIL

1	7	01	04	02	02.3	08.0	.	.	.	$\approx 00^10-08^15, NW-N$
2	6	06	07	00	04.3	04.9	.	.	.	$\approx 00^10-08^15, \approx 04^15-19^30$
3	8	08	10	05	05.0	01.5	.	.	.	$\bullet 02^45-15^30; 21^45-24$
4	6	10	10	10	10.0	00.0	06.5	.	.	$\bullet 10^10-14^45; 21^05-24; \approx 12^30-24$
5	6	10	10	05	06.3	00.0	21.4	.	.	$\bullet 10^10-20^15, 23^30-24; \approx 00-24$
6	8	08	02	00	02.3	06.6	12.6	.	.	$\bullet 00^40-04^30 \approx 00^17-15 \approx 01^21-24$
7	8	04	07	02	04.3	10.8	.	.	.	$\approx 00^20-08^30, 19^45-24$
8	7	09	09	03	07.0	02.4	.	.	.	$\approx 00^20-09^30, 21^30-24$
9	8	09	10	10	05.7	00.5	.	.	.	$\approx 00^40-04^30, F_{SE} 5^52-19^52$
10	8	10	02	06	06.0	06.6	.	.	.	$F_{SSE-SSW} 06^21-13, 17^52-19; F_{S} 13-17^52; \bullet 23^50-24$
11	7	10	08	06	06.0	02.9	03.0	.	.	$\bullet 00^20-04^45, 09^15-12^15; 18^45-19^15, F_{NW} 10^18, 11^10$
12	8	03	09	10	07.3	05.9	01.2	.	.	$\approx 04^15-06^15; \bullet 21^45-24$
13	6	10	10	10	10.0	00.0	03.7	.	.	$\approx 00^10-14^45; 16^10-11^15, 18^30; F_{W} 15^15-17^03$
14	8	10	08	05	07.7	04.8	05.8	.	.	$\bullet 02^35-17^30; 10^11-20^15, 19^45$
15	8	06	10	10	06.7	03.7	00.3	.	.	$\approx 00^20-10^50; \bullet 15^45-19^30$
16	6	10	10	10	10.0	00.0	01.4	.	.	$\bullet 07^15-15^30; \approx 12^30-16^15$
17	7	06	04	02	04.0	09.3	01.4	.	.	$\approx 05^15-10^30, F_{NW} 11^24-15^29; \approx 22^15-24$
18	6	09	05	04	06.0	08.2	.	.	.	$\approx 00^10-08^30, 21^15-24; \approx 05^15-16^45; F_{NNE} 13^26-15^12$
19	8	03	07	09	06.3	08.2	.	.	.	$\approx 00^10-08^30; \bullet 19^45-21^05$
20	7	03	10	10	07.7	06.8	00.0	.	.	$F_{SE-WNW} 08^46-14^53; 18^15-18^30; 14^30-19^45; \bullet 14^40-19; \bullet 19-20^15$
21	7	05	07	10	07.3	05.2	18.3	.	.	$\bullet 14^55-20^45; 22^45-24; F_{WNW} 15^52; \nabla 15^55-16^05$
22	8	09	08	00	05.7	09.0	03.1	.	.	$\bullet 00^35-16^30; \approx 01^14-24$
23	8	00	08	10	06.0	06.6	00.0	.	.	$\approx 00^20-09^30; \bullet 01^22-24$
24	6	10	10	10	10.0	01.0	06.4	.	.	$\approx 00^10-02^45; 4^50-5^10, 17^45-18^15; 13^30-24; F_{SE} 15^59-24; F_{SE} 06^36$
25	7	10	10	06	06.7	00.2	05.1	.	.	$\bullet 00^10-10^30; F_{SE} 00^40$
26	6	10	10	07	05.0	00.0	01.8	.	.	$\bullet 00^10-08^30; \approx 08^30-19^30, F_{W} 11^57; \approx 01^20-24$
27	7	00	02	03	01.7	11.6	00.2	.	.	$\approx 00^10-08^30, 20^15-24$
28	8	00	02	00	00.7	12.0	.	.	.	$\approx 00^20-08^30, 21^15-24$
29	8	09	08	04	07.0	04.2	.	.	.	$\approx 00^10-08^30; \bullet 12^55-13$
30	8	10	06	00	05.3	06.9	00.1	.	.	$\bullet 03^45-4; 6^15-17^30; \approx 01^19-24$
MES.										
WRED.		06.9	07.4	05.8	06.7	147.8	52.3			

Б. 51.172

$H_s = 132 \text{ m}$ $H_D = 131.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dies	7	7	
1	8	000	000	00	00.0	12.3	00.0	.	$\Delta^{0-10-8^{30}}$
2	8	050	050	06	06.0	09.5	.	.	$\Delta^{0-10-7^{45}} 20^{30} 22^{30}$
3	8	010	050	07	05.7	05.5	.	.	$\Delta^{0-11^{30}}$
4	8	000	060	03	03.0	10.2	00.0	.	$\Delta^{0-10-7^{30}} 20^{30} 24$
5	8	020	020	02	02.0	11.0	.	.	$\Delta^{0-10-7^{45}} 22^{45} 24$
6	8	010	070	08	05.3	09.5	.	.	$\Delta^{0-10-8^{45}} 23^{15} 24$
7	8	09	10	10	09.7	03.5	.	.	$\Delta^{0-10-6^{45}} 22^{30} 24$
8	8	08	020	04	05.0	10.0	.	.	$\Delta^{0-10-7^{30}} 18^{02} 18^{10} 18^{05} 18^{20} F_{NW} 20^{46}$
9	8	050	10	10	08.3	01.3	00.2	.	$\Delta^{0-13^{45}} 24$
10	8	10	10	10	10.0	00.0	11.6	.	$\Delta^{0-10-24} F_{NW} 8^{05} 19^{40} F_{NW} 15^{08}$
11	8	10	10	05	06.3	00.8	25.9	.	$\Delta^{0-14^{30}} = 05^{30} 15^{30} F_{NW} 21^{62}$
12	7	10	050	10	08.2	03.8	03.8	.	$\Delta^{0-3^{45}} 9^{45}$
13	7	060	040	00	03.3	10.5	00.0	.	$\Delta^{0-20-24}$
14	8	000	030	00	01.0	12.6	.	.	$\Delta^{0-10-10^{30}} 19^{45} 24$
15	8	000	040	00	01.3	11.6	.	.	$\Delta^{0-10-9^{45}} 20^{15} 24$
16	7	05	10	07	06.7	00.0	.	.	$\Delta^{0-10-7^{45}} 10^{45} 16^{30}$
17	7	10	05	01	06.7	04.4	00.1	.	$\Delta^{0-7^{35}} 9^{45} 11^{30} 14^{20} \Delta^{0-14^{58}} 15^{03}$
18	7	020	10	09	07.0	08.8	00.6	.	$\Delta^{0-20-0^{30}}$
19	8	020	060	08	05.3	10.8	.	.	$F_{SE-ESE} 4^{52} 8^{35} 24$
20	8	040	050	02	03.7	11.0	.	.	$F_{SE} 0-4^{53} \Delta^{0-19^{30}} 24$
21	8	060	030	01	03.3	12.0	.	.	$\Delta^{0-10-7^{30}} 20^{30} 24$
22	8	010	000	01	00.7	12.6	.	.	$\Delta^{0-10-7^{30}} 21^{30} 24$
23	8	020	050	07	04.7	10.6	.	.	$\Delta^{0-10-9^{45}} 17^{30} 22^{45} 24$
24	8	010	030	00	01.3	12.0	.	.	$\Delta^{0-10-11^{30}} 10^{30} 23^{30} 24 F_{NW} 15^{03} 16^{20}$
25	8	010	070	06	04.7	12.1	.	.	$\Delta^{0-10-7^{30}} F_{NW} 10^{40} 15^{45} 19^{32}$
26	7	060	10	05	08.3	03.5	.	.	$\Delta^{0-10^{30}} 6^{15} \Delta^{0-11^{58}} 14^{20} 17^{45} 17^{55} F_{WNW} 12^{46} 14^{48} \Delta^{0-13^{45}} 14^{45} 16^{55} 20^{45} 18^{15}$
27	7	10	10	10	10.0	00.0	04.5	.	$\Delta^{0-3^{45}} 5^{45} 12^{25} 14^{30} = 05^{45} 6^{30}$
28	7	10	05	09	09.3	01.5	00.3	.	$\Delta^{0-10^{30}} 22^{10} \Delta^{0-20^{50}} 21^{49}$
29	8	000	050	00	01.7	13.2	01.1	.	$\Delta^{0-23^{30}} 24$
30	8	000	070	01	02.7	11.2	.	.	$\Delta^{0-10-9^{30}} 21^{15} 24$
31	8	060	040	05	05.0	10.4	.	.	$\Delta^{0-10-8^{45}} 20^{15} 24$
MES.									
VRD.		04.4	06.2	04.5	05.2	246.3	48.5		

РЕЦЕНА

1973 JUN

1	8	000	010	00	00.1	13.5	.	.	$\Delta^{0-10-7^{30}} 19^{45} 24$
2	8	000	010	00	00.3	12.5	.	.	$\Delta^{0-10-7^{45}}$
3	8	000	080	02	03.2	09.2	.	.	$\Delta^{0-10^{30}} 10^{15} 15^{30} 19^{30} 17^{15} \Delta^{0-16^{40}} 17^{45}$
4	8	10	10	10	10.0	01.3	00.2	.	$\Delta^{0-11^{30}} 14^{15} \Delta^{0-22^{30}} 24$
5	8	09	080	00	05.7	05.6	04.5	.	$\Delta^{0-10-7^{30}} \Delta^{0-17^{45}} 20^{10} 17^{50} 19^{45} F_{ESE} 18^{08} 22^{10}$
6	8	040	050	04	04.3	09.2	.	.	$\Delta^{0-13^{45}} 4^{20} \Delta^{0-7^{01}} 8^{10} 23^{15} 24$
7	7	060	06	00	04.7	08.9	00.5	.	$\Delta^{0-10-4^{08}} F_{NW} 4^{02} 4^{20} \Delta^{0-2^{40}} 4^{32} 17^{40} 17^{48} 18^{12} 14^{40} 16^{55} 22^{15} \Delta^{0-12^{17}} 21^{15}$
8	8	040	020	09	05.0	09.0	16.1	.	$\Delta^{0-2^{08}} 2^{35} 11^{08} 16^{55} 17^{30} 17^{42} 05^{35} 16^{58} 18^{15} F_{NW} 4^{14} 23^{35} 16^{21} \Delta^{0-2^{32}} 5^{18} 22^{15} \Delta^{0-17^{45}} 22^{15}$
9	8	10	080	09	09.0	04.9	35.7	.	$\Delta^{0-12^{40}} 8^{40} 12^{15} 17^{30} 20^{30} = 05^{40} 13^{36} \Delta^{0-23^{15}} 7^{15} 15^{10} 16^{15} F_{ESE-SW} 5^{03} 16^{15}$
10	7	10	05	10	09.7	00.0	13.7	.	$\Delta^{0-19^{30}} 24$
11	7	060	040	05	05.0	10.4	02.4	.	$\Delta^{0-10-7^{30}} 19^{45} 24$
12	7	06	050	00	03.7	10.4	.	.	$\Delta^{0-20-2^{45}} 20^{30} 24$
13	7	000	040	00	01.3	11.6	.	.	$\Delta^{0-20-8^{30}}$
14	8	000	040	00	01.3	11.5	.	.	$F_{WNW-NW} 10^{17} 6^{07} 11^{32} 15^{02} \Delta^{0-23^{30}} 8^{45}$
15	7	10	05	04	07.7	02.2	00.4	.	$F_{WNW} 7^{03} 11^{15} \Delta^{0-19^{45}} 24$
16	8	000	060	04	03.3	10.2	02.5	.	$\Delta^{0-10-7^{30}} 20^{15} 24 F_{WNW} 9^{32} 11^{04}$
17	8	010	070	02	03.3	08.5	.	.	$\Delta^{0-10-8^{30}} F_{W} 12^{09} 15^{32} T^{0-13^{10}} 13^{20} \Delta^{0-2^{13}} 14^{29} \Delta^{0-18^{55}} 21^{15}$
18	8	000	080	10	06.0	09.2	.	.	$\Delta^{0-3^{30}} 7^{36}$
19	7	030	050	07	05.0	09.2	05.1	.	$\Delta^{0-23^{30}} 6^{30}$
20	8	010	040	03	02.7	12.5	.	.	$\Delta^{0-3^{30}} 8^{30}$
21	8	000	090	10	06.3	08.4	.	.	$\Delta^{0-3^{30}} 8^{30} \Delta^{0-18^{20}} 18^{40} 21^{05} 22^{15}$
22	8	05	060	00	05.0	09.6	00.8	.	$\Delta^{0-23^{30}} 7^{36} F_{NE} 17^{53} 18^{20}$
23	8	10	050	08	07.7	07.0	.	.	$\Delta^{0-10^{30}} 23^{00} F_{NW} 9^{36} \Delta^{0-14^{55}} 15^{15} 23^{45} 24 \Delta^{0-20^{15}} 21^{15}$
24	8	060	05	09	06.0	07.8	00.0	.	$\Delta^{0-13^{15}} 14^{15} \Delta^{0-13^{30}} 14^{20} 20^{30} 23^{15}$
25	8	10	10	08	09.3	02.8	00.8	.	$\Delta^{0-11^{05}} 16^{15}$
26	7	10	040	03	05.7	11.0	00.8	.	$\Delta^{0-24^{30}} 13^{30} \Delta^{0-19^{30}} 24$
27	8	000	030	00	01.0	13.2	.	.	$\Delta^{0-20-0^{45}}$
28	8	000	040	05	03.0	12.6	.	.	$\Delta^{0-23^{30}} 7^{36} \Delta^{0-21^{30}} 24$
29	8	030	020	10	05.0	12.0	.	.	$\Delta^{0-10-8^{15}} 18^{21} 23^{15} \Delta^{0-21^{40}} 24 \Delta^{0-21^{50}} 23^{10}$
30	8	09	080	01	06.0	06.5	03.3	.	$\Delta^{0-0-0^{45}} 2^{45} 3^{15}$
MES.									
VRD.		04.6	05.5	04.4	05.0	261.4	87.2		

BE. 51.172

H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9		Oblačnost N (0—10)				Intencija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies					
1	F	06	060	05	07.0	08.3	.	.	.	.
2	7	10	060	06	07.3	06.1	.	.	.	.
3	7	10	050	05	05.3	01.7	.	.	.	.
4	E	05	050	05	07.7	09.1	00.1	.	.	.
5	7	05	100	05	06.0	03.6	.	.	.	.
6	7	020	080	00	03.3	10.1	02.5	.	.	.
7	8	10	010	06	05.7	06.4	00.0	.	.	.
8	7	040	050	07	05.3	05.0	00.4	.	.	.
9	7	010	030	03	02.3	11.6	02.0	.	.	.
10	E	050	060	00	04.3	09.0	.	.	.	.
11	8	050	060	03	04.7	10.5	.	.	.	.
12	7	010	050	00	02.0	10.4	.	.	.	.
13	7	000	060	08	04.7	07.1	.	.	.	.
14	8	000	040	04	02.7	11.4	01.4	.	.	.
15	E	040	030	05	04.0	10.9	.	.	.	.
16	E	000	030	00	01.0	13.3	01.0	.	.	.
17	H	000	010	00	00.3	12.3	.	.	.	.
18	E	020	000	02	01.3	10.7	.	.	.	.
19	E	000	040	03	02.3	12.8	00.0	.	.	.
20	E	050	050	00	04.7	08.0	00.4	.	.	.
21	8	000	010	00	00.3	13.1	.	.	.	.
22	E	000	030	02	01.7	12.7	.	.	.	.
23	8	040	050	04	04.3	08.7	14.2	.	.	.
24	8	010	080	10	06.3	06.9	.	.	.	.
25	7	10	08	10	05.3	04.5	08.0	.	.	.
26	E	040	060	06	05.3	10.3	.	.	.	.
27	E	060	09	03	06.0	06.9	.	.	.	.
28	E	05	060	03	06.0	07.2	00.1	.	.	.
29	7	10	10	03	07.7	01.1	00.2	.	.	.
30	7	09	070	00	05.3	07.5	00.2	.	.	.
31	7	010	050	00	02.0	11.9	.	.	.	.
MES.										
VRED.	04.5	05.4	03.9	04.6	274.1	30.5				

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1973 AVUGST

1	8	06	060	00	04.7	06.2	.	.	.	.
2	8	000	010	01	00.7	12.2	.	.	.	.
3	7	060	09	10	08.3	02.0	.	.	.	.
4	E	10	060	10	08.7	03.5	00.0	.	.	.
5	E	09	040	00	04.3	08.1	05.5	.	.	.
6	7	000	040	00	01.3	11.1	.	.	.	.
7	8	000	060	00	00.0	12.2	.	.	.	.
8	7	000	050	07	04.0	08.4	.	.	.	.
9	7	010	040	00	01.7	12.4	.	.	.	.
10	E	000	000	00	00.0	12.0	.	.	.	.
11	8	000	000	00	00.0	12.5	.	.	.	.
12	E	000	000	05	01.7	12.3	.	.	.	.
13	E	000	030	05	04.0	10.2	.	.	.	.
14	E	060	060	01	04.3	09.4	01.7	.	.	.
15	E	080	040	00	04.0	10.3	00.0	.	.	.
16	E	000	050	03	02.7	11.2	.	.	.	.
17	E	000	08	05	05.7	08.7	.	.	.	.
18	E	050	050	00	03.3	10.6	00.0	.	.	.
19	E	09	040	00	04.3	09.1	00.0	.	.	.
20	8	000	050	00	01.7	11.7	00.0	.	.	.
21	E	040	010	00	01.7	11.5	.	.	.	.
22	6	000	040	00	01.3	08.5	.	.	.	.
23	7	000	050	06	03.7	09.1	.	.	.	.
24	7	070	050	10	07.9	07.8	.	.	.	.
25	E	000	000	00	00.0	08.9	03.5	.	.	.
26	7	08	080	10	08.7	06.2	00.7	.	.	.
27	7	10	10	09	09.7	00.0	00.0	.	.	.
28	7	10	09	10	09.7	01.4	18.6	.	.	.
29	7	10	10	10	10.0	00.0	05.8	.	.	.
30	7	10	040	05	07.7	03.1	10.4	.	.	.
31	E	05	070	04	06.7	05.5	03.4	.	.	.
MES.										
VRED.										
			04.2	04.6	04.0	04.2	256.1	50.4		

BR. SI. 172

$$H_s = 132 \text{ m } H_b = 131.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Valjivost 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	7	010	100	09	06.7	03.6	.	.	$\Delta 02^{30} 09^{30}$
2	7	000	040	00	01.3	10.7	.	.	$\Delta 0-1 130 8^{45} 20^{15} 24$
3	8	000	020	00	00.7	10.9	.	.	$\Delta 0-2 0-8 19^{45} 24$
4	8	000	000	00	00.0	11.4	.	.	$\Delta 0-10-8^{45} 19^{45} 24$
5	8	000	010	00	00.3	11.3	.	.	$\Delta 0-2 0-8^{30} 20-24$
6	8	000	010	00	00.3	11.0	.	.	$\Delta 0-0-8^{30} 20-24$
7	8	000	020	00	00.7	10.6	.	.	$\Delta 0-10-8^{15} 20^{45} 24$
8	8	000	000	00	00.0	09.7	.	.	$\Delta 0-20-8^{30} 19^{45} 24$
9	7	030	050	00	02.7	09.7	.	.	$\Delta 0-2 0-8^{45} 23^{15} 24$
10	8	000	020	09 R	03.7	10.1	.	.	$\Delta 0-10-8^{45} 19^{45} 20^{25} 21^{45} 22^{25} 21^{45} F_{www} 20^{34} 21^{45} 20^{45} 21^{40} 0-2 23^{40} 24$
11	7	09	020	00	03.7	06.9	10.5	.	$\Delta 0-2 0-3^{45} 0-1 19^{45} 24$
12	7	030	060	00	03.0	10.0	.	.	$\Delta 0-10-8^{45} 19^{45} 24$
13	8	05	05	06	06.7	02.8	.	.	$\Delta 1-2 0-8^{45} 20^{30} 24$
14	8	040	030	00	02.3	08.2	.	.	$\Delta 1-2 0-8^{45} 19^{45} 24$
15	8	000	000	00	00.0	09.8	.	.	$\Delta 0-2 0-8^{30} 19^{30} 24$
16	7	04	000	00	01.3	09.5	.	.	$\Delta 0-10-8^{15} 19^{30} 24$
17	8	030	07	10	06.7	06.0	.	.	$\Delta 0-10-8^{45} 0-1 16^{30} 22^{30}$
18	7	09	060	10	08.3	09.2	04.6	.	$F_{SE} 12^{37} 21^{50} F_{ESE} 21^{30} 24$
19	8	10	05	06	08.3	00.1	.	.	$F_{ESE} 0-17^{03} 0-2 25 0^{35} F_{ESE} 17^{03} 22^{20}$
20	7	10	10	00	06.7	00.8	05.5	.	$\Delta 0-10^{15} 9^{00} 0-1 19-24$
21	8	000	000	03	01.0	10.1	00.4	.	$\Delta 1-2 0-9^{30}$
22	8	000	070	10	05.7	07.9	.	.	$\Delta 1-2 2-8^{30} 0-2 15^{57} 17^{45} 19^{27} 23^{35} 0-2 16^{20} 16^{45} 19^{45} 21^{11} F_{NW} 16^{37}$
23	8	10	070	00	05.7	06.0	25.8	.	$\Delta 0^{45} 7^{15} 0-1 19^{30} 24$
24	8	09	090	05	07.7	04.5	00.0	.	$\Delta 1-2 0-8^{30} F_{ESE} 17^{45} 24$
25	8	09	060	05	06.7	06.3	.	.	$F_{SE} 0-4^{11} 6^{24} 9^{56} 0-2 19^{30} 24$
26	7	10	09	10	09.7	03.2	.	.	$\Delta 0-2 0-9 18-24 = 20^{20} 24$
27	6	10	10	10	10.0	00.0	.	.	$\Delta 0-10-8^{30} = 0-4 0-15^{30} 0-1 14^{35} 15^{15} 18^{45} 24$
28	6	10	10	10	10.0	00.0	04.9	.	$\Delta 0-3^{40} 1 = 0^{40} 24 0-6^{30} 9^{30} 14^{55} 16^{30}$
29	7	10	060	00	05.3	03.8	00.1	.	$\Delta 0-10^{30} 0-1 21^{30} 24$
30	8	000	020	00	00.7	09.9	.	.	$\Delta 0-2 0-9^{30} 19-24$
MES.									
MRED.		04.3	04.8	03.4	04.2	210.6	51.9		

1	8	C20	030	CC	C1.7	C9.3	.	.	$\Delta^{0-2} 0-10^{30} 19^{15} 24; \equiv 0^{130} 7^{45}$
2	7	000	030	CC	C1.0	C6.5	.	.	$\Delta^{0-2} 0-8^{36} 19^{30} 24; \equiv 0^{130} 7^{45}$
3	6	C9	10	10	C9.7	C0.0	.	.	$\Delta^{0-2} 0-0^{36} \equiv 2^{030} 1^{45} \equiv 2^{145} 4^{30} \equiv 2^{1430} 24$
4	7	10	030	CC	C4.3	C8.5	.	.	$\Delta^{0-2} 0-13^{16} \Delta^{0-1} 4^{15} 7^{45} 19^{45} 24$
5	7	000	000	CC	C0.0	C8.4	.	.	$\Delta^{0-1} 0-8^{36} 22^{45} 24$
6	8	00	000	00	C0.0	10.1	.	.	$\Delta^{0-1} 0-8^{30} 19^{30} 24$
7	8	000	000	CC	C0.0	10.0	.	.	$\Delta^{0-2} 0-8^{45} 22^{30} 24$
8	8	040	070	C3	C4.7	C7.7	.	.	$\Delta^{0-2} 0-6^{30} F_{ESE} 9^{10} 12^{45}$
9	8	050	020	C4	C3.7	C8.2	.	.	$\Delta^{0-2} 0^{45} 24 \equiv 0^{2215} 24$
10	6	10	000	CC	C3.3	C5.6	.	.	$\Delta^{0-2} 0-4^{30} 19^{45} 24; \equiv 0^{22} 0-4^{20} 9^{30} 22^{15}; \equiv 1^{420} 9^{30}$
11	6	C0	010	CC	C0.3	C9.3	.	.	$\Delta^{0-2} 0-9^{30} 19^{30} 24; \equiv 1^{545} 15^{30}$
12	7	C8	030	10	C7.0	C6.2	.	.	$\Delta^{0-1} 0-6^{45} 2^{130} 24; \equiv 0^{645} 1^{30} F_{N-NW} 15^{00} 20^{10}$
13	7	10	08	C3	C7.0	C2.5	.	.	$\Delta^{0-1} 0-8^{45} 20^{45} 24; \equiv 0^{10} 0-7^{30} F_{ESE} 3^{35} 4^{10} 7^{44} 24$
14	8	C10	080	C2	C3.7	C5.6	.	.	$\Delta^{0-1} 45 1^{45} 1^{30} 13^{45} 22^{45} 23^{40} F_{S} 15^{52} 16^{23} 9^{16} 16^{25}$
15	8	C8	09	C7	C8.0	C4.5	C0.1	.	$\Delta^{0-1} 4^{15} 8^{30} 0^{13} 15 F_{S} 19^{38} 2^{125}$
16	8	010	10	00	C3.7	C6.1	CC.4	.	$\Delta^{0-1} 19^{45} 24$
17	8	C9	020	01	C4.0	C6.0	00.0	.	$\Delta^{0-1} 6^{45} F_{N} 13^{40} 14^{35} 17^{04} 18^{52}; \Delta^{0-1} 13^{40} 14^{45}; 16^{45} 21^{15}; 6^{17} 15 17^{58} 17^{45} 17^{50} 8^{0-2} 17$
18	8	09	10	10	C9.7	C6.5	14.3	.	$\Delta^{0-2} 0^{30} 24$
19	8	04	000	00	C1.3	C9.7	14.3	.	$\Delta^{0-2} 0^{30} 24$
20	8	C2	050	C5	C4.0	C7.2	.	.	$\Delta^{0-2} 0-9^{45} 19^{30} 24$
21	8	C6	10	C7	C7.7	C0.0	.	.	$\Delta^{0-2} 0-8^{30} F_{SE} 10^{25} 15^{50}; 6^{18} 15 19^{25} 10^{19} 10^{25} 13^{0-2} 22^{45} 24; 8^{0-2} 22^{50} 24$
22	6	10	10	C2	C7.3	CC.0	15.7	.	$\Delta^{0-1} 0-13^{0-130} 0^{130} 13^{40} 6^{50} 13^{50}; 9^{130} 14^{45} F_{NW} 13^{43} 15^{25}$
23	7	020	040	00	C2.0	C8.7	C1.4	.	$\Delta^{0-1} 0^{30} 5^{45} 20^{15} 24; \Delta^{0-1} 5^{15} 7^{30}$
24	7	10	10	10	C0.0	C0.0	.	.	$\Delta^{0-2} 0-7^{45}; 0^{745} 14^{45} 20^{30} 22^{30}; 0^{18} 45 19^{30} F_{NNE} 20^{04}$
25	7	10	05	C6	C6.3	C4.5	CC.3	.	$\Delta^{0-2} 0-9^{45} 19^{30} 24$
26	7	C30	000	C2	C1.7	C8.6	.	.	$\Delta^{0-2} 0-8^{45} 12^{30} 24; \Delta^{0-1} 8^{45} 24$
27	6	C0	000	CC	CC.0	C7.8	.	.	$\Delta^{0-2} 0-8^{45} 12^{30} 24; \Delta^{0-2} 5^{45} 19^{30} \Delta^{0-1} 19^{45} 23^{15}$
28	5	CC	020	CC	CC.7	C8.1	.	.	$\Delta^{0-2} 0-9^{30} \equiv 1^{2} 5^{45} 19^{30} \equiv 5^{45} 6^{30} \Delta^{0-1} 19^{45} 24$
29	7	CC	000	CC	C0.0	C8.7	.	.	$\Delta^{0-2} 0-8^{45} \equiv 5^{45} 8^{30} 18^{30} 20^{45} \Delta^{0-1} 17^{45} 20^{45} \equiv 0^{2} 20^{45} 21^{30} \equiv 2^{1430} 24$
30	6	10	080	10	C5.3	C2.4	.	.	$\Delta^{0-2} 0-8^{36} \equiv 1^{850} 10^{15} \equiv 2^{10} 24; F_{W} 14^{48}$
31	7	10	070	08	C8.3	C2.1	.	.	$\Delta^{0-2} 0-12^{15}$
MES.									
PRE.	C4.9	C4.6	C3.2	C4.3	189.6	32.2			

BR. ST. 172

$H_s = 132 \text{ m}$ $h_b = 131.6 \text{ m}$ $h_l = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inselacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	7	CC	CC	CC	CC.C	09.C	.	.	$\angle 03^30-8^45 23^45 24$
2	6	CC	CC	CC	CC.C	08.2	.	.	$\angle 01^0-10^30 21^30 24$
3	6	CC	CC	CC	CC.C	09.C	.	.	$\angle 01^0-9^30 22^45 24$
4	6	CC	CC	CC	CC.C	08.7	.	.	$\angle 01^0-0^45 FSE 4^30 24, FSE 22^5$
5	6	CC	CC	CC	CC.C	08.6	.	.	$FSE 0-5^05, \angle 02^30 24$
6	6	CC	CC	CC	CC.C	07.C	.	.	$\angle 00^0-6^30 FSE 22^30 24, \angle 02^30 24$
7	7	CC	CC	CC	CC.C	08.1	.	.	$\angle 00^0-0^30 FSE NNE-NNW 0^30 23^30 24, 13^59, 16^45, \angle 07^30 18^30, \angle 02^19 30 24$
8	6	CC	CC	CC	CC.C	08.5	.	.	$\angle 00^0-24$
9	6	CC	CC	CC	CC.C	08.5	.	.	$\angle 00^0-24, \angle 03^30 4^30, \angle 04^30 8^30$
10	6	CC	CC	CC	CC.C	08.5	.	.	$\angle 00^0-24, \angle 04^30 8^30, \angle 05^30 9^15, \angle 05^45 21^30, \angle 02^19 30 24$
11	7	CC	CC	CC	CC.C	08.2	.	.	$\angle 01^0-8^30 22^30 24, \angle 06^45 9^30, \angle 08^45 22^30$
12	4	CC	CC	CC	CC.C	08.2	.	.	$\angle 01^0-7^45, \angle 24^30 5^45, \angle 12^30 24, \angle 05^45 12^30, \angle 06^20 6^50, \angle 02^05 24$
13	5	CC	CC	CC	CC.C	08.7	.	.	$\angle 00^0-5^30 7^45 24, \angle 01^0-0^45, \angle 00^45 9^15, \angle 02^30 7^40, \angle 06^45 7^15, 9^30 10^30$
14	5	CC	CC	CC	CC.C	08.7	.	.	$\angle 00^0-24, \angle 02^15 23^15$
15	7	CC	CC	CC	CC.C	08.6	.	.	$\angle 00^0-10^30, FSE 15^45, \angle 02^30 24$
16	7	CC	CC	CC	CC.C	08.7	.	.	$\angle 00^0-11^05, 13^45, FSE 22^45$
17	7	CC	CC	CC	CC.C	08.5	.	.	$\angle 04^20 9^30, \angle 01^0-17^45 22^30, \angle 02^30 24$
18	6	CC	CC	CC	CC.C	08.1	.	.	$\angle 00^0-9^30 22^30 24$
19	7	CC	CC	CC	CC.C	08.2	.	.	$\angle 01^0-9^30, FSE 6^50, 11^20, \angle 02^45 24$
20	7	CC	CC	CC	CC.C	08.0	.	.	$\angle 00^0-6^45 20^30 24, \angle 06^45 8^30$
21	7	CC	CC	CC	CC.C	08.1	.	.	$\angle 00^0-13^05, \angle 01^0-9^30 21^30 24, FSE NW 9^24, 14^40, FSE NW 10^24, 11^13$
22	7	CC	CC	CC	CC.C	07.5	.	.	$\angle 00^0-0^45, \angle 06^15 11^30$
23	7	CC	CC	CC	CC.C	07.5	.	.	$\angle 00^0-0^30 8^45, \angle 06^45 12^30$
24	7	CC	CC	CC	CC.C	07.5	.	.	$\angle 00^0-8^45$
25	7	CC	CC	CC	CC.C	07.2	.	.	$\angle 00^0-17^45 18^55, FSE NW 17^40, 17^47$
26	6	CC	CC	CC	CC.C	08.0	.	.	$\angle 00^0-12, FSE NW 10^04, \angle 01^0-12^30 13^45, 18^45 24, \angle 02^30 24$
27	7	CC	CC	CC	CC.C	08.7	.	.	$\angle 00^0-10^30, \angle 02^30 24$
28	6	CC	CC	CC	CC.C	08.0	.	.	$\angle 00^0-5^30 17^45, \angle 08^45 24, \angle 02^30 24$
29	7	CC	CC	CC	CC.C	08.0	.	.	$\angle 00^0-10^30, \angle 01^0-20^45 24, \angle 02^30 24$
30	6	CC	CC	CC	CC.C	08.5	.	.	$\angle 00^0-10^30, \angle 01^0-13^15, \angle 01^0-13^45 16^30, \angle 02^30 24$
PES.									
MEC.		05.9	05.6	04.5	05.4	126.6	48.5		

1	6	CC	CC	CC	CC.C	01.2	13	[X]
2	7	CC	CC	CC	CC.C	00.0	11	[X]
3	7	CC	CC	CC	CC.C	02.2	11	[X]
4	7	CC	CC	CC	CC.C	02.0	11	[X]
5	7	CC	CC	CC	CC.C	00.3	11	[X]
6	7	CC	CC	CC	CC.C	00.4	10	[X]
7	7	CC	CC	CC	CC.C	00.2	06	[X]
8	7	CC	CC	CC	CC.C	00.0	03	[X]
9	6	CC	CC	CC	CC.C	00.4	02	[X]
10	7	CC	CC	CC	CC.C	07.0	.	[X]
11	7	CC	CC	CC	CC.C	06.7	.	[X]
12	7	CC	CC	CC	CC.C	05.6	.	[X]
13	7	CC	CC	CC	CC.C	05.9	.	[X]
14	6	CC	CC	CC	CC.C	05.2	.	[X]
15	6	CC	CC	CC	CC.C	00.0	00.2	[X]
16	6	CC	CC	CC	CC.C	02.3	03.6	[X]
17	6	CC	CC	CC	CC.C	02.3	01	[X]
18	7	CC	CC	CC	CC.C	08.3	00.0	[X]
19	7	CC	CC	CC	CC.C	06.7	00.0	[X]
20	6	CC	CC	CC	CC.C	05.4	.	[X]
21	6	CC	CC	CC	CC.C	05.0	.	[X]
22	6	CC	CC	CC	CC.C	03.2	.	[X]
23	7	CC	CC	CC	CC.C	07.1	.	[X]
24	6	CC	CC	CC	CC.C	05.4	.	[X]
25	6	CC	CC	CC	CC.C	07.7	.	[X]
26	6	CC	CC	CC	CC.C	00.7	00.0	[X]
27	7	CC	CC	CC	CC.C	00.0	03.0	[X]
28	6	CC	CC	CC	CC.C	06.0	00.1	[X]
29	7	CC	CC	CC	CC.C	00.0	.	[X]
30	7	CC	CC	CC	CC.C	00.6	00.0	[X]
31	7	CC	CC	CC	CC.C	01.3	.	[X]
PES.								
MEC.		06.2	07.0	05.3	06.2	95.5	29.0	

BR. ST. 247

 $H_s = 52 \text{ m}$ $H_b = 52.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijest 0-9	Oblačnost N (0-10)				Inzolucija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	6	05	05	07	06.3	01.0	.	.	
2	7	10●	10●	10●	10.0	00.0	.	.	● 7-24
3	7	10●	10	10	10.0	00.5	15.2	.	● 0-7 ⁴⁰ 23-24
4	7	10≡	05○	02	07.0	02.3	01.5	.	● 0-6 ¹⁰ ≡ 11-10, Δ 17 ³⁰ 23 ³⁰
5	6	05	05	00	06.0	00.4	.	.	≡ 0 ⁰⁵ 5 ⁴⁵ i, 8 ²⁰ 20 ²⁰ i
6	6	00	04○	01	03.7	03.6	.	.	≡ 17 ⁰⁵ 21 ²⁰ i
7	6	00	03○	00	01.0	06.2	.	.	⊥ 11-8
8	6	00	00○	00	00.0	07.1	.	.	⊥ 11-9
9	6	00	00○	00	00.0	06.9	.	.	⊥ 11-9 ³⁰
10	6	00	01○	00	00.3	07.1	.	.	⊥ 11-10
11	6	01	03○	04	02.7	06.1	.	.	⊥ 11-10, ≡ 21 ⁴⁰ 23, ≡ 23-24
12	6	01	00○	00	00.3	06.5	.	.	≡ 0-4 ²⁰ ≡ 4 ²⁰ 24
13	6	00	00○	00	00.0	06.7	.	.	≡ 0-18 ²⁰ 21 ⁴⁰ 24; ≡ 18 ²⁰ 21 ⁴⁰
14	6	00	00○	00	00.0	08.9	.	.	≡ 0-3 ¹⁰
15	6	05	10	10	05.7	00.0	.	.	● 22 ⁴⁰ 23 ⁴⁰
16	6	10	10●	10●	10.0	00.0	00.0	.	● 07 ⁵⁰ 9, 13-24, ● 9-13, 18 21-22 ³⁰
17	6	10	05	10	05.7	00.0	34.0	.	● 0-13 ⁴⁰ 4 ⁴⁰ 12 ¹⁰ 22 ²⁰ 24
18	6	10●	10●	10●	10.0	00.0	03.5	.	● 0-24 i, ≡ 17-23 ³⁰ 24
19	7	10	10●	10●	10.0	00.0	64.2	.	● 0-24 i, ≡ 0 ⁰⁵ 2 ³⁵ 18 ⁴⁰ 8, 20 ¹⁰ 24 i
20	7	10	10	10	10.0	00.0	58.2	.	● 0-3, 14 ²⁰ 18 ²⁰ i
21	7	10	10	10●	10.0	00.7	00.6	.	● 7 ⁰⁵ 7 ³⁰ 19 ¹⁰ 21 ³⁰
22	7	10●	10●	10	10.0	00.0	12.0	.	● 15 9 ⁴⁰ 13 ³⁰ 18 i
23	7	10●	10	10≡	10.0	00.0	01.3	.	● 4 ⁵⁰ 13 ⁴⁰ ≡ 19 ⁵⁵ 21
24	6	10≡	10	05	06.3	02.6	01.6	.	≡ 0-9 ⁴⁰ ≡ 21 ⁴⁰ 23 ⁴⁵
25	6	10	06○	00	06.0	06.1	.	.	≡ 4 ³⁰ 5, ≡ 5-23 ²⁵
26	6	05	04○	00	04.3	06.3	.	.	
27	6	10	10	10	10.0	00.0	.	.	
28	7	10●	10●	10	10.0	00.0	03.6	.	● 0 ⁴⁰ 10 i, ≡ 17 ⁵⁰ 24
29	6	05	05	00	06.0	00.1	06.7	.	≡ 0-24 i
30	6	06	03	10	07.0	00.1	.	.	≡ 0-4, ≡ 4-18 i
31	6	10	10	10	10.0	00.0	.	.	● 21 ⁴⁰ 24
MES.									
WREC.		07.1	06.6	05.4	06.5	05.4	205.1		

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1	7	10●	10	10●	10.0	00.0	12.6	.	● 0-14 ⁵⁰ i, 20 ¹⁵ 24
2	7	10≡	10●	04	06.0	00.0	24.1	.	● 0-5 ⁵⁰ 8 ⁴⁵ 14 i, 19-24, ≡
3	6	06	00	00	05.3	04.0	00.1	.	Δ 0-8, ≡ 15 ⁵⁵ 19 ³⁰ , ≡ 19 ³⁰ 24 i
4	8	00	00○	00	00.0	05.7	.	.	≡ 0 ⁵⁰ 24 i
5	6	00	00○	00	00.0	05.7	.	.	≡ 0-19 ⁴⁵ i
6	6	00	00○	00	00.0	05.7	.	.	⊥ 11-8, Δ 18-24
7	6	01	03○	00	01.3	05.7	.	.	Δ 0-7 ³⁰
8	6	00	03○	00	01.0	05.7	.	.	Δ 11-7 ³⁰
9	6	10	10	10	10.0	00.2	.	.	Δ 11-7 ³⁰
10	7	10	10●	10●	10.0	00.0	.	.	● 7 ¹⁵ 24 i
11	6	10●	10●	07	05.0	00.0	34.3	.	● 0-7 ²⁰ 11 ⁵⁰ 14 ³⁰ i, ≡ 0-5 ¹⁵ 12 ¹⁰ 13
12	8	10	10	00	06.7	03.0	04.2	.	≡ 7 ¹⁵ 13 ⁵⁵ 19 ²⁵ 12 ³⁰ i, ≡ 8 ⁵⁵ 19 ²⁵
13	6	00	04○	04	02.7	05.7	.	.	Δ 19-24, 19 ²⁵ 12 ³⁰ i
14	6	10	0	10●	10.0	00.0	.	.	Δ 0-19 ²⁰ 13 ⁴⁰ 16 ³⁰ 24, ≡ 18 ⁵⁵ 19 ⁴⁵ 20 ¹⁰ 24
15	6	10●	10●	10	10.0	00.0	22.3	.	● 2 0-14 ³⁰ i, 23 ²⁰ 24, ≡ 0-15 ⁴⁰ i, 18 1-24 i, Δ 12-13 ²⁰ i
16	6	10	10●	10●	10.0	00.0	30.5	.	● 0-24 i, 18 0-11 i, ≡ 3-7 ¹⁰ i, 14 ¹⁰ 16 ⁰⁵ , ≡ 4-4 ³⁰
17	7	10●	10●	10	10.0	00.0	62.2	.	● 0-8 ⁴⁰ 11 ⁰⁵ 19 ³⁰ i, ≡ 0-5 0 ²⁵ 4 ⁵⁰ 5 ⁴⁰ i
18	6	10	10	10	10.0	03.5	07.3	.	≡ 10 ⁰⁵ 12 ¹⁰
19	6	06	10	10●	05.3	00.7	.	.	● 11 ⁰⁵ 22 ¹⁵
20	6	06	10	00	06.0	02.0	00.2	.	≡ 11 ²⁰ 15 ²⁰ , ≡ 15 ²⁰ 24 i
21	6	00	04○	00	01.3	05.6	.	.	≡ 0-18 i
22	6	05	10	10	05.7	00.3	.	.	● 21 ⁵⁰ 24
23	6	10●	10	10	10.0	00.0	05.7	.	● 0-7 ⁵⁰ i, 12 ⁴⁰ 13 ²⁰
24	6	05	07○	04	06.7	03.4	06.8	.	
25	7	10*18	10	10	10.0	00.0	03.7	.	* 4 ⁴⁰ 11 ⁴⁰ i, 18 5 ³⁰ 9, ● 11 ⁴⁰ 13 ⁴⁰ , ≡ 14 ⁴⁰ 16 ¹⁵ , ≡ 16 ¹⁵ 24
26	6	10	05	00	06.3	06.5	14.6	.	≡ 0-14 ³⁰ i
27	6	00	06○	00	02.7	10.1	.	.	≡ 9 ⁴⁰ 23 ⁵⁰
28	6	10	10	10	10.0	00.0	.	.	≡ 0 ⁴⁵ 3, 9 ³⁰ 24 i
MES.									
WREC.		06.9	07.7	05.3	06.6	101.5	228.6		

BR. ST. 247

 $H_s = 52 \text{ m}$ $H_b = 52.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insekcija broj sati	Padavina R mm	Snežni pokrivac h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	8	C8	050	03	C5.3	C4.C	.	.	F 0-15 9 ⁴⁵ -16 ⁰⁵ ;
2	8	C5	080	00	C4.3	C5.6	.	.	F 22 ⁴⁵ ni
3	8	C8	10	05	05.0	03.4	.	.	F 12 ⁰⁰ -17 ⁰⁵ 20 ⁵⁰ 23 ¹⁰
4	8	00	030	03	02.C	C5.1	.	.	F 6-16 ⁰⁰ 22 ⁰⁰ -23 ¹⁵
5	8	C6	060	00	C4.C	C5.6	.	.	F 10 ⁵⁵ 16 ²⁵
6	8	C10	020	C8	C3.7	10.1	.	.	
7	8	10	10	10	10.C	04.7	.	.	• 18 ³⁰ 18 ⁴⁰ 19 ⁴⁵ 24
8	8	10	10	10	10.C	00.0	.	.	• 0-24 12 ¹⁵ -18 ¹⁵
9	8	10	10	10	10.C	00.4	59.0	.	• 0-14 ⁴⁰ 18 ⁰⁰ -3 F 13 ¹⁵ -14 ¹⁵
10	8	C8	080	10	C6.7	C8.1	C3.9	.	• 1 ⁰⁰ 2 ³⁰ F 9 ²⁰ -10 ²⁵ F 10 ²⁵ -24 ¹⁵
11	8	10	10	10	10.C	00.7	.	.	F 0-7 ²⁰ 13 ³⁰ -14 ³⁰ 18 ²⁰ -24; F 7 ²⁰ -13 ³⁰
12	8	000	C10	C9	C3.3	10.4	.	.	F 0-22 ¹⁵
13	8	10	10	10	10.C	00.0	.	.	F 1-12
14	8	C5	050	C4	07.3	06.7	.	.	
15	8	C5	C50	C4	06.C	C5.7	.	.	F 18 ⁴⁰ 24
16	8	C4	040	C5	04.3	C7.5	.	.	F 0-10 ³⁵
17	8	040	010	C4	C3.C	10.5	.	.	
18	8	10	10	10	10.C	06.7	.	.	F 13 ⁵⁰ 24
19	8	C7	05	00	C5.3	C0.1	.	.	F 0-4 ¹⁵ 13 ⁴⁰ -17 ¹⁵
20	8	000	010	00	00.3	11.2	.	.	F 7-22 ⁵⁰
21	8	000	000	00	00.C	11.2	.	.	
22	8	000	000	00	00.C	11.2	.	.	F 9 ⁰⁰ 10 ³⁰
23	8	000	000	C4	C1.3	10.7	.	.	
24	8	C5	10	10	C5.7	02.2	.	.	
25	8	10	10	10	10.C	00.C	.	.	• 10 ¹⁵ -10 ⁴⁰ 15-17 ³⁰ ;
26	8	10	040	10	08.0	04.2	C2.C	.	• 0 ⁴⁵ 8 ⁴⁵
27	8	C80	080	C3	C6.3	07.7	C0.3	.	
28	8	10	10	10	10.C	00.C	.	.	• 14 ⁴⁵ 23 ³⁰
29	8	10	05	10	C5.7	C3.5	C6.8	.	• 15 ³⁰ -23
30	8	09	080	10	C5.0	C5.7	C3.2	.	
31	8	C8	C70	C3	C6.C	06.1	.	.	• 17 ⁰⁵ 17 ⁴⁵
PES.									
WRED.		C6.5	C6.4	C6.1	C6.3	182.2	75.2		

1	8	10	080	00	C6.C	10.4	C0.3	.	
2	8	C0	C20	C0	C0.7	11.7	.	.	△ n-8
3	8	10	10	10	10.C	00.C	.	.	△ n-8 F 10 ³⁰ -17 ³⁰ • 13-13 ¹⁰ 18 ³⁰ -24; R 4 19 ¹⁰ -24
4	8	10	10	C1	C7.0	C0.1	28.2	.	• 0-12 ³⁰ 18 ⁴⁰ -4 ³⁰ F-F 15-24 ¹⁵
5	8	10	000	C0	C3.3	C2.4	10.C	.	F 0-12 ¹⁰ 21 ³⁰ -24; F 12 ³⁰ -21 ³⁰ ;
6	8	000	030	C0	C1.C	09.4	.	.	F 0-19 ⁰⁵
7	8	C80	C70	00	C5.C	10.5	.	.	
8	8	09	C30	C0	C4.C	05.3	.	.	
9	8	C8	080	10	C8.7	C1.5	.	.	△ n-8 F 13-16 ⁴⁵
10	8	10	10	10	10.C	C0.C	.	.	F 8 ⁴⁵ 11 ¹⁰ F 14 ²⁵ -16 ⁵⁰ 19-23 ³⁰ ;
11	7	10	10	10	10.C	C2.2	C5.2	.	• 19 ⁴⁰ -20 ¹⁰ 23-24
12	8	10	080	C6	08.0	C6.3	C7.6	.	• 0-15 ¹⁰ 20 ¹⁵ -22 ²⁰ F 0 ⁰⁵ 0 ¹⁰
13	8	10	10	C3	C7.7	C0.2	11.4	.	• 1-3 ⁴⁰ 17 ³⁰ -17 ³⁵
14	8	10	10	10	10.C	02.1	C8.5	.	• 0 ³⁰ -12 ⁴⁵ 16 ³⁰ -16 ³⁵ R 4-8 ¹⁵ F 7 ³⁰ 15 ¹⁵
15	8	10	10	C4	C8.C	C0.C	C0.3	.	• 7 ¹⁰ 11 ¹⁵
16	8	C30	10	10	C7.7	C4.4	C3.4	.	• 6-10 ³⁰ F 17 ⁴⁰ 18 ⁰⁵
17	8	C30	C40	C1	C2.7	C9.5	.	.	F 9 ³⁵ 15 ⁴⁰
18	8	000	000	C0	00.0	12.4	.	.	F 9 ¹⁰ ni
19	8	10	C50	10	C5.7	C6.2	.	.	
20	8	10	10	C6	C8.7	C2.C	C1.2	.	• 21 ⁰⁵ 21 ¹⁰
21	8	C60	10	10	C8.7	C4.1	C6.2	.	• 2-23 ¹⁰ F 11 ⁰⁵ 17 ⁵⁰ R 12 ⁴⁵ 17 ⁴⁰ ;
22	8	C8	C70	C0	C5.0	C7.1	C4.6	.	F 9 ⁴⁰ -18 ¹⁵ 12 ³⁰ -20 ²⁰ ;
23	8	C70	10	10	C5.C	C1.7	C3.1	.	• 17 ⁴⁵ 19 ¹⁵
24	7	10	10	10	10.C	C0.C	C0.8	.	• 16 ⁵⁵ 18 ³⁰
25	8	10	10	10	10.C	00.7	26.3	.	• 7 ³⁰ 24
26	8	10	10	03	C7.7	C0.1	C2.5	.	• 0-17 ⁴⁰ 23 ¹⁰ -23 ⁵⁰
27	8	C7	C60	C8	C7.0	C8.3	C0.1	.	• 12 ⁰⁵ 15 ¹⁰ 17 ⁴⁰ 18
28	8	10	C30	C0	C4.3	C1.5	.	.	△ n-8, • 17 ⁴⁵ 20 ³⁰ ;
29	8	10	10	10	10.C	C1.5	.	.	
30	8	C60	C00	C0	02.C	11.1	C2.2	.	• 12 ¹⁰ -12 ⁴⁰ 15 ¹⁰ -21 ²⁰
PES.									
WRED.		C7.8	07.3	05.1	06.7	145.8	128.2		

BR. ST. 247

$H_s = 52 \text{ m}$ $H_D = 52.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	8	000	000	00	00.0	13.3	.	.	.
2	8	040	040	00	02.7	12.1	.	.	.
3	8	000	080	03	03.7	07.6	.	.	• 23 ³⁰ 23 ⁴⁰
4	8	060	050	10	08.3	12.0	00.5	.	.
5	8	070	060	00	05.0	12.9	.	.	.
6	8	070	030	06	05.3	11.4	.	.	.
7	8	09	080	00	05.7	08.8	.	.	.
8	8	09	080	01	06.0	10.8	.	.	F 14-15 ⁵⁰ i
9	8	100	100	10	10.0	00.0	00.0	.	• 05 ⁴⁰ 24, F 23 ⁴⁰ 24
10	8	10	10	07	05.0	00.9	26.5	.	• 0-7 ³⁰ i, 12 ³⁰ 13 ⁴⁰ , F 0-6 ⁴⁰ 9 ⁴⁵ 11 ²⁰
11	8	020	05	00	03.7	11.6	00.1	.	.
12	8	080	070	10	08.3	10.7	.	.	F 19 ⁴⁰ 24
13	8	10	050	01	06.7	03.3	.	.	F 3 ³⁰ 12 ⁴⁰ 18 ⁵⁰ 24, F 12 ⁴⁰ 18 ⁵⁰
14	8	020	060	00	02.7	11.0	.	.	F 0-2 ⁴⁵ i
15	8	000	040	03	02.3	12.2	.	.	Δ n-8
16	8	00	040	01	01.7	09.1	.	.	Δ n-8 ³⁰
17	8	09	10	10	09.7	00.8	.	.	Δ n-7 ³⁰ , • 8-8 ⁴⁵ 14 ⁴⁰ 14 ⁵⁰ , F 21 ³⁰ 23 ²⁵
18	8	10	08	00	06.0	06.8	00.0	.	.
19	8	000	10	10	06.7	07.5	.	.	F 8 ²⁰ 16 ⁴⁵
20	8	080	000	00	02.7	12.4	.	.	.
21	8	050	050	00	03.3	13.2	.	.	.
22	8	020	080	00	02.3	11.0	.	.	.
23	8	020	040	00	02.0	13.1	.	.	.
24	8	000	020	00	00.7	12.7	.	.	.
25	8	010	030	00	01.3	12.7	.	.	F 5 ⁴⁰ 24i
26	8	000	06	00	02.0	12.6	.	.	F 0-20 ⁴⁰ i
27	8	000	040	03	02.3	13.6	.	.	F 4 ⁴⁰ 24i
28	8	020	050	06	04.3	12.2	.	.	F 0-1 ⁴⁰ i
29	8	07	070	07	07.0	07.1	.	.	R 15 ³⁰ 16, F 15 ³⁰ 16 ⁴⁰ i, • 15 ⁴⁰ 16
30	8	000	030	05	02.7	13.2	00.0	.	F 14 ³⁰ 19 ²⁵ , • 16 ⁴⁰ 16 ⁴⁵
31	8	070	080	07	07.3	08.6	.	.	.
PES.									
WRED.		04.4	06.1	03.2	04.6	305.2	27.5		

1	8	10	050	00	06.3	05.0	00.0	.	.
2	8	000	020	00	00.7	13.2	.	.	.
3	8	030	060	04	04.3	06.5	.	.	.
4	8	10	10	08	09.3	02.4	02.2	.	• 11 ³⁰ 12 ³⁰ i
5	8	080	070	03	06.0	09.4	.	.	.
6	8	070	080	00	05.0	08.4	.	.	.
7	8	020	030	07	04.0	12.2	.	.	F 10 ⁴⁰ 15 ⁵⁵ 21 ⁴⁰ 23 ²⁵
8	8	040	020	10	05.3	10.7	.	.	Δ 20-23 ³⁰ i, • 20 ⁴⁰ 23 ⁵⁰ 18 21 ⁴⁰ 24
9	8	10	070	10	09.0	03.1	02.7	.	• 6 ⁴⁵ 8 ³⁰ i, R 6 ²⁰ 9, F 10 ²⁰ 12 ²⁰
10	8	10	08	07	06.3	04.3	01.7	.	• 15 ⁵⁵ 16 ⁴⁰
11	8	040	08	02	04.7	08.8	01.1	.	F 9 ³⁰ 11 ⁴⁰
12	8	010	020	00	01.0	12.5	.	.	F 6-11 ²⁰
13	8	000	020	05	02.3	11.0	.	.	F 17 ³⁰ 18 ³⁵ 18 18 ⁵⁵ 19 ²⁰ Δ 20 ⁴⁰ 22i
14	8	08	100	04	07.3	02.8	.	.	R 10 ²⁵ 13, • 10 ⁴⁰ 14 ⁴⁰ 1
15	8	020	040	00	02.0	11.4	00.5	.	F 5-11 ³⁰ i, F 12 ³⁰ 24
16	8	000	020	00	00.7	12.9	.	.	F 0-12 ⁵⁵ 20 ⁴⁰ 24i, F 12 ⁵⁵ 20 ⁴⁰
17	8	000	020	03	01.7	12.5	.	.	F 0-3 ²⁰ 7 ⁴⁰ 12 ³⁰ i
18	8	020	050	10	07.0	06.8	.	.	.
19	8	10	07	05	07.3	05.7	11.5	.	Δ 1-11, Δ 2 ³⁰ 3 ⁴⁰ , • 4 ³⁰ 7 ²⁵ i
20	8	000	030	00	01.0	13.2	00.1	.	.
21	8	030	030	03	03.0	11.5	.	.	.
22	8	020	060	00	02.7	12.3	.	.	.
23	8	030	08	10	07.0	10.7	.	.	F 13 ⁴⁰ 16 ⁴⁰ , • 19 ³⁰ 19 ³⁰ 19 ⁴⁰ 19 ⁴⁵ ni
24	8	040	060	06	05.3	06.4	00.0	.	F 12 ³⁰ 16i
25	8	040	060	02	04.0	04.0	00.7	.	• 1-3 ⁴⁵ , 14 ⁴⁵ 15 ⁴⁰ 16 14 ²⁵ 14 ³⁵
26	8	08	070	02	05.7	07.8	00.5	.	• 15 ²⁵ 15 ⁴⁵
27	8	000	010	02	01.0	13.5	00.5	.	.
28	8	000	010	00	00.3	13.8	.	.	.
29	8	000	000	00	00.0	13.0	.	.	.
30	8	09	050	00	04.7	12.3	.	.	• 8-8 ⁴⁵ , F 16 ⁴⁰ 18 ⁴⁰ , F 18 ⁴⁰ 22 ³⁰
PES.									
WRED.		04.1	05.1	03.4	04.2	278.5	22.7		

BR. 51. 247

H_s = 52 m H_b = 52.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Inzolacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	8	040	070	03	04.7	06.5	.	.	.	R 12 ⁰⁵ 12 ²⁰ F 13-ni
2	8	000	070	08	05.0	10.0	.	.	.	F 13 ⁴⁵ 13 ⁵⁵ 23 ⁴⁰ 24; 20-20 ⁴⁵
3	8	08	050	09	07.3	06.5	00.0	.	.	F 0-0 ⁴⁵ 10 ¹⁵ 12 ²⁰ 15 ⁴⁰ 16, 19 ⁵⁰ 21 ⁵⁰ ; 1 ⁴⁰ 2, 8 ³⁰ 8 ⁵⁰
4	8	030	020	07	04.0	10.5	00.0	.	.	F 15 ⁴⁰ ni
5	8	020	060	04	04.0	08.5	.	.	.	R 15 ³⁰ 16 ⁴⁵
6	8	000	060	00	02.0	11.5	.	.	.	R 17 ³⁰ 17 ⁴⁵ F 17 ⁴⁵ 20 ³⁵
7	8	000	020	00	00.7	11.5	.	.	.	F 12 ²⁵ 15 ⁰⁵ R 14 ⁴⁰ 14 ³⁰ ; 14 ⁴⁵ 14 ³⁰
8	8	030	060	02	03.7	10.7	.	.	.	R 13 ⁵⁵ 14 ⁴⁰ ; 14 ⁴⁰ 14 ³⁰ ; 14 ⁴⁰ 14 ³⁰
9	8	000	070	01	02.7	10.7	00.0	.	.	R 6 ³⁵ 9 ⁴⁰ ; 8 ⁴⁰ 9 ³⁰ 16 ⁴⁰ 16 ⁵⁰
10	8	05	070	01	07.7	04.5	00.0	.	.	F 12 ²⁰ 14 ⁴⁰ 18 ³⁵ 20 ⁴⁰
11	8	08	05	03	06.7	07.1	04.6	.	.	F 1 ⁴⁰ 14 ³⁰ 18 ³⁵ 20 ⁴⁰
12	8	000	020	03	01.7	12.7	.	.	.	F 1 ⁵⁰ ni
13	8	000	060	00	02.0	09.5	.	.	.	• 13 ²⁵ 13 ⁵⁰ R 13 ³⁵ 13 ⁵⁵
14	8	030	060	02	03.7	11.2	00.0	.	.	F 10-13 ²⁰ i
15	8	020	040	02	02.7	10.4	.	.	.	
16	8	10	010	00	03.7	10.1	.	.	.	
17	8	000	000	00	00.0	13.6	.	.	.	
18	8	080	050	00	05.7	11.6	.	.	.	F 18 ⁴⁰ 19
19	8	000	030	05	02.7	10.1	.	.	.	F 17 ⁴⁵ 17 ⁴⁵
20	8	000	030	00	01.0	13.6	.	.	.	F 14 ⁵⁰ 15
21	8	000	010	00	00.3	13.7	.	.	.	
22	8	000	010	00	00.3	13.5	.	.	.	F 11 ⁴⁰ ni
23	8	000	030	00	01.0	13.5	.	.	.	F 8 ²⁰ 18 ⁴⁵
24	8	10	050	10	05.7	02.3	.	.	.	• 17 ²⁵ 11 ³⁰ 19 ⁰⁵ 22; R 7 ⁴⁰ 8 15-24; 9 ²⁵ 24; 15 ²⁰ 15 ⁴⁵ F 13 ³⁰ 15 ⁴⁰
25	8	10	10	10	10.0	02.5	46.5	.	.	R 0-4; 5 ⁰⁵ 3 ⁴⁰ 8 ⁴⁰ 4; F 0 ⁵⁰ 3 ⁴⁰ ; 4-22i
26	8	08	05	08	08.3	07.0	27.3	.	.	• 12 ⁴⁰ 14 ³⁰ ; R 13 ⁴⁵ 15; F 13 ⁵⁰ 16 ³⁰
27	8	10	030	10	07.7	05.4	15.5	.	.	• 10 ⁴⁵ 12 ⁴⁰
28	8	000	08	00	02.7	08.4	.	.	.	F 13 ⁵⁰ 14 ⁴⁵ R 12 ⁴⁰ 14 ³⁰ ; 12 ⁴⁵ 14 ¹⁵
29	8	000	060	04	03.3	10.8	05.7	.	.	R 18 ²⁰ 20 ⁴⁰ ; 19 ⁰⁵ 19 ⁴⁰ ; 19 ⁴⁵ 20 ¹⁰ F 19 ³⁰ ni
30	8	000	030	00	01.0	12.8	00.0	.	.	F 20 ¹⁰ 22 ⁵⁰ i
31	8	020	030	02	02.3	12.8	.	.	.	F 1 ⁴⁰ 2 ⁵⁵ 7-11 ⁴⁰ i
MES.										
RED.		03.2	05.0	03.2	03.8	06.3	100.0			

1	8	08	060	00	04.7	11.3	.	.	.	F 2-ni
2	8	040	030	00	02.3	11.3	.	.	.	• 06 ¹⁵ 7
3	8	050	030	05	05.7	09.2	00.2	.	.	• 08 ⁰⁵ 10 ⁴⁵
4	8	08	08	08	08.0	06.5	.	.	.	R 8-10i; 8 ⁰⁵ 10 ⁴⁵
5	8	000	04	00	01.3	11.6	00.0	.	.	R 13 ³⁰ 14 ³⁰
6	8	000	030	00	01.0	13.0	.	.	.	
7	8	000	000	00	00.0	12.7	.	.	.	F 4 ⁴⁰ 5 ³⁰
8	8	000	010	02	01.0	12.5	.	.	.	
9	8	000	000	00	00.0	12.7	.	.	.	F 1 ³⁵ 7 ⁵⁰ 10 ¹⁵ 12 ⁵⁰ ; F 7 ⁵⁰ 10 ¹⁵
10	8	000	000	00	00.0	13.0	.	.	.	F 0-5 8 ¹⁵ 12 ³⁰ 16 ¹⁵ 24
11	8	000	000	00	00.0	13.2	.	.	.	F 0-2 ³⁰ 5 ⁴⁰ 14 ¹⁵ 18 ²⁰ 21i
12	8	000	000	00	00.0	13.0	.	.	.	F 20 ¹⁰ 22 ²⁰ i
13	8	020	020	00	01.3	12.3	.	.	.	F 7 ¹⁵ 13i 21 ³⁰ ni
14	8	000	060	02	02.7	11.4	.	.	.	F 9 ⁴⁰ 21 ⁴⁰ 23 ³⁰ 23 ⁵⁵ ; F 21 ¹⁰ 23 ³⁰ i
15	8	000	000	00	00.0	12.5	.	.	.	F 0 ⁰⁵ 12 ⁵⁰ 16 ³⁵ 24i
16	8	000	030	02	01.7	12.4	.	.	.	F 0-3 ⁰⁵ 21 ⁵⁰ ni
17	8	020	050	00	02.3	12.2	.	.	.	F 14 ⁵⁰ ni
18	8	000	050	03	02.7	11.4	.	.	.	F 17-ni
19	8	000	080	03	03.7	10.2	.	.	.	F 15 ⁴⁰ 15 ³⁵
20	8	000	000	00	00.0	12.0	.	.	.	
21	8	000	020	00	00.7	11.7	.	.	.	
22	8	010	070	06	04.7	05.5	.	.	.	F 17 ⁵⁰ 19 ¹⁵
23	8	000	030	00	01.0	12.1	.	.	.	F 19 ³⁰ 21 ⁵⁵ F 20 ¹⁰ 20 ⁴⁰ i
24	8	000	000	04	01.3	11.0	.	.	.	F 2-ni; 21 ⁴⁰ 23 ⁴⁰ R 22-23 ³⁰
25	8	05	040	00	04.3	07.5	00.5	.	.	• 1-2 ³⁰ F 11 ⁵⁵ 12 ⁴⁰
26	8	040	070	05	05.3	03.2	.	.	.	• 17 ¹⁵ 17 ⁴⁰ R 17 ³⁵ 17 ⁴⁵
27	8	10	080	05	05.0	02.3	00.0	.	.	• 20 ²⁵ 22 ³⁰ i; 21 ⁴⁰ 23 ¹⁰
28	8	10	070	05	07.3	07.7	17.0	.	.	F 0 ⁴⁰ 0 ⁴⁵ ; 1 ⁵⁰ 6
29	8	10	050	10	08.3	05.2	00.2	.	.	R 5 ¹⁵ 5 ⁴⁰ 20 ¹⁰ 22 ¹⁵ ; 5 ⁴⁵ 6 ³⁵ 20 ⁵⁵ 22; F 20 ⁴⁵ ni
30	8	040	050	00	03.0	06.5	11.2	.	.	R 4 ²⁰ 5 ²⁵
31	8	030	030	00	02.0	11.6	.	.	.	• ni-8
MES.										
RED.		02.7	03.5	02.1	02.8	24.0	25.5			

BR. ST. 247

 $H_s = 52 \text{ m}$ $H_b = 52.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)				Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	E	050	070	06	06.0	07.9	.	.	F 15 ⁴⁵ -18 ⁴⁰ 21 ⁴⁰ -24i; 15 ⁵⁰ -19 ³⁰ i; 18 ⁴⁰ -19
2	E	050	020	00	02.3	11.6	04.5	.	F 0-4 ²⁰ 10 ⁴⁰ -22 ³⁰ i; 4 ²⁰ -10 ⁴⁰
3	E	000	020	00	00.7	12.0	.	.	F 3-8 ⁵⁰ i
4	E	000	000	00	00.0	12.1	.	.	.
5	E	000	010	00	00.3	12.1	.	.	.
6	E	000	010	00	00.3	12.0	.	.	F 7 ⁴⁰ -12i
7	E	000	000	00	00.0	11.5	.	.	.
8	E	000	020	00	00.7	10.8	.	.	.
9	E	000	010	00	00.3	11.4	.	.	.
10	E	000	020	04	02.0	11.1	.	.	.
11	E	10	10	00	06.7	03.7	.	.	8 ³⁰ -8 ⁵⁵ F 10 ³⁵ -22 ⁴⁰ F 22 ⁴⁰ -24i
12	E	020	000	00	00.7	11.6	00.0	.	F 0-9 ⁴⁰ F 9 ⁴⁰ -12 ⁵⁰ i
13	E	000	000	00	00.0	11.6	.	.	F 20-24i
14	E	010	010	00	00.7	11.0	.	.	F 0-1 ²⁰ i
15	E	000	010	03	01.3	11.0	.	.	.
16	E	060	030	00	03.0	06.7	.	.	8 ⁴⁰ -23 ⁵⁰ i; F 21 ⁴⁰ 21 ²⁰ 20 ²⁵ 24i; 18 ²⁰ 24i; 20 ⁵⁰ 21 ⁴⁰
17	E	000	080	10	06.0	06.1	.	.	12 ⁵⁵ 13 ⁵⁰ i; 18 ⁰⁵ 24i; 15 ⁴⁰ 19i; F 20 ⁴⁵
18	7	10	10	10	10.0	01.9	19.0	.	0-17i; 19 ⁴⁵ 24i; 0-9 ³⁰ i; 18 ³⁵ 23 ⁴⁰ ; 18 ⁰ 19 ⁴⁵ i; 0 ²⁰ 2 ³⁰ F 14 ⁵³ 15 ⁰⁵ 10 ⁰⁵ F 19 ⁴⁰
19	E	10	050	10	05.7	02.7	24.7	.	0-1 ⁴⁰ 14 ⁵⁰ 15 ¹⁰
20	E	070	070	00	04.7	09.5	26.5	.	.
21	8	02	030	05	03.3	11.1	.	.	Δ n-9 ²⁰
22	E	07	05	04	06.7	03.2	.	.	Δ n-7 ⁴⁰ 6 ⁵⁰ 7 ¹⁵ 11-17 ²⁰ i; 22-24i; F 13-14 ²⁰ 16 ⁴⁰ ; 14 ³⁰ 6 ²⁵ 21 ⁵⁰ 24i
23	E	07	05	02	06.0	02.4	25.8	.	0-1 ¹⁰ 10-11 ⁵⁰ ; 13 ⁵ 11, 22 ³⁰ 24i.
24	E	010	050	00	03.3	10.3	01.8	.	18 ⁵⁰ 24i
25	E	080	070	00	05.0	10.2	.	.	Δ 0-6 ³⁰
26	E	05	08	00	05.7	04.5	.	.	6 ⁵⁰ 7 ⁴⁰ 10 ⁴⁵ 10 ⁵⁰ 13-24i; 13 ⁵⁰ 7, 12 ⁵⁵ 23 ³⁰ ; F 7 ²⁰ 15 ⁵⁵ i; 13-24
27	7	10	10	10	10.0	00.0	.	.	10-1, 10-2, F 10-23 ⁴⁵
28	E	05	06	02	04.3	05.3	48.2	.	.
29	E	000	010	00	00.3	10.5	.	.	.
30	E	030	000	00	01.0	10.7	.	.	Δ 0-7 ⁴⁵
MEŠ. REC.		03.6	04.3	02.2	03.4	256.5	210.5		

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1973 OKTOBAR

1	8	000	000	00	00.0	10.7	.	.	F 6 ⁴⁰ -n
2	8	000	000	00	00.0	10.6	.	.	.
3	8	000	070	00	02.3	10.2	.	.	F 18-22 ⁵⁵ F 8 ⁴⁰ 18i; 22 ⁵⁵ 24i
4	8	000	000	00	00.0	10.6	.	.	F 0-4i
5	8	000	000	00	00.0	10.4	.	.	F 4 ⁴⁵
6	8	000	000	00	00.0	10.5	.	.	.
7	8	000	040	00	01.3	10.4	.	.	.
8	8	030	070	10	06.7	05.0	.	.	0-19 ⁴⁵ 13 ⁴⁰ 23 ⁴⁵ 24i; 11-12 ³⁰ 18 ³⁰ 23 ⁴⁵
9	8	10	080	02	06.7	06.4	35.2	.	1-20-3 ⁴⁰ 15 ⁴⁵ 15 ⁴⁵ F 14 ⁵⁵ 23 ⁰⁵ i
10	8	09	000	00	03.0	08.6	00.1	.	F 4 ²⁵ 12, F 23 ⁵⁵
11	8	000	000	08	02.7	09.9	.	.	.
12	8	04	060	08	06.0	04.1	.	.	Δ n-7
13	8	07	050	00	04.0	04.4	.	.	Δ n-7
14	8	04	030	09	05.3	06.4	.	.	Δ n-7 ⁴⁰ 20 ¹⁰ 24i; 18 ²⁰ 24i; 22-24i
15	7	09	10	10	05.7	00.0	33.6	.	0-24i; 18 ³⁵ 10 ³⁰ i; 18-20i
16	7	10	10	10	10.0	00.0	28.6	.	0-3 ¹⁰ 15 ³⁰ 23 ⁴⁰ F 20 ³⁵ 23 ⁵⁵
17	8	030	050	03	03.7	07.8	03.2	.	F 0 ¹⁰ 4 ⁵⁵ 8-15 ¹⁰ i
18	8	09	070	08	08.0	07.0	.	.	F 11 ¹⁰ 14i
19	8	10	10	01	07.0	02.1	.	.	F 2 ¹⁰ 2 ⁴⁰ F 2 ⁴⁰ 10i
20	8	030	070	09	06.0	04.5	.	.	Δ n-6 ⁵⁰
21	7	10	10	10	10.0	00.0	00.2	.	2 ⁴⁰ 3 ¹⁰ 24i
22	7	10	10	10	10.0	00.0	14.0	.	0-17 ⁴⁰ i; F 1-8 ³⁰ 14-24i; 10-11 ¹⁵ 13 ³⁵ 14 ³⁰ ; 14-15
23	8	070	040	00	03.7	10.1	35.4	.	F 0-11, F 11-14i; 17 ¹⁰ 21i
24	8	08	060	00	04.7	07.9	.	.	F 9 ⁴⁰ 18, F 18 ⁴⁰ 24i
25	8	020	060	00	02.7	08.3	.	.	F 0-23 ³⁰ 22 ³⁰ 24i
26	8	050	070	00	04.0	08.3	.	.	F 0-10 ⁴⁰
27	8	050	020	00	02.3	08.3	.	.	.
28	8	020	000	00	00.7	09.9	.	.	Δ n-6 ³⁰
29	8	000	000	00	00.0	09.8	.	.	Δ 20-24i
30	8	000	010	00	00.3	09.7	.	.	Δ 0-8, 19 ³⁰ -n
31	8	000	000	00	00.0	09.7	.	.	.
MEŠ. REC.		04.2	04.4	03.1	03.9	221.6	154.6		

ER. ST. 247

 $H_s = 52 \text{ m}$ $H_b = 52.6 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		7	14	21	Sred Dias				
1	6	C70	C10	CC	C2.7	C5.8	.	.	F 0-24
2	6	CC0	CC0	CC	CC.0	C5.3	.	.	F 0-145
3	6	CC0	CC	CC	CC.0	C5.8	.	.	Δ n-7
4	6	CC0	C2	CC	CC.7	C5.7	.	.	Δ n-7 ³⁰
5	6	C70	C60	1C●	C6.3	C7.2	.	.	● 18 ⁴⁰ 23 ³⁰ i
6	6	1C	1C●	1C●	1C.0	CC.8	C3.0	.	● 1-24i
7	7	1C●	1C●	1C●	1C.0	CC.0	38.2	.	F 0-18 ⁰⁵ 22-24; F 2-3 ¹⁵ F 18 ⁴⁵ 22i; ● 10-24
8	6	C60	1C	1C●	C6.7	C3.0	71.5	.	● 20-04 ¹⁰ 14 ¹⁵ 14 ³⁰ i; 18 ²⁰ 23; F 0-13 ⁰⁰ 22 ⁵⁰ 24i
9	6	1C●	1C	C4	C6.0	CC.0	C6.4	.	F 0-22 ¹⁰ i; ● 6 ⁴⁰ 7
10	6	C10	C10	CC	CC.7	C5.4	CC.0	.	.
11	6	CC0	CC0	CC	CC.0	C5.3	.	.	Δ 1 n-8 19-24
12	6	CC0	C30	CC	C1.0	C5.0	.	.	Δ 10-8 17-24; F 17 ¹⁰ 21 ³⁰
13	6	1C	C6	C7	C7.7	CC.0	.	.	Δ 0-8 17 ³⁰ 24
14	6	C7	1C	1C	C5.0	CC.0	.	.	Δ 10-10 ● 22 ³⁰ 24
15	6	1C	1C	C8	C5.3	C3.8	C5.4	.	● 10-2 ⁰⁰ 5 ³⁰ 6 ³⁰ F 5 ⁵⁵ 7 ²⁰ Δ 18-24
16	6	1C	C60	C2	C6.0	C5.3	.	.	Δ 0-8 18-24
17	6	C50	C5	C7	C6.3	C3.5	.	.	Δ 20-9 ● 11 ²⁰ 11 ⁴⁰ F 20 ⁴⁵ 24i
18	6	C60	C20	CC	C2.7	C6.5	CC.0	.	F 0-0 ¹⁵ 19 ³⁰ 24
19	6	C3	C70	C5	C5.0	C7.5	.	.	Δ n-7 ³⁰ 20 ¹⁰ n
20	6	1C	C60	C4	C6.7	C1.0	.	.	Δ 19-n
21	6	C1	C10	CC	CC.7	C5.2	.	.	F 1 ¹⁰ 23 ⁴⁰
22	6	C5	C40	CC	C4.3	C6.7	.	.	F 0 ¹⁵ 6 ⁵⁰
23	6	CC	CC0	CC	CC.0	C5.0	.	.	Δ n-9 ³⁰
24	6	C6	1C	1C	C6.7	CC.3	.	.	.
25	6	1C	1C	1C	1C.0	CC.5	CC.1	.	● 19-19 ⁴⁵ 21-24i
26	7	1C●	1C●	1C●	1C.0	CC.0	C1.6	.	● 5 ⁰⁰ 24 F 21 ⁵⁵ 24
27	7	1C●*	1C●	1C	1C.0	CC.7	41.6	.	● 0 ⁰⁰ 1 ¹⁰ F 0 ⁴⁵ 7 ⁰⁵ ● 1 ⁵⁰ 5 ● 6 ⁴⁰ 9 F 7 ³⁵ 11 ⁵⁵
28	6	C7	C10	CC	C2.7	C7.8	C1.4	.	F 5-11 ⁵⁰ 17 ³⁰ 18 ³⁰ F 11 ⁵⁰ 17 ³⁰
29	6	CC	C60	1C	C5.3	C6.3	.	.	● 21 ³⁰ 24 F 0 ⁰⁵
30	6	1C*	C6	C2	C6.0	C2.7	45.2	23	* 0-6 ⁰⁰ 13-5 ⁴⁵ F 7 ²⁰ 7 ³⁰ 12-21 ⁰⁰ i; F 7 ³⁰ 12, 17 ⁴⁰ 18 ²⁵
MES.									
REC.		C6.0	C5.6	C4.6	C5.4	150.1	214.7		

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1	7	C6	1C	1C	C6.7	CC.0	.	20	* 9 ³⁵ 11 ¹⁰ 16 ²⁰ 19
2	6	C6	1C	1C*	C6.7	CC.0	CC.8	18	F 145 2 ⁰⁰ 5 ⁴⁰ 17 ⁴⁰ 23 ⁴⁰ 24; F 17 ⁴⁰ 23 ⁴⁰ * 19-23
3	7	1C	1C	1C	1C.0	CC.0	CC.2	12	F 0-13 ⁰⁰ 9 ⁴⁰ 15 ⁴⁰ F 13 ⁰⁰ 9 ⁴⁰ * 11 ⁵⁰ 12 ⁴⁰
4	7	1C	1C	1C●	1C.0	CC.0	CC.0	10	● 7-8 ⁴⁰ 17-24i
5	6	1C	CC0	CC	C2.3	C4.0	C4.0	08	● 0 ²⁰ 5 ⁵⁰ i
6	6	CC	CC0	CC	CC.0	C6.6	.	03	F 3-4 ⁴⁰
7	6	CC	C5	C6	C5.7	C5.5	.	.	Δ 2 n-8 ⁴⁰
8	6	C3	C6	1C●	C7.0	C2.6	.	.	Δ n-7, F 17 ⁴⁰ n, ● 19 ⁵⁰ 24i
9	7	1C●	1C●	1C●	1C.0	CC.0	11.6	.	● 0-24 F 21 ¹⁵ 24i; F 22 ⁴⁰ 23 ³⁰
10	6	1C	1C	1C	1C.0	CC.5	14.4	.	● 0-6 ¹⁵ F 0-1 ⁰⁵ 4 ¹⁰ 13; * 4-4 ⁴⁵ F 4 ⁰⁵ 4 ³⁰ 13-24
11	6	C7	C3	C2	C4.0	C6.2	.	.	F 0-2 ³⁰
12	6	1C	C70	CC	C5.7	C2.1	.	.	.
13	6	CC	1C	1C	C6.7	C1.4	.	.	Δ n-8 ⁴⁰
14	6	C6	C30	CC	C3.0	C7.5	.	.	Δ n-8 ⁰⁵ 20 ¹⁰ n
15	7	1C●	C7	C8	C6.3	CC.0	CC.8	.	● 6 ⁰⁵ 11 ⁴³ F 11 ²⁰ 9 ⁰⁵ Δ 11 ⁴³ 11 ⁴⁴ F 11 ⁴⁵ 12 ¹⁵ * 13-13 ³⁰ F 19 ⁰⁵ 21 ⁵⁰
16	6	C2	C10	CC	C1.0	C7.7	C5.4	.	● n-n F 13 ²⁰ 15i
17	7	1C	1C●*	1C●	1C.0	CC.3	.	.	* 12 ⁵⁰ 13 ²⁰ * 13 ²⁰ 13 ⁵⁰ ● 13 ⁵⁰ 24, = 20-24
18	5	1C●	1C●	C7	C5.0	CC.0	24.9	.	● 0-18 ¹⁰ 0-8 ³⁰ 11 ²⁰ 18 ³⁰
19	7	C5	C5●	1C●	C5.3	CC.0	25.0	.	● 9 ⁰⁵ 10 ⁴⁰ 13 ²⁰ 24i
20	7	1C	1C●	1C	1C.0	CC.0	18.5	.	● 0-15 ³⁰ i, = 17-24
21	7	1C	1C	1C	1C.0	C1.2	C6.1	.	● 4 ³⁰ 8 ¹⁰ i F 11 ¹¹ 23 ⁴⁰ i
22	7	1C	1C●	1C	1C.0	CC.0	11.6	.	F 0-9 13 ¹⁰ 16 ²⁴ i ● 8 ¹⁵ ni
23	6	1C●	1C	CC	C6.7	CC.3	45.0	.	● n-9 ²⁰ = 0-2 17 ¹⁵ n
24	6	1C●	C40	CC	C4.7	C2.5	C1.2	.	● n-8 ²⁰ = 0-8 ⁴⁵ ● 11 ⁵⁰ 12 ⁰⁵ = 0-2 17 ¹⁵ 24
25	6	1C	C5	1C	C5.7	C3.4	CC.4	.	● 0-2 0-n, ● 19 ²⁰ 19 ³⁰
26	7	1C●	1C●	C6	C5.3	CC.0	C3.5	.	● 2 n-5 ⁰⁰ 13 ⁵⁰ 17 ¹⁰ F 4 6 ⁰⁵ 6 ²⁰ F 12-16 ⁵⁵ ● 13 ¹⁰ 13 ⁵⁰ F 16 ⁵⁵ 23 ³⁵
27	6	1C	C4	CC	C4.7	C6.5	45.6	.	● n-6 ¹⁰ F 0 ¹³ 3
28	6	C6	C6	1C●	C6.7	C2.0	.	.	● 19-ni
29	6	C3	C20	CC	C1.7	C7.3	CC.8	.	.
30	6	C6	C5	C5	C6.7	C1.5	.	.	.
31	6	C7	1C●	1C	C5.0	CC.0	.	.	● 9 ³⁰ 15i
MES.									
REC.		C7.6	C7.5	C6.5	C7.2	71.1	225.5		

BR. ST. 267

$H_s = 232 \text{ m}$, $H_b = 233.3 \text{ m}$, $h_t = 2.0 \text{ m}$, $h_r = 1.3 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	8	04	09	03	05.3	04.2	.	.	.	$\angle 0-10^{30} 10^{30}$
2	7	09	10	10*	05.7	00.0	.	.	.	$\angle 0-10-9^{30} 10^{30} 17^{30} 24^{30} = 15^{30} 22^{30} 16^{30} 17^{30} = 22-24$ [X]
3	5	10	05	10	05.7	00.6	03.5	02	.	$\angle 0-2^{30} 5^{30} 7^{30} 23-24^{30} = 10-5^{30} 2-6^{30} 10^{30} 23^{30} = 7^{30} 10^{30} 19^{30} 22^{30} 23^{30} 24^{30}$
4	3	10	10	10	10.0	00.0	02.2	.	.	$\angle 0-13^{30} = 0-19^{30} 2^{30} 13^{30} 10^{30} 13^{30} 24^{30} = 19^{30} 24^{30}$ [X]
5	6	10*	05	10	05.7	00.0	06.6	.	.	$\angle 0-0^{30} = 0-17^{30} 19^{30} 22^{30} 10^{30} 10^{30}$
6	5	10	10	10	10.0	00.0	00.6	.	.	$\angle 3^{30} 24^{30}$
7	7	10	10	10	10.0	00.0	.	.	.	$\angle 0-11^{30} F_{NNE} 12^{30} 23$
8	6	10	10	10	10.0	00.0	.	.	.	$\angle 9^{30} 24^{30}$
9	6	10	10	10	10.0	00.0	.	.	.	$\angle 0-24^{30}$
10	7	10	10	10	10.0	00.0	.	.	.	$\angle 0-6^{30} 15^{30} 20^{30} 11^{30} 12^{30}$
11	7	00	08	08	05.3	00.4	00.0	.	.	$F_{NNE} 15^{30} 16^{30}$
12	7	08	09	07	08.0	00.5	.	.	.	$F_{NNW-N-NNE} 3^{30} 3^{30} 5^{30} 5^{30} 12-19^{30} 22^{30} 24^{30}$
13	7	09	05	01	06.3	04.1	.	.	.	$F_{N0-21^{30}}$
14	7	01	00	00	06.3	08.1	.	.	.	$\angle 20-24^{30}$
15	6	00	05	09	04.7	06.5	.	.	.	$\angle 0-10-10^{30} 19^{30} 24^{30} = 12^{30} 15^{30} 19^{30} 24^{30}$
16	5	07	10*	10*	09.0	00.0	.	.	.	$\angle 0-11^{30} \angle 0-7^{30} 12^{30} 24^{30}$ [X]
17	7	10*	08	10	05.3	00.5	01.8	04	.	$\angle 0-10-8^{30} = 20^{30} 24^{30}$ [X]
18	3	10	10	10	10.0	00.0	00.0	.	.	$\angle 0-14^{30} 17^{30} 24^{30} = 10^{30} 16^{30} 17^{30} 8^{30} 12^{30} 16^{30} = 11^{30} 17^{30}$
19	1	10	10	10	10.0	00.0	00.4	.	.	$\angle 0-4^{30} = 4^{30} 21^{30} 10^{30} 10^{30} 12^{30} 11^{30} = 0-18^{30} 21^{30} 24^{30}$
20	2	10	10	10	10.0	00.0	00.5	.	.	$\angle 0-2^{30} = 2-13^{30} 16^{30} 17^{30} 10^{30} 12^{30} = 13^{30} 24^{30} 16^{30} 23^{30}$
21	5	10	10	10	10.0	00.0	00.6	.	.	$\angle 0-6^{30} 11^{30} 24^{30} = 6^{30} 11^{30}$
22	6	10	10	10	10.0	00.0	.	.	.	$\angle 0-17^{30}$
23	7	10	10	10	10.0	00.0	00.0	.	.	$\angle 0-5^{30} 10^{30} 14^{30} 23^{30} 40$
24	7	10	10	10	10.0	00.0	00.6	.	.	$\angle 0-16^{30} 18^{30} 10^{30} 18^{30} 19^{30}$
25	7	10	09	10	05.7	00.6	00.2	.	.	$\angle 14-17^{30} F_{NNE} 9^{30} 9^{30} 18^{30} 20^{30}$
26	7	06	08	05	06.3	00.6	.	.	.	$\angle 8^{30} 16^{30} \angle 0-20-24^{30}$
27	6	06	00	02	02.7	08.1	.	.	.	$\angle 0-6^{30} 15^{30} 24^{30} = 5^{30} 24^{30} 16^{30} 24^{30}$ [X]
28	2	10*	10*	10*	10.0	00.0	00.0	.	.	$\angle 0-10-21^{30}$ [X]
29	7	10*	10*	10*	10.0	00.0	16.2	17	.	$\angle 0-8^{30} = 6^{30} 8^{30} F_{NE} 17^{30} 18^{30}$ [X]
30	7	10	05	00	06.3	04.6	04.4	22	.	$\angle 0-17^{30} 8^{30} = 7^{30} 24^{30}$ [X]
31	6	10	08	10	05.3	03.3	00.0	15	.	
MES.										
WRED.		08.4	08.7	08.2	08.4	42.1	37.6			

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1973 FEBRUAR

1	6	05	05	10	05.3	00.2	00.0	10	.	$\angle 3-24^{30} 17^{30} 23^{30}$ [X]
2	5	10	10	06	08.7	00.0	06.9	07	.	$\angle 0-6^{30} = 0-16^{30} 9^{30}$ [X]
3	3	10	10	05	09.7	00.0	00.1	03	.	$\angle 0-19^{30} 17^{30} 24^{30} = 15^{30} 5^{30} = 5^{30} 17^{30} 10^{30} 16^{30} F_{NW} 18^{30} 19^{30}$ [X]
4	7	09	01	00	03.3	05.2	05.8	.	.	$F_{NNE} 17^{30} 23^{30}$
5	6	10	10	10	10.0	00.0	.	.	.	$\angle 05-9^{30} = 7^{30} 15^{30} 21^{30} 24^{30}$
6	7	10	07	00	05.7	03.0	.	.	.	$\angle 0-10^{30} \angle 20-24^{30}$
7	7	00	06	03	03.0	07.8	.	.	.	$\angle 0-10-9^{30} 22^{30} 24^{30} = 6^{30} 13^{30} 18^{30} 24^{30} \angle 0-11^{30} 22^{30}$
8	6	01	01	00	00.7	08.1	.	.	.	$\angle 1-20-8^{30} = 0-14^{30}$
9	6	06	08	00	04.7	05.2	.	.	.	$\angle 0-12-8^{30} = 6^{30} 24^{30} \angle 11^{30} 14^{30} \angle 0-11^{30} 15^{30} 24^{30}$
10	7	08	08	10	08.7	04.3	.	.	.	$\angle 0-10-8^{30} = 0-13^{30} F_{SSE} 22^{30} 24^{30}$
11	7	10	05	01	06.7	00.7	00.2	.	.	$F_{SSE-S-NNE} 0-4^{30} 6^{30} 8^{30} 20^{30} 22^{30} \angle 0-10^{30} 14^{30} 12^{30} 14^{30}$
12	6	10	10	10	10.0	00.0	00.0	.	.	$\angle 8^{30} 10^{30} \angle 0-15^{30} 15^{30} F_{N} 10^{30} 16^{30} 17^{30} 18^{30}$
13	7	00	03	00	01.0	00.7	00.7	.	.	$\angle 0-15-8^{30} 21^{30} 24^{30} \angle 0-11^{30} 21^{30}$
14	7	04	05	05	07.3	01.6	.	.	.	$\angle 0-10-9^{30} = 6^{30} 12^{30} F_{SE} 14^{30} 24^{30}$
15	7	10	10	10	10.0	01.1	.	.	.	$F_{SSE} 0-14^{30} \angle 0-11^{30} 24^{30}$
16	7	10	10	04	08.0	02.1	13.7	.	.	$\angle 0-18^{30} 3^{30} 45^{30} 11^{30} 15^{30} F_{SE-WNW} 17^{30} 9^{30} 14^{30} 14^{30} T 12^{30} 13$
17	8	02	05	10	07.0	04.1	04.5	.	.	$\angle 0-6-7^{30} F_{NNE} 17^{30} 24^{30} \angle 0-17^{30} 18^{30} 21^{30} 23^{30}$
18	7	09	08	05	08.7	00.7	00.1	.	.	$F_{NNE} 0-9^{30}$
19	7	04	10	10	08.0	03.9	.	.	.	$\angle 0-11^{30} 8^{30} = 6^{30} 13^{30}$
20	6	10	10	10	10.0	00.0	.	.	.	$\angle 7^{30} 16^{30} F_{N} 21-23$
21	7	10	05	00	06.3	04.4	.	.	.	$\angle 0-22-24^{30}$
22	7	10	05	08	09.0	00.1	00.0	.	.	$\angle 20-14^{30} \angle 0-4^{30} 5^{30} \angle 0-20^{30} 20^{30}$
23	7	05	05	08	07.3	02.1	00.1	.	.	$\angle 0-15-19^{30} 20^{30} F_{NW} 17^{30} 18$
24	7	10	05	01	06.7	02.1	00.2	.	.	$\angle 5^{30} 9^{30} \angle 0-18^{30} 18^{30}$
25	7	08	10	10*	05.3	00.0	00.4	.	.	$\angle 0-8^{30} = 7^{30} 12^{30} F_{SSE-NNE} 13^{30} 14^{30} 19^{30} 21^{30} \angle 0-19^{30} 19^{30} \angle 0-11^{30} 24^{30}$ [X]
26	7	10	10	00	06.7	00.0	09.1	18	.	$\angle 1-20-5^{30} F_{NW} 9^{30} 18^{30}$ [X]
27	7	04	08	01	04.3	07.0	.	04	.	$F_{N} 15^{30} 20^{30}$ [X]
28	7	05	10	10	05.7	00.5	.	02	.	$F_{N-NW-WNW} 9^{30} 15^{30} 18^{30} 20^{30} \angle 0-14^{30} 15^{30}$ [X]
MES.										
WRED.		07.4	08.3	05.7	07.1	73.2	35.6			

BR. ST. 267

 $H_s = 232 \text{ m}$ $H_b = 233.3 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.3 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Intencija broj sati	Padavine R mm	Snežni pokriivač h cm	Razvoj vremena w
		14	7	14	21				
1	7 10	06	10	08.7	01.6	00.0	02	$F_{WNW-N} 2^{45} 3^{40} 13^{28} 16^{40}$; [X]	
2	7 10	08	08	08.7	03.3	.	.	[X]	
3	7 10	09	10	09.7	02.6	.	.	$F_{NNE} 15^{09} 15^{30}$	
4	7 10	08	08	08.7	01.9	.	.	$F_{N-NNE} 12^{45} 18^i$; $* 21^{30} 22^{20}$	
5	7 10	09	00	06.3	02.3	00.0	.	$* 0-11^{00} 10^{30} F_N 13^{30} 20^{20} i$	
6	7 03	09	05	05.7	04.9	00.0	.	$F_{NNE} 12^{45} 16^{53}$	
7	7 04 0	09	10	07.7	06.3	.	.	$\angle 0-8^{30} \bullet 23-23^{30}$	
8	7 10	10	10	10.0	00.0	00.2	.	$F_{SE} 15^{34} 17^i \bullet 18^{30} 24^i$	
9	6 10	10	10	10.0	00.2	00.4	.	$\bullet 0-5^{15} i, 14^{45} 19^{15} = 6-14^{40} F_{NNE} 15^{10} 18^{40}$	
10	7 10*	10	10*	10.0	00.4	04.4	02	$* 0-12^{30} 10^{35} 14^{25} 24^i = 10^{30} 12^{20} \bullet 14^{25} 20^{25} F_N 15^{08} 15^{52} i$; [X]	
11	2 10	10*	10	10.0	00.0	05.6	.	$* 0-12^{30} 0-0^{30} 9^{30} 20^{10} = 6^{10} 8^{40} 21-21^{30} = 20^{10} 21^i$; [X]	
12	7 09	05	10	08.0	04.5	13.0	09	$F_{NNE} 15^{05} 20^i$; [X]	
13	3 10*	10*	10*	10.0	00.0	02.4	01	$* 0-1^{10} 22^{30} = 22^{10} 24^i$; [X]	
14	7 10	09	04	07.7	02.5	12.3	06	$= 0-3^{40} * 2^{30} = 5^{30} F_{NNE} 17^{02} 20^{39}$; [X]	
15	7 09	08	09	08.7	03.7	.	.	.	
16	7 10	10	10	10.0	00.0	.	.	.	
17	7 10	09	09	09.3	02.9	.	.	.	
18	5 10*	10	10	10.0	00.0	00.0	.	$* 0-16^{30} 12^{30} \bullet 0-12^{30} 17^{20} 20^{30} 21^{45} = 16^{40} 24^i$	
19	7 10	09	09	09.7	00.7	04.2	.	$= 0-1^{15} F_N 10^{20} 16^{35} i, \bullet 14^{50} 17^{10} i$	
20	7 10	04 0	01	05.0	04.0	00.0	.	$\bullet 0-14^{15} 17^{30} 8^{10} i, F_{NNE} 6^{45} 18^{45} i$	
21	7 04 0	04 0	00	02.7	09.5	00.0	.	$\angle 0-17^{40}$	
22	7 09	08 0	00	05.7	03.5	.	.	.	
23	7 00 0	00 0	00	00.0	09.6	.	.	$\angle 0-8^i = 6-7^{40}$	
24	7 04 0	09	10	07.7	04.1	.	.	$\angle 0-30^i 8^i$	
25	7 10	10	10	10.0	00.0	00.1	.	$\bullet 0-15^{50} 9^{05} 11^{20} 12^{10} 16^{20} 19^{05}$	
26	7 09	10	00	06.3	03.9	00.4	.	.	
27	7 04 0	06 0	09	06.3	05.8	.	.	$\angle 0-10-8^{30}$	
28	7 09	10	10	09.7	00.5	.	.	$\bullet 0-13^{40} 24^i, F_{SE} 13^{50} 14^{20}$	
29	5 10	10	10	10.0	00.0	17.4	.	$\bullet 0-20^{24} i = 7^{30} 24^i$	
30	6 10	09	10	09.7	01.1	15.8	.	$\bullet 0-10-9^{20} i = 0-24^i$	
31	7 10	08	10	09.3	01.6	00.0	.	$= 0-12^{40} i, \bullet 0-6^{40} 8^{10} 16^{20} 18^{20}$	
MES.									
WRED.		08.5	08.3	07.5	08.1	91.4	76.2		

SKCPJE

1973 APRIL

1	7 04	05 00	00	03.0	08.2	00.3	.	$\angle 0-10^{10} 21-24^i = 4^{10} 10^{40}$
2	7 00 00	02 00	00	00.7	10.4	.	.	$\angle 0-12^{00} 9^{30} 14^{30} 24^i = 6^{05} 11^{40}$
3	8 00 00	05 00	08	04.3	07.6	.	.	$\angle 1-20-9^{30} i$
4	7 09	10	10	09.7	01.6	.	.	$F_{SE} 9^{30} 16^{20} i, \bullet 0-10^{20} 24^i, T 14-16^{10} i, 18, 14^{45} 15^{30}$
5	7 10	09	09	08.0	00.2	11.3	.	$\bullet 0-10-0^{20} 3^{40} 6^{20}$
6	7 10	10	10	10.0	00.0	00.0	.	$\bullet 03^{30} 9^{15} 17^{45} 18^{20} i, F_{N-NNE} 4^{45} 4^{55} 17^{50} 17^{53}$
7	7 03	03 00	00	02.0	10.0	00.9	.	$\angle 0-13^{15} 9^{30} 20-24^i = 4^{10} 9^{20}$
8	7 02 00	04 00	08	04.7	11.0	.	.	$\angle 1-20-8^i$
9	7 09 00	08	05	07.3	06.2	.	.	$\angle 1^{120} 9 F_{SE} 16^{45} 20^i, T 19^{15} 21$
10	7 10	03 00	01	04.7	04.1	.	.	$F_S 11^{20} 24^i$
11	7 08	10	08	08.7	00.3	.	.	$F_{SE} 0-3^{40} \bullet 08^{02} 18^{25} i$
12	8 03 00	03 00	09	05.0	08.4	00.5	.	$\angle 1-20-8^{30}$
13	8 09	10	01	06.7	05.2	.	.	$\angle 1^{120} 8 F_{WNW} 13^{45} 14^{10}$
14	8 08	06	10	08.0	03.4	.	.	$\bullet 0-16^{00} 18^{20} 21^{25} 22^{10}$
15	6 10	10	10	10.0	00.0	03.9	.	$\bullet 0-14^{50} 17^{45} i, 11^{20} 24^i, F_{WNW} 21^{20} 24^i$
16	7 10	10	10	10.0	00.0	18.0	.	$\bullet 0-10-1^{20} F_{WNW} 0-16^{30}$
17	7 09	09	08	08.7	03.7	.	.	$\bullet 12^{30} 13^{05} F_{NNE} 18^{40} 18^{50} i, T 21^{30} 24^i$
18	7 00 00	01 00	01	00.7	11.3	00.0	.	$\angle 0-3, \angle 0-121-24^i$
19	7 10	09	09	09.3	02.8	.	.	$\angle 0-10-8^i, \bullet 0^{15} 55 20^{25} i$
20	7 09	08	01	06.0	04.0	00.0	.	$F_{SSE} 15^{10} 17^{05} i, \bullet 0-16^{40} 17^{20}$
21	8 07	06 00	04	05.7	06.0	00.0	.	$\angle 0^{120} 7^{20} \bullet 09^{37} 9^{40} 17^{30} 18^{30} F_{WSW-S-WNW} 13^{10} 18^i, \angle 20^{30} 24^i$
22	8 04 00	07	01	04.0	10.4	00.3	.	$\angle 0-2, \angle 1^{10} 7^{50} F_{WNW} 16^{22} 16^{40}$
23	7 04 00	10	10	08.0	02.9	.	.	$\angle 0-10-3^{40} \angle 0^{13} 40 6^{50} \bullet 0^{17} 15 21^i$
24	7 10	10	10	10.0	01.6	00.0	.	$\angle 0-19-9^{05} 18-19^{30} \bullet 10-11^{20} 18 F_{NW} 17^{28} 17^{45} T 17^{30} 18$
25	8 05 00	06 00	02	04.3	07.7	11.9	.	$= 4^{20} 9^{30} F_{WNW} 12^{15} 18^{20} i, \angle 19^{20} 20^{30}$
26	7 05 00	10	10	08.3	02.3	.	.	$\angle 10-8^i \bullet 09^{05} 15^{20} i, 18^{35} 22^{10} i$
27	7 01 00	06 00	00	02.3	08.9	00.1	.	$\angle 0-12^{10} 24^i$
28	7 00 00	03 00	03	02.0	10.3	.	.	$\angle 1-20-8^{30} = 6^{15} 11^{30}$
29	7 04 00	09	10	07.7	04.5	.	.	$\angle 0-10-7^{10} i, \bullet 15^{30} 23^{30}$
30	7 10	03 00	02	05.0	06.5	03.8	.	$\bullet 02^{20} 4^{40} 17-8^{30} i = 4^{45} 9^{30}$
MES.								
WRED.		06.1	06.8	05.5	06.2	159.5	51.0	

PR. ST. 267

H_s = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Vrijest 0-9	Oblačnost N (0-10)				Inolacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21				
1	8	CC	01	CC	CC.3	12.3	CC.6	.	Δ ⁰⁻¹⁰⁻⁹ 21-24
2	7	CC	06	CC	CC.0	11.0	.	.	Δ ²⁻⁰⁻¹⁷ 30
3	7	C9	08	C4	C7.0	C8.2	.	.	.
4	7	04	08	CC	C4.0	C8.0	.	.	Δ ⁰⁻¹⁰⁻⁹ 24
5	8	C6	C2	CC	C2.7	C9.4	.	.	Δ ⁰⁻¹⁻²⁰⁻⁸ 45 21-24
6	7	02	01	C8	03.7	11.8	.	.	Δ ⁰⁻¹⁰⁻⁹
7	7	C9	C7	C5	C7.0	C4.0	.	.	Δ ⁰⁻²²⁻²⁴
8	6	10	10	01	C7.0	C0.0	.	.	Δ ⁰⁻¹⁰⁻⁹ 40 19 ³⁰ 24; = 9-14 ⁴⁰ 22 ³⁰ 24;
9	7	C6	05	10	C6.3	C5.6	.	.	Δ ⁰⁻²⁰⁻¹⁷ 40 = 0-6 ⁴⁰ F _{N-NNE} 12 ⁰⁵ 22 ³⁵ ; ● ⁰⁻¹⁵ 05 15 ⁰⁸ 16 ⁰⁴ 16 ²⁵ 16 ²⁰ 19 ⁰⁰ 16 ²⁵ 19 ²⁰
10	7	09	10	C5	C6.0	C0.0	13.4	.	● ⁰⁻¹⁻²⁰⁻⁴ 30 20-18 ⁴⁰ ; [16 ³⁰ 16 ⁴⁰
11	7	C5	C6	CC	C3.7	C7.8	C1.0	.	Δ ⁰⁻²¹⁻²⁴
12	7	07	03	C9	C6.3	10.0	.	.	Δ ⁰⁻²⁰⁻⁸ 30 F _N 15 ²⁵ 20 ²⁵ ;
13	7	10	10	10	C0.0	C0.0	C2.7	.	● ⁰⁻¹⁰ 40 24;
14	7	10	09	C2	C7.0	C3.3	C8.4	.	● ⁰⁻¹⁰⁻⁸ 40
15	7	00	02	04	C2.0	12.7	C0.0	.	Δ ⁰⁻¹⁰⁻⁹
16	7	01	04	C6	C3.7	C9.6	.	.	Δ ⁰⁻²⁰⁻⁸ 40 T 14 ³⁵ 18 ¹⁰ ; F _N 16-16 ²³ 16 ⁰⁸ 16 ⁴⁰ ; ● ⁰⁻¹⁶ 12 19 ⁴⁰
17	7	10	10	10	C0.0	C0.5	C7.3	.	= 3-5 ⁴⁰ F _{NNE} 12 ⁵³ 21 ³⁰ ; ● ⁰⁻¹⁶ 05 16 ¹⁵
18	7	C5	10	CC	C5.0	C1.1	C0.0	.	Δ ⁰⁻¹³ 36 8 ³⁰ 20 ²⁰ 24; ● ⁰⁻¹⁶ 05 16 ²⁵
19	6	10	08	10	C5.3	C2.3	C0.0	.	Δ ⁰⁻¹⁰⁻⁸ 30 = 6 ³⁵ 15 ²⁰
20	7	C9	08	CC	C5.7	C4.8	.	.	Δ ⁰⁻¹⁰⁻⁸ 40 18 ⁴⁰ 24; = 13 ³⁰ 8 ³⁰
21	7	C5	01	CC	C2.0	12.4	.	.	Δ ⁰⁻²⁰⁻⁹ 20-24; = 3 ³⁰ 8 ³⁰
22	7	C1	06	C5	C4.0	12.4	.	.	Δ ⁰⁻²⁰⁻⁸ 30 20-24
23	7	C2	04	C2	C2.7	11.5	.	.	Δ ⁰⁻²⁰⁻⁸ 40 20-24
24	7	C1	03	C2	C2.0	12.2	.	.	Δ ⁰⁻²⁰⁻⁸ 30 F _N 16 ²⁰
25	8	03	08	C2	04.3	C6.9	.	.	F _N 0-0 ²⁵ 9-20 ²⁰ ;
26	8	C8	08	10	C6.7	C3.4	.	.	F _{NNE-N} 6 ³² 13 ²⁰ ; 16 ²⁰ 20 ⁵⁰ ; ● ⁰⁻¹⁰ 25 9 ⁴⁰ ; ● ⁰⁻¹⁻² 10-13 ¹⁵ ; 20 ³⁰ 20 ⁴⁰
27	8	C5	10	10	C5.7	C1.0	.	.	F _{NNE-NNW} 12 ²⁰ 14 ¹⁰ 10 ¹⁵ 10 ⁴⁵ ; ● ⁰⁻¹⁷ 30 23 ³⁰ ;
28	7	10	10	10	C0.0	C0.0	C1.0	.	● ⁰⁻¹⁴ 5 13 ¹⁰
29	8	06	08	04	C6.0	C0.5	C0.0	.	Δ ⁰⁻¹³ 10 8 ³⁰ ; ● ⁰⁻¹³ 05 13 ²⁵ ; ● ⁰⁻¹ 13 ⁵³ 14 ⁰³
30	7	C2	C5	C1	C2.7	12.3	C1.2	.	Δ ⁰⁻¹⁰⁻⁸ 30 12-24
31	8	04	08	10	C7.3	C6.1	.	.	Δ ⁰⁻¹⁰⁻⁹ ; 9 ³⁰ 10 ²⁵ T 14 ³⁵ 16 ²⁰ ; 15 ⁰⁵ 15 ¹⁵ ; 15 ⁰⁸ 15 ²³ F _N 15-15 ¹⁵ ; ● ⁰⁻¹ 15 ²³ 17 ¹⁵ ; 20 ¹⁵ 22 ¹⁰
MES.									
REC.		05.6	06.5	C4.5	C5.6	208.1	53.6		

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1973 JUN

1	7	C2	C3	CC	C1.7	12.3	C2.1	.	= 8 ³⁰ 10 ⁴⁰ Δ ⁰⁻¹ 18 ⁴⁵ 24
2	8	01	01	08	C2.3	12.2	.	.	Δ ⁰⁻²⁰⁻⁹ 17 23-24
3	7	00	09	06	C5.0	10.4	.	.	Δ ⁰⁻³ 20 Δ ⁰⁻²⁻⁸
4	7	C8	10	C4	C7.3	C1.4	.	.	● ⁰⁻²³ 50 24
5	7	C8	05	08	07.0	C7.6	C0.0	.	● ⁰⁻⁵ 55 6 ⁰⁵
6	7	00	04	C7	C3.7	10.1	.	.	Δ ⁰⁻¹ 13 ³⁰ 8 ³⁰ T 18 ¹⁰ 19 ³⁰
7	7	10	03	C1	C4.7	C3.7	.	.	.
8	7	07	03	C4	C4.7	10.9	C1.4	.	● ⁰⁻¹⁰ 55 5 ³⁰ 19 ²⁰ 24; T 19 ⁴⁰ 20 ¹⁰ 23 ⁴⁵ 24;
9	7	C8	04	02	04.7	C6.7	C0.5	.	Δ ⁰⁻³ 19 ³⁰ 19 ³⁰ ; ● ⁰⁻¹⁰ 55 13 ³⁰ ; 17 ¹⁴ 17 ²⁰ 14 ⁴⁰ 14 ⁴⁹ ; ● ⁰⁻⁰⁵ 3 ³⁰ ; 22 ⁴⁵ 24; T 12 ⁰⁰ 15 ¹⁴ 18 ¹⁵ ; 18 ¹²
10	7	07	09	07	C7.7	C2.2	C2.5	.	● ⁰⁻⁰ 14 ⁵⁵ 12 ¹² 15 ²⁵ 17 ¹⁰ ; F _{N-NW} 11 ¹² 11 ²⁰ 14 ⁵⁵ 15 ³⁰ [12 ²⁵ F _N 12 ²⁰ 12 ²⁰
11	7	10	05	08	C9.0	C1.9	C0.0	.	F _N 9 ³⁰ 18 ⁴⁰ ; ● ⁰⁻¹ 18 ²⁵ 18 ³⁴ ; ● ⁰⁻¹ 18 ³⁴ 19 ⁰⁵
12	7	C6	04	C4	C4.7	C6.3	C1.6	.	F _N 12 ³⁰ 17 ⁴⁰ T 17 ¹⁴ 17 ⁴⁰
13	7	C4	05	10	C6.3	07.2	.	.	Δ ⁰⁻¹⁰ 30 7 ³⁰ = 2 ⁴⁰ 10 ³⁰ T 14 ³⁰ 18 ¹⁰ ; F _N 15 ¹⁰ 15 ³⁰ ; ● ⁰⁻¹ 15 ²⁵ 16 ¹⁰ ; 15 ³⁰ 15 ⁴⁰ 15 ³⁵ 16 ¹⁵
14	7	03	05	08	C5.3	C9.2	C4.3	.	Δ ⁰⁻¹⁰⁻⁹ = 2 ⁴⁰ 9 ³⁰ T 13 ²⁰ 20 ¹⁵ ; 18 ⁵⁰ 19 ²⁰ ; ● ⁰⁻¹ 18 ⁵⁰ 19 ⁴⁸ ; ● ⁰⁻¹ 19 ³⁰ 20 ¹⁰ ; ● ⁰⁻¹ 16-18 ¹⁰ ;
15	7	09	10	06	C8.3	00.2	C4.0	.	● ⁰⁻¹ 6 ³⁰ 10 ⁰⁵ ; F _{NW} 9 ⁵⁰ 18 ³⁰ ; Δ ⁰⁻¹ 23-24
16	8	C2	05	09	C6.7	C6.7	C0.4	.	Δ ⁰⁻²⁰⁻⁸ F _N 8 ³⁰ 20 ³⁰ ;
17	8	04	05	02	C2.7	10.2	.	.	.
18	8	01	02	C8	C3.7	C9.8	.	.	Δ ⁰⁻² 7 ³⁰
19	7	10	10	04	C8.0	00.3	.	.	● ⁰⁻¹⁷ 13 ²⁰
20	8	C2	C4	CC	C2.0	12.1	C5.4	.	Δ ⁰⁻¹⁰⁻⁹ F _{NW} 11 ⁵⁰ 16 ¹⁰ ;
21	7	00	02	C2	C1.3	13.0	.	.	Δ ⁰⁻⁸
22	7	C3	04	CC	C2.3	11.7	.	.	.
23	8	C1	02	CC	C1.0	10.9	.	.	F _{NNE} 13 ⁰⁶ 16
24	8	C3	C4	C3	C3.3	09.5	.	.	● ⁰⁻¹⁰ 55 10 ²⁴ F _{N-NW} 12 ²⁴ 18 ⁵⁶
25	8	C6	05	09	C6.7	C5.6	C0.0	.	Δ ⁰⁻¹ 6 ¹⁰ ; F _{NNE} 14 ²⁰ 18 ⁴⁰ ; 20 ¹⁵ 20 ⁴⁰
26	8	C9	06	01	C5.3	C4.5	C0.1	.	● ⁰⁻¹⁰ 0 ⁴⁰ 11 ²⁵ 12; T 13 ⁵⁰ 16 ¹⁵
27	7	01	04	CC	C1.7	10.4	C0.0	.	Δ ⁰⁻¹⁰⁻⁸ 17 ⁴⁰ 8 ⁴⁰
28	7	CC	C1	CC	C0.3	13.8	.	.	Δ ⁰⁻¹ 1-6 ⁴⁰
29	8	00	00	CC	C0.0	13.1	.	.	.
30	7	C4	04	C4	C4.0	C5.8	.	.	T 9 ³⁰ 10 ¹⁵ 12 ⁵⁵ 19 ⁴⁵ ; ● ⁰⁻¹ 9 ³⁴ 9 ⁵⁵ 15 ⁰⁷ 18 ⁰⁵ ; F _N F _{NNE} 14 ⁵⁷ 15 ⁴⁰ 16-16 ³⁰ 16 ⁰⁵ 24
MES.									
REC.		C4.3	C4.9	C4.2	C4.4	240.1	22.7		

BR. ST. 267

 $H_s = 232 \text{ m}$ $H_b = 233.3 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.3 \text{ m}$

Dan	Vrijeme 0-9	Oblaknost N (0-10)				Insekcija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	7	C20	040	1C●	05.3	06.8	01.4	.	$\Delta 1-7^{30} T 15-19^{30} \cdot 17-22^{30} \cdot 17^{40} 19^{05} F 17^{35} 18, 19^{30} 21$
2	7	08	10R	10	09.3	05.6	01.1	.	$\Delta 3^{30} 11^{30} T 13^{30} 15^{30} F 14^{30} 15^{30}$
3	7	040	040	09	05.7	06.6	.	.	$\Delta 3-9^{30} 14-15^{30} T 11^{30} 16^{30} \cdot 21^{30} 22^{30} \cdot 15^{30} 16^{30} \cdot 19^{35} 24i$
4	7	09	040	C3	05.3	05.5	00.0	.	$\Delta 10-5, 11^{30} 17^{30} \cdot 18^{30} 9^{35} F 16^{30} 16^{35} \cdot 17^{30} 18^{35} \cdot 17^{30} 18^{35}$
5	8	050	060	04	05.0	09.4	00.6	.	$T 14^{30} 19^{05} \cdot FNE-WNW 14^{45} 18^{30} \cdot 17^{05} 18^{35} \cdot 17^{35} 18^{35}$
6	7	07	040	C1	04.0	10.5	00.0	.	$\Delta 0-10-7^{30} 23^{30} 24$
7	7	000	010	09●R	03.3	10.4	.	.	$\Delta 0-10-8, F 12^{30} 13^{30} \cdot 12^{55} 13^{05} \cdot T 19^{40} 21^{30} \cdot 17^{30} 20^{30} 20^{30} 20^{30}$
8	7	000	010	1C R	03.7	11.2	C3.7	.	$\Delta 0-7^{30} = 4^{20} 6^{30} T 17^{35} 20^{35} \cdot F_N 17^{50} 18^{35} \cdot 18^{35} 19^{30} \cdot 19^{30} 19^{35} \cdot 19^{30} 20^{30}$
9	7	000	030	08	03.7	10.0	08.9	.	$\Delta 2^{30} 10^{30} F_N 17^{50} 18^{35} T 18^{30} 19^{35} \cdot 22^{30} 24$
10	7	010	10●	07	06.0	06.5	01.9	.	$\Delta 0^{35} 1^{35} T 1^{35} 3^{30} \cdot 11^{35} 13^{30} \cdot 0-1 2^{30} 12^{35} 14^{30} \cdot 17^{30} 2^{30} F_N 11^{30} 13^{35} 12^{35} 2^{30}$
11	7	10	1C	1C	1C.0	00.4	03.7	.	$\Delta 1^{35} 7, F_N 8^{30} 9^{35} 15^{30} 18$
12	7	09	090	06	08.0	03.2	00.0	.	$\Delta 0^{35} 1^{30} T 13^{30} 14^{35} 17^{30} \cdot 17^{30} 16^{30} 16^{35} 16^{40}$
13	7	06	040	09	06.3	08.3	05.3	.	$\Delta 1^{30} 9, 21-24 \cdot T 15-16^{30} \cdot 16^{30} 17^{35} \cdot 16^{35} 17^{35}$
14	7	000	030	01	01.3	11.6	00.0	.	$\Delta 0-7 = 4^{20} 7^{30}$
15	7	010	040	09	04.7	09.5	.	.	$\Delta 0-8$
16	8	000	010	00	00.3	13.2	.	.	$\Delta 0-7^{30}$
17	7	000	000	00	00.0	13.2	.	.	$\Delta 0-10-7^{30}$
18	8	000	00	00	02.7	08.8	.	.	$\Delta 0-7^{30}$
19	8	000	000	01	00.3	11.9	.	.	$\Delta 0-6^{30} F_{NNE} 5^{35} 8$
20	8	C20	030	C1	02.0	12.1	.	.	$\Delta 0-8, F_N 17^{45} 20^{30}$
21	8	C20	010	C1	01.3	12.8	.	.	.
22	7	000	010	00	00.3	13.1	.	.	.
23	8	000	000	00	00.0	12.8	.	.	.
24	7	C20	060	03	03.7	10.8	.	.	$\Delta 2^{30} 7, F_{NNE} 22^{30} 24$
25	7	10●	040	10●	08.0	06.3	C4.6	.	$F_{NNE-WNW} 0-20^{30} 12^{35} 17^{30} \cdot 0-14-8^{30} 20^{30} 24 \cdot F_{NNE} 16^{30} 22^{35}$
26	7	1C●	1C	C1	07.0	02.3	20.7	.	$\Delta 0-10-7^{35} 13^{35} 16^{35}$
27	7	08	08	03	06.3	02.5	10.2	.	$\Delta 0-10-8, 13^{35} 11^{30} 12^{30}$
28	7	020	030	C2	02.3	10.6	00.0	.	$\Delta 10-8 = 1^{30} 9^{30} T 18^{35} 20^{35} F 18^{30} 19^{30} \cdot 0-1 19^{40} 20$
29	7	000	030	10●R	04.3	12.7	00.5	.	$\Delta 1^{30} 6^{30} F_{NNE} 19^{30} 20^{35} T 19^{30} 20^{30} 16^{30} 20^{35} 23^{35} \cdot 1-2 20^{30} 20^{40} \cdot 0-1 20^{40} 24$
30	7	040	050	08	05.7	10.1	09.2	.	$F_N 18^{35} 20^{35}$
31	7	010	05	10	06.7	07.5	.	.	$\Delta 1^{30} 8, F_W 16^{30} 16^{35} \cdot 16^{35} 16^{35} \cdot 16^{35} 17^{00}$
MES.									
WRED.		03.3	04.5	C5.0	04.3	276.7	71.6		

SKOPJE

1973 AUGUST

Dan	Vrijeme 0-9	Oblaknost N (0-10)				Insekcija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias	7	7	
1	7	010	040	00	01.7	10.7	C2.0	.	$\Delta 0^{30} 4^{30} \cdot 16^{42} 16^{44} T 16^{30} 16^{55}$
2	7	000	020	C5	02.3	12.3	00.0	.	$\Delta 0-10-8, 21-23$
3	7	09	10R	03	07.3	03.3	.	.	$\Delta 1^{30} 7^{30} \cdot 0-1 16^{35} 15^{05} \cdot 22^{05} 24 \cdot T 11^{00} 14^{30} \cdot 13^{30} 13^{30} \cdot 19^{30} 24$
4	7	10●	05	C1	05.3	06.7	C6.3	.	$\Delta 0-10-3^{30} 6^{30} 7, 14^{30} 15^{30} \cdot 4^{30} 6^{30} T 13^{30} 16^{30} \cdot 18^{30} 21$
5	7	050	040	C2	03.7	07.9	00.0	.	$\Delta 0-10-8, 21-24 \cdot T 12^{35} 17^{30}$
6	7	000	020	02	01.3	11.9	.	.	$\Delta 1-20-7$
7	7	010	020	02	01.7	10.9	.	.	$\Delta 0-8$
8	7	000	020	00	00.7	11.7	.	.	$\Delta 2-8$
9	7	020	010	00	01.0	11.5	.	.	$F_N 8^{30} 18^{05}$
10	8	000	010	00	00.3	12.4	.	.	$\Delta 0^{30} 7, F_{NNE} 8^{30} 12, 16^{35} 18$
11	8	000	000	00	00.0	12.6	.	.	.
12	8	000	010	00	00.3	12.6	.	.	.
13	8	000	040	06	03.3	11.6	.	.	.
14	7	010	C30	04	02.7	08.2	.	.	$\Delta 0-10-7^{30} 20^{30} 24 \cdot F_{NNE-N} 9^{05} 16^{30}$
15	7	010	05	01	02.3	11.5	.	.	$\Delta 10-7, F_N 13^{30} 19^{30}$
16	7	010	040	C1	02.0	11.8	.	.	.
17	7	010	050	01	02.3	10.6	.	.	.
18	7	040	C50	02	03.7	09.4	.	.	$\Delta 0-10-7$
19	7	010	040	00	01.7	11.1	.	.	$F_N 10^{30} 15^{30} \cdot 21-24$
20	7	000	020	00	00.7	12.4	.	.	$\Delta 10-7$
21	8	000	020	01	01.0	12.0	.	.	$\Delta 0-10-7^{30}$
22	8	000	030	00	01.0	11.7	.	.	.
23	7	000	010	00	00.3	10.6	.	.	$\Delta 2^{30} 10^{35}$
24	7	000	010	00	00.3	08.1	.	.	$T 14^{35} 19^{30} \cdot 16^{30} 16^{30} \cdot 16^{30} 19^{30} \cdot 0-1 17^{35} 17^{30} \cdot 18^{35} 19^{35} 21^{30}$
25	7	05	040	00	03.0	07.6	00.1	.	$\Delta 1^{30} 7^{30} T 14^{35} 17^{30} \cdot F_N 14^{30} 16^{30} \cdot 0-1 17^{35} 17^{30} \cdot 18^{35} 19^{35} 21^{30}$
26	7	040	040	1C●R	06.0	07.3	00.0	.	$\Delta 1^{30} 5^{30} T 12^{35} 12^{55} F_{WNW} 16^{30} 16^{40} \cdot 0-1 18^{35} 23^{30} \cdot 18^{30} 21^{30} \cdot 1-2 19^{30} 20^{30}$
27	7	08	060	1C●	06.0	06.2	16.2	.	$\Delta 0-10-8, 10^{30} 12^{30} \cdot 19^{35} 21^{30} \cdot 19^{35}$
28	7	10●	09	09	09.3	01.4	13.0	.	$\Delta 0-10-8, 10^{30} 12^{30}$
29	7	09	07	10●	08.7	04.0	C2.9	.	$\Delta 0-7^{30} = 5^{30} 8^{30} \cdot 0-1 14^{30} 24 \cdot T 16^{30} 20^{30} \cdot 20^{30} 23^{30}$
30	7	09	07	07	07.7	02.7	07.2	.	$\Delta 0-10-0^{30} 16^{30} 18^{30} \cdot T 16-16^{35} \cdot 16^{35} 16^{35} \cdot F_N 16^{30} 16^{30} \cdot 19-19^{35}$
31	7	05	06	C6	07.0	05.1	19.4	.	
MES.									
WRED.		02.9	03.7	C2.7	03.1	287.8	67.1		

BR. ST. 267

 $H_s = 232 \text{ m}$ $H_b = 233.3 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.3 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies			
1	8	C8	09	10	05.0	04.6	05.1	.	0-10 ³⁰ 4 ¹⁰ 19 ³⁰ 21 ³⁰ T 14 ³⁰ 16 ³⁰ 19 ³⁰ 19 ⁴⁰ 18 ³⁵ 19 ³⁰ 18 ³⁰ 19 ³⁰ 21-23 ⁵⁰
2	7	10	10	00	06.7	00.9	31.5	.	0-11 ³⁵ 4 ¹⁰ 12 ³⁰
3	7	04	04	00	02.7	10.2	01.6	.	0-10 ¹⁹ 19 ⁴⁰ 24 ¹⁰ 7 ³⁰ 9 ⁴⁰
4	7	00	01	00	00.3	11.4	.	.	0-20 ¹⁹ 4 ⁴⁵ 3 ⁴⁵ 9 ³⁰
5	8	00	02	00	00.7	11.0	.	.	0-8 ¹⁹ 19 ³⁰ 24 ¹⁰
6	7	00	03	00	01.0	10.2	.	.	10-8 ³⁰ 5 ²⁰ 11 ²⁰
7	7	00	01	01	00.7	10.9	.	.	0-10 ¹⁹ 20 ¹⁵ 24 ¹⁰
8	7	00	03	02	01.7	09.8	.	.	0-20 ¹⁰ 15 ²³ 24 ¹⁰ 4 ³⁰ 7 ⁴⁵
9	7	00	01	00	00.3	10.9	.	.	0-10 ¹⁹ 19 ³⁰ 24 ¹⁰ 4 ²⁰ 7 ³⁰
10	7	00	01	00	00.3	10.7	.	.	0-1-2 10 ¹⁹ 19 ³⁰ 24 ¹⁰ 4 ²⁰ 9 ⁴⁰
11	8	08	10	09	09.0	02.3	.	.	1-20-2 ³⁵ FNE-NNE 2 ³² 5 ⁰⁵ 12 ¹⁰ 24 ¹⁰ ; 0-14 ⁵⁸ 15 ¹⁰
12	8	03	02	02	02.3	11.0	00.0	.	FNE 0-1 0-13 ³⁰ 7 ²³ 24 ¹⁰
13	8	03	01	00	01.3	09.7	.	.	0-20-8 ¹⁵ FNE 15 ²⁰ 19 ³⁰
14	7	00	01	00	00.3	10.6	.	.	0-11 ²² 19 ¹⁹ 24 ¹⁰
15	7	00	01	05	02.0	09.9	.	.	0-1-20-8 ⁴⁰ 18 ³⁰ 24 ¹⁰ 9 ³⁰ 10 ⁴⁰ 21 ³⁰ 22 ⁴⁰
16	7	02	05	03	03.3	08.2	.	.	1-20-8 ⁵⁰ 23 ³⁰ 24 ¹⁰
17	7	00	01	01	00.7	09.7	.	.	0-10-8 ²⁰ 1 ⁴⁰ 4 ²⁰ 7 ⁴⁰
18	7	09	04	10	07.7	06.1	02.6	.	0-11 ³⁰ 3 ⁴⁰ 15 ⁴⁵ 21 ²⁰ 5 ³⁰ 12 ¹⁵ T 16 ⁴⁰ 17 ¹⁰ 17 ¹⁰ 21 ¹⁵ ; 0-1-2 17 ¹⁰ 20 ¹⁰
19	7	10	10	10	10.0	00.0	48.7	.	0-1-2 2 ⁴⁰ 15 ⁴⁵ 19 ⁴⁵ 21 ³⁵ 17 ³⁵ 5 ⁴⁰ FSE 11 ³⁰ 16 ³⁵ 4 ¹⁹ 21 ¹⁰ 17 ⁴⁰ 22 ²⁰
20	7	10	06	04	06.7	04.0	17.9	.	0-17-7 ⁵⁵ 0-9 ⁰⁵ 9 ²⁵ 17 ⁰⁰ 17 ¹⁰ 17 ⁰⁰ 17 ⁰⁰ 17 ⁰⁰
21	8	06	03	01	03.3	09.2	04.3	.	1-18 ³⁰ 24 ¹⁰
22	8	09	02	02	04.3	08.2	.	.	0-10-10 ¹⁵ 19 ³⁰ 24 ¹⁰ 7 ⁵⁵ 9 ³⁵
23	7	02	04	00	02.0	09.7	.	.	0-1-20-8 ⁴⁰ 18 ³⁰ 24 ¹⁰
24	7	00	03	00	01.0	09.8	.	.	1-20-10 ⁵⁰ 12 ³⁰ 24 ¹⁰ 4 ³⁰ 7 ⁴⁵ 5 ¹⁰ 6 ⁰⁵
25	8	00	00	00	00.0	09.7	.	.	1-20-9 ¹⁹ 24 ¹⁰ 1 ²⁰ 7 ³⁰
26	8	00	00	00	00.0	09.9	.	.	0-10-9 ¹⁸ 20 ²⁴
27	7	10	00	10	09.3	01.8	.	.	0-1-20-10 ⁵⁰ 5 ¹⁵ 11 ⁴⁰ 0-10 ⁴⁵ 11 ⁴⁰ T 15 ⁴⁰ 18 ⁰⁵ 18 ⁰⁵ 20 ⁴⁵ 0-11 ¹⁰ 19 ²⁰
28	6	09	09	07	08.3	02.2	04.3	.	0-24 ¹⁰ 0-6 ⁴⁵ 15 ⁴⁵ 9 ⁴⁵ 14 ²⁵ 20 ²⁰ FNE 13 ¹⁵ 15 ⁰⁴ 17 ⁴⁰ 18 ¹¹ 4 ²⁰ 4 ²²
29	7	05	05	00	04.7	03.8	03.5	.	0-17-1 ¹⁹ 24 ¹⁰
30	6	03	01	00	01.3	05.6	.	.	0-10-10 ³⁰ 20 ²⁴ 0 ²⁰ 15 ⁴⁵
MES.									
WRED.		03.8	03.7	02.6	03.4	232.0	119.5		

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1	6	10	06	00	05.3	07.1	.	.	0-10-10 ¹⁹ 19 ³⁰ 24 ¹⁰ 0-2 ³⁰ 5 ⁴⁰ 13 ⁴⁰ 2 ³⁰ 5 ⁴⁰
2	7	02	01	00	01.0	08.8	.	.	0-20-10 ¹⁰ 19 ²⁴ 2 ³⁰ 5 ¹⁵ 7 ⁴⁵ 11 ⁴⁵ 5 ¹⁵ 7 ⁴⁵
3	7	04	01	00	01.7	08.3	.	.	0-20-9 ²⁴ 18 ³⁰ 24 ¹⁰ 2 ⁴⁰ 10 ³⁰ 5 ¹⁰ 6 ⁴⁵
4	7	08	03	10	07.0	04.4	.	.	0-10-9 ¹⁵ 5 ²⁰ 8 ⁵⁰ FNE-N 8 ⁴⁵ 10 ³⁰ 13 ⁰⁰ 16 ⁰²
5	8	05	01	00	02.0	09.1	.	.	0-21 ³⁰ 24 ¹⁰
6	7	00	01	00	00.3	09.3	.	.	0-10-9 ⁴⁵ 20 ²⁴
7	7	02	01	02	01.7	10.0	.	.	0-20-8 ⁵⁰ 18 ³⁰ 24 ¹⁰
8	7	06	04	10	06.7	06.9	.	.	1-20-9 ³⁰
9	7	10	10	10	10.0	00.0	04.1	.	0-14 ⁴⁰ 20 ²⁰ 5 ³⁰ 6 ⁴⁵
10	7	09	03	00	04.0	07.2	08.4	.	0-10 ¹⁵ 1 ⁴⁰ 5 ³⁰ 11 ³⁵ 0-120 ³⁰ 24 ¹⁰
11	7	00	01	00	00.3	09.3	.	.	0-10-10 ¹⁷ 20 ²⁴ 2 ³⁰ 11 ³⁰
12	7	00	02	01	01.0	07.9	.	.	0-1-20-10 ¹⁹ 19 ³⁰ 24 ¹⁰ 0 ¹⁰ 13 ³⁵ 23 ¹⁵ 24 ¹⁰ 5 ⁴⁰ 8 ⁴⁵
13	7	06	06	10	07.3	05.8	.	.	0-20-8 ⁴⁰ 0-4 ¹⁵ 0 ²³ 24 ¹⁰
14	7	08	06	10	06.0	03.4	00.2	.	0-10-20 ¹⁰ 16 ¹² 16 ¹⁹ 23 ³⁰ 24 ¹⁰ 5 ¹⁵ 12 ¹⁵ 0-21 ³⁰ 23 ³⁰
15	7	07	09	08	08.0	04.4	02.2	.	0-128 ⁴⁵ 8 ²⁰ 5 ¹⁰ 19 ³⁰ 7 ⁸
16	7	05	08	03	05.3	06.7	00.4	.	0-0 ³⁰ 0 ²⁰
17	8	06	08	00	04.7	04.2	.	.	0-10-9 ¹⁵ FSE-NNE 13 ²² 14 ³⁷ 23 ³⁰ 24 ¹⁰
18	8	03	04	00	02.3	09.6	.	.	FNE 0-5 ⁴²
19	8	04	03	03	03.3	08.8	.	.	0-11 ²⁰ 10 ⁴⁰ 19 ¹⁰ 24 ¹⁰
20	7	03	03	00	02.0	07.0	.	.	
21	7	05	08	00	05.7	04.1	.	.	0-10-8 ³⁰ 20 ¹⁰ 24 ¹⁰
22	7	08	09	10	05.0	02.5	.	.	0-10 ¹⁰ 5 ¹⁵ 11 ⁴⁵ FNE-NE-E-S-W 12 ⁵⁷ 19 ³⁵ 0-2 16 ³⁴ 22 ¹⁰ 18 ²⁰ 22
23	8	06	02	00	02.7	08.5	29.1	.	FNE 4 ⁰² 16 ¹⁰ 1 ¹⁰ 22 ²⁴
24	7	09	10	10	09.7	00.0	.	.	0-0-8 ¹⁵ 6 ¹⁰ 14 ³⁰
25	7	09	09	10	09.3	00.0	.	.	FNE 18 ⁵⁵ 21 ¹⁰
26	7	03	04	06	04.3	08.7	.	.	
27	8	06	06	00	04.0	08.0	.	.	14 ¹⁵ 9 ³⁰ 1 ²⁰ 20 ²⁴
28	7	06	00	00	02.0	08.2	.	.	0-10-9 ¹⁰ 6 ¹⁰ 12 ¹⁵ 0-119 ³⁰ 24 ¹⁰
29	7	00	00	00	00.0	08.1	.	.	0-1-20-8 ⁴⁰ 20 ²⁰ 24 ¹⁰ 5 ²⁰ 12 ³⁰ 21 ¹⁵ 24 ¹⁰ 0-118 ⁴⁰ 20 ²⁰
30	7	00	02	00	00.7	08.3	.	.	1-20-8 ⁴⁰ 0-13 ³⁰
31	7	09	03	00	04.0	04.7	.	.	24 ¹⁵ 8 ⁴⁰ FNE 11-20 ⁵⁰
MES.									
WRED.		05.2	04.3	03.3	04.3	199.7	44.4		

BK. ST. 267

 $H_s = 232 \text{ m}$ $H_b = 233.3 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.3 \text{ m}$

Dan	Valjivost 0-9	Oblačnost N (0-10)					Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21	Sred Dias			
1	8	C6○	C1○	CC	C2.3	C8.6	.	.	$F_{NNW-NNE} 155 15^{17} 19^{51} 20^{56} i$
2	7	CC○	CC○	CC	CC.0	C9.0	.	.	$\angle 0-14-8^{40}$
3	7	CC○	CC○	CC	CC.0	C8.7	.	.	$\angle 0-13-10, \infty 09^{30} 11^{45}$
4	8	C2○	C3○	CC	01.7	C8.8	.	.	$\angle 0-10-9^{30} 21^{40} 24; = 9^{10} 11^{40}$
5	7	1C	C3○	CC	C4.3	C5.4	.	.	$\angle 0-9-15^{30} 13^{30}$
6	6	C7≡	C4○	C9	06.7	C3.9	.	.	$\angle 0-10-8^{15} = 2^{20} 7^{25} = 7^{25} 24$
7	4	10	1C	1C●	10.0	C0.0	.	.	$\angle 0-17^{30} 18^{40}; F_{NNE} 17^{50} 22^{05}; \bullet 0-18^{40} 24; T 23^{58} 24$
8	7	10	10	1C●	10.0	C0.0	21.5	.	$T 0-0^{13} 13; 0^{14} 0^{17}; \bullet 0-12-0-4^{54} 19^{40} 24; \Delta 0-13^{40} 4^{30} 10^{45} 5^{10}$
9	6	10*	1C●	1C●	10.0	C0.0	16.4	01	$\bullet 0-10-6^{25} 5^{10} 5^{45} 11^{45} 24; \bullet 0-10^{25} 4^{40} 6^{10}; \bullet 6-11-11^{45} i$
10	6	10	1C	C9	C5.7	C0.0	C7.5	.	$\bullet 0-10-3^{30} = 3^{40} 24$
11	6	1C●	1C	10	10.0	C0.0	CC.0	.	$= 0-24 \bullet 05^{40} 10^{30} 21^{40} 24$
12	6	1C●	1C	C4	08.0	C0.5	C0.2	.	$= 0-15^{40} 19^{40} 24; \bullet 0-17^{40} i; \angle 0-17^{30} 24$
13	6	1C	01○	CC	C3.7	C3.6	C0.0	.	$= 0-24 \angle 0-10-11^{19} 24$
14	5	10●	10	10	10.0	C0.0	C0.0	.	$= 0-6^{15} 13^{35} 24; \angle 1-2-0-6^{10} \bullet 06^{10} 9^{10}$
15	6	C9	C2○	CC	C3.7	C5.7	C1.0	.	$= 0-15^{30} 23-24; \bullet 2-3-6^{05} \angle 20-24$
16	6	02≡	08	00	C3.3	C4.2	.	.	$\angle 0-10-0^{30} 21^{30} 24; = 0-6^{14} 9^{40} 16^{45} \angle 0-9-6^{15} 7^{40} 9^{20} 9^{40} = 07^{10} 9^{20}$
17	5	1C≡	04○	09	07.7	C2.2	.	.	$\angle 0-10-13^{30} \bullet 0-17^{30} 17^{10} = 4-5^{10} 12^{45} 13^{40} = 15^{10} 6^{20} = 6^{20} 12^{45} F_{NNE} 13^{38} 13^{32}$
18	8	03	01○	00	01.3	C7.8	.	.	$\angle 0-4^{30} 8^{16} F_{NNE} 12^{04} 19^{50} i$
19	8	C1○	00○	CC	00.3	C7.3	.	.	$\angle 0-10^{30} 10^{10} 23-24$
20	6	C9	C7	1C	C6.7	C3.9	.	.	$\angle 0-10-8^{40} = 5^{30} 17^{05} F_{NNE} 17^{12} 22^{32}$
21	8	C1	05○	C6	C4.0	C8.6	.	.	$F_{N-NNW} 10^{30} 15^{30} i 19^{30} 20$
22	7	C0	02○	06	C2.7	C8.3	.	.	$\angle 0-3-7^{30} 21^{50} 24$
23	7	CC	01○	00	00.3	C7.9	.	.	$\angle 0-1-2-0 \angle 9^{20} 18^{30} 24; = 1^{30} 12^{40} 23-24$
24	6	C3	06○	C2	C3.7	C4.5	.	.	$\angle 0-20-9^{50} 21^{50} 24; = 0-24$
25	6	C4	00○	CC	C1.3	C6.3	.	.	$= 0-24 \angle 0-10-9^{30} 21-24$
26	5	C2	08	C5	C5.0	C2.5	.	.	$\angle 0-10-8^{40} = 0-19^{40} \angle 20^{30} 23^{30} F_{NNE} 22^{15} 24; \bullet 0-12^{45} 24$
27	7	10*	C9	10*	C5.7	C0.0	C7.4	01	$\bullet 0-1^{10} F_{NNE} 0-3^{32} \angle 1^{10} 2 \bullet 0-12-6^{40} 17^{40} 24; \angle$
28	7	10*	C6○	C6	C7.3	C0.6	C0.6	01	$\bullet 0-10^{10} 1^{10} 6^{20} 7^{25} 11^{30} 12^{35} \angle 0-23^{30} 24; \angle$
29	7	CC	00○	10	C3.3	C8.0	C0.0	.	$\angle 0-10-16^{40} 17^{40} 24; = 2^{10} 6^{30}$
30	4	1C	1C*	1C*	10.0	C0.0	.	.	$\angle 1-20-7^{25} \bullet 0-17^{25} 16^{40} 19^{25} 21^{40} i; F_{NNE} 14^{45} 20^{50} i; \angle 18^{40} 19^{40} \angle$
MES.									
MED.		06.0	05.0	C4.5	C5.3	126.3	55.4		

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1	7	C1	1C	1C*	C7.0	C4.4	C5.2	C7	$\bullet 0-17^{25} 24 \angle$
2	4	C9*	1C*	1C*	C5.7	C0.0	C7.0	15	$\bullet 0-10-2^{10} 6^{15} 7^{40} 12^{45} 24; = 2^{10} 10^{40} \angle$
3	5	1C*	1C*	10	10.0	C0.0	16.0	33	$\bullet 0-10-19^{15} \angle$
4	5	1C	1C	10	10.0	C0.0	C2.3	34	$= 5^{15} 24 \angle \bullet 09^{05} 9^{15} i \angle$
5	4	10≡	00○	00≡	C3.3	C0.4	C0.0	26	$= 0-5^{15} 10^{30} 18^{20} = 5^{15} 10^{30} 21-24; = 18^{20} 21 V 20^{20} 24 \angle$
6	1	1C≡	1C≡	1C≡	10.0	C0.0	.	22	$= 0-24 V 0-24 \angle$
7	3	1C≡	1C≡	10≡	10.0	C0.0	.	19	$= 0-24 V 2-0-24 \angle$
8	5	CC	04○	CC	C1.3	C4.1	C0.0	16	$\angle 0-24 = 0-0^{15} = 0^{15} 21^{30} \angle 0^{20} 1^{30} = 21^{30} 24 \angle$
9	4	10≡	05	C2	C5.7	C2.4	.	16	$= 0-10-3 V 2-0-21^{20} = 0-13-9^{30} = 9^{30} 11^{30} = 11^{30} 21^{10} F_N 21^{10} 24 i \angle$
10	7	1C	1C	10	10.0	C0.0	.	15	$F_{NNE} 0-17^{40} i; \bullet 21^{50} 24 \angle$
11	5	1C	10*	10	10.0	C0.0	C8.7	20	$\bullet 0-10-14^{10} i = 14^{10} 24 \angle$
12	5	10	1C	CC	C6.7	C0.0	C0.8	20	$= 0-20^{45} = 20^{45} 24 V 0-122^{30} 24 \angle$
13	4	10	10	10	10.0	C0.0	.	18	$V 2-0-24 = 0-1 = 1-5^{45} = 5^{45} 12^{35} i = 6^{30} 7^{05} 12^{35} 24 \angle$
14	4	10●	1C	1C	10.0	C0.0	C4.0	15	$= 0-15^{30} \bullet 0-10^{25} 2^{55} 5^{45} 11^{35} = 0-15^{30} 17^{40} = 0-17^{40} 24 \angle \angle 0-14^{40} \angle$
15	7	1C≡	1C●	1C*	10.0	C0.0	14.0	13	$= 0-10-11^{45} 12^{40} 13^{10} = 11^{45} 13^{30} i; \bullet 0-13^{20} 13^{40} \bullet 0-13^{40} 14; \bullet 0-14-22^{05} F_{NNW} 13^{25}$
16	7	C9	06○	CC	C5.0	C3.2	C4.3	13	$F_{NNW} 1^{10} 11^{55} \angle 1-2-11-11^{30} \angle$
17	7	04	09	C8	C7.0	C5.6	.	09	$= 21^{30} 24 \angle$
18	6	09	C5○	C5	C6.3	C5.7	.	09	$= 0-24 \bullet 016^{40} 17^{15} \angle$
19	6	C8	01○	CC	C3.0	C4.8	C0.1	08	$= 0-24 \bullet 02^{30} 4^{30} \angle$
20	5	1C	04○	06	C6.7	C3.1	.	07	$= 0-24 \angle$
21	4	10≡	08	00≡	C6.0	C0.3	.	07	$= 0-5^{10} 12-20^{50} = 0-15^{10} 6^{25} 11^{10} 12-21^{30} 24; = 1-2^{45} 11^{10} \angle$
22	5	10≡	03○	1C●	C7.7	C2.8	.	04	$= 0-0^{14} 6-6^{20} 11^{30} 12^{10} = 0^{30} 6^{10} 12^{40} 24; = 6^{20} 11^{30} \bullet 0-18^{40} 20^{40} i \angle$
23	5	C8	C0○	00	C2.7	C5.5	C0.0	03	$= 0-21^{40} = 21^{40} 22^{30} = 22^{30} 24 \angle$
24	4	1C≡	10	10●	10.0	C0.0	.	03	$= 20-10^{40} = 10^{30} 13^{10} 15^{30} 24 i; = 11^{40} 18^{10} i; \bullet 0-18^{30} 24 \angle$
25	3	1C●	10≡	10●	10.0	C0.0	C1.1	02	$= 0-18^{30} \bullet 0-10-10^{30} = 18^{30} 24; \bullet 0-20^{10} 20^{50} \angle$
26	5	C9	08	C4	C7.0	C2.5	C0.2	01	$= 0-1, 3^{30} 10^{30} i; = 1-3^{30} 6^{20} 8^{15} 10^{30} 15^{30} 20^{10} 24; \bullet 0-10^{40} F_{SE} 15^{15} 18^{25} i \angle 17^{45}$
27	8	C2	02○	CC	C1.3	C8.0	C0.1	.	$= 0-1^{40}$
28	6	C5	09○	C6	C6.7	C3.2	.	.	$\angle 0-1^{30} 8 = 6^{10} 24$
29	5	1C●	C3○	CC	C4.3	C1.7	C0.0	.	$= 0-18^{30} \bullet 0-15^{20} 7^{40}$
30	6	10	1C	1C	10.0	C0.0	C0.3	.	$= 13^{30} 24$
31	3	1C	1C≡	1C	10.0	C0.0	.	.	$= 0-7^{20} 16^{30} 20^{40} = 7^{20} 16^{30} 20^{40} 24; \bullet 0^{35} 13^{40} \bullet 0-16^{45} 20^{10}$
MES.									
MED.		C8.5	C7.3	C6.2	C7.3	60.7	64.1		

***B) Mesečni i godišnji
pregled***

Mesec	Oblačnost hm (0-10)				Insolacija broj sati	Vlažnost vazduha						Padavine R mm			Broj dana sa:																																										
	7	14	21	Sred. (Dias)		e mm	U m %				Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)		R mm					●	★	✱	Δ	⚡	▲	R T	≡	☐																						
							7	14	21	Sred.				Min	Tn	Tx	Tx	Tx	Tn	F(0-12)	F(0-12)	R	R	R	R																																
																										mm										mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm								
BR. ST. 6 KNEŽEVICA																																								H _s = 2514 m H _b = 2519.0 m h _t = 2.0 m h _r = 1.9 m																	
I	5.2	5.6	5.1	5.4	102.7	01.5	70	74	78	74	14	070	015.8	62	13	29	31	.	.	.	.	11	C5	C6	1C	14	C5	C2	.	14	.	.	.	.	.	.	18	31																			
II	5.2	5.5	3.4	4.8	120.5	01.4	66	65	67	66	12	C98	C23.6	15	19	24	28	.	.	.	.	15	04	05	04	11	09	04	.	11	.	.	.	.	.	01	1C	28																			
III	6.0	6.7	5.5	6.1	120.2	01.7	70	75	76	74	14	C31	011.1	06	18	26	31	.	.	.	.	C7	04	04	12	10	05	C1	.	1C	.	.	.	.	.	15	31																				
IV	6.5	6.5	7.4	7.6	126.0	02.2	86	85	88	88	15	179	048.3	10	15	28	30	.	.	.	.	17	05	.	13	22	17	06	C1	22	.	04	.	01	.	02	23	30																			
V	4.7	6.7	5.5	5.8	225.9	03.6	69	73	75	72	15	067	015.4	25	.	C5	17	.	.	.	.	C9	C3	C3	C5	11	C9	C3	C7	C6	01	C1	.	04	.	06	15	31																			
VI	5.5	7.5	6.2	6.6	182.7	05.0	78	82	84	81	23	263	C92.4	23	.	.	05	.	.	.	.	13	04	01	11	15	12	06	14	C4	C2	01	.	03	.	05	22	18																			
VII	6.5	5.1	7.7	7.7	115.7	05.6	83	84	89	85	44	284	C39.6	23	.	.	06	.	.	.	.	1C	02	.	12	20	18	1C	16	04	01	.	.	05	01	12	24	03																			
VIII	4.6	7.4	6.0	6.1	179.8	06.1	77	84	82	81	36	193	C44.5	29	.	.	.	.	.	.	.	03	.	02	09	14	11	06	14	C1	.	C1	.	C2	.	07	17	.																			
IX	4.5	5.6	5.1	5.1	174.9	04.6	69	70	76	72	16	429	097.5	25	.	.	08	.	.	.	.	C6	02	11	C9	15	14	1C	13	C6	01	02	01	.	.	05	15	04																			
X	5.3	5.1	3.8	4.7	154.4	02.7	60	60	55	62	18	285	117.9	17	C2	07	24	.	.	.	.	13	06	09	08	12	11	04	06	12	C3	03	02	.	.	03	14	30																			
XI	4.2	5.3	3.0	4.2	134.6	01.8	57	58	56	57	13	C40	C26.6	C7	C7	14	29	.	.	.	.	23	15	C9	C3	06	04	C1	01	06	.	.	.	.	.	09	30																				
XII	4.5	6.3	4.1	4.8	104.0	01.7	62	65	66	64	13	123	050.8	22	10	27	31	.	.	.	.	15	14	10	08	1C	C6	05	.	1C	.	01	.	.	01	12	31																				
GCD.	5.3	6.6	5.3	5.7	1711.4	03.2	70	73	74	72	12	2082	117.4	77.8	84	162	240	.	.	.	.	15C	64	6																																	

[illegible]

[illegible]

[illegible]

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetra nD, Fm (0-12)																																																																										
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C																																																										
		7	14	21	Sred. (Dias)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		č.	j.	č.	j.																																																						
φ = 43° 23' N λ = 17° 36' E Gr. ΔG = + 1h 10 min.																													LISTICA																													BR. ST. 131																												
I	-	C1.C	C6.5	C3.7	04.2	C9.3	-0C.7	14.6	04	-0C.8	14.11	1C	C4.7	.	.	.	.	.	.	C2	02.0	.	.	.	01	01.0	.	.	83																																																									
II	-	C2.4	08.8	04.3	05.0	10.1	0C.3	16.2	06	-0C.4	27	15	C3.4	.	.	.	.	.	.	03	01.7	.	.	.	.	.	.	.	66																																																									
III	-	02.9	11.3	C5.5	06.5	12.1	0C.4	18.8	27	-0C.2	01	19	C3.2	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	71																																																									
IV	-	C7.6	13.4	C9.0	C9.7	14.7	C3.5	22.2	30	-02.0	14	13	C4.8	.	.	.	.	.	.	C9	03.0	.	.	.	.	.	.	.	68																																																									
V	-	15.2	23.1	15.3	17.3	24.1	05.1	30.0	06	03.0	11	10	C2.1	.	.	.	.	.	.	C1	C2.0	.	.	C1	02.0	.	.	81																																																										
VI	-	18.2	25.5	18.7	20.3	26.4	12.6	31.6	29	0C.0	17	1C	C2.2	.	.	.	.	.	.	05	01.8	.	.	.	.	.	.	75																																																										
VII	-	15.8	26.0	21.4	22.6	29.3	14.7	35.4	18	05.4	29	09	C2.2	.	.	.	.	.	.	05	02.0	.	.	.	.	.	.	79																																																										
VIII	-	19.2	29.2	21.5	22.8	36.2	15.0	35.0	12	11.8	05.04	04	C2.2	.	.	.	.	.	.	C1	04.0	.	.	.	.	.	.	88																																																										
IX	-	16.1	26.0	18.0	19.6	26.9	12.3	32.0	07.04	06.8	13	06	C2.0	.	.	.	.	.	.	C1	C2.0	.	.	.	.	.	.	83																																																										
X	-	09.8	19.4	11.7	13.1	20.3	07.0	27.6	02	-01.4	29	11	C5.4	.	.	.	.	.	.	C2	03.0	.	.	.	.	.	.	80																																																										
XI	-	C3.3	12.2	C5.3	06.5	12.5	00.8	18.0	17	-1C.6	30	14	C2.6	.	.	.	.	.	.	C2	01.0	.	.	.	.	.	.	74																																																										
XII	-	C2.3	07.5	04.4	04.6	08.6	-0C.4	13.8	29	-13.6	01	07	C2.0	.	.	.	.	.	.	C5	01.4	.	.	.	.	.	.	81																																																										
GCD.	-	05.8	17.7	11.6	12.7	18.7	06.2	35.4	48.VI	-13.6	4.XII	128	C3.2	.	.	.	.	.	.	36	02.2	.	.	C2	01.5	.	.	929																																																										
φ = 43° 50' N λ = 17° 38' E Gr. ΔG = + 1h 10 min.																													PROZGR																													BR. ST. 132																												
I	-	-C2.2	C2.7	-C1.C	-0C.4	04.0	-04.6	05.6	19	-12.6	14	C8	C2.0	.	.	.	.	.	.	3C	02.8	.	.	.	C7	01.6	.	.	48																																																									
II	-	-C1.9	03.3	-0C.7	0C.0	04.5	-04.2	13.4	08	-1C.8	27	11	C1.3	.	.	.	.	.	.	38	02.6	.	.	.	C9	01.4	.	.	26																																																									
III	-	-C1.6	06.2	00.7	01.5	07.3	-03.6	15.8	27	-1C.2	01	17	C1.8	.	.	.	.	.	.	32	02.4	.	.	.	18	C1.9	.	.	26																																																									
IV	-	03.6	09.8	04.3	05.5	11.3	01.C	2C.6	30	-02.6	18	15	C2.1	.	.	.	.	.	.	31	02.5	.	.	.	18	02.2	.	.	26																																																									
V	-	11.6	19.5	11.7	13.6	21.2	06.6	28.4	22	01.6	18	17	C1.8	C1	03.0	C6	C3.2	C7	02.5	.	.	.	.	13	02.1	02	C2.5	47																																																										
VI	-	14.4	21.6	14.7	16.3	23.5	05.8	31.2	28	05.2	16	11	C1.5	C1	C2.0	10	C2.9	.	.	.	.	.	.	16	C2.2	01	C2.0	51																																																										
VII	-	15.9	24.0	15.7	17.8	26.3	11.3	34.8	17	07.6	25	15	C2.2	C1	03.0	.	.	.	.	.	.	.	.	10	02.3	.	.	67																																																										
VIII	-	14.2	24.0	15.6	17.3	25.9	1C.6	3C.8	21.07	07.2	17.16	C9	C1.7	.	.	.	.	.	.	C1	02.0	.	.	.	13	02.1	.	.	70																																																									
IX	-	11.5	22.1	13.4	15.1	24.9	07.6	30.6	24.05	02.6	15.13	C7	C1.3	.	.	.	.	.	.	08	02.8	.	.	.	09	C1.8	01	C2.0	65																																																									
X	-	C5.3	14.9	C7.7	08.9	17.2	02.1	26.6	03.02	-05.2	23	08	C2.0	.	.	.	.	.	.	13	02.8	.	.	.	10	01.5	.	.	62																																																									
XI	-	-01.5	07.2	00.1	01.5	09.3	-05.5	15.4	06	-21.8	30	C2	C2.0	.	.	.	.	.	.	17	02.6	.	.	.	09	C1.8	.	.	62																																																									
XII	-	-02.6	03.5	-C1.5	-00.5	05.2	-06.3	11.8	25	-17.8	11.02	C5	C1.8	.	.	.	.	.	.	18	02.8	.	.	.	04	01.8	.	.	66																																																									
GCD.	-	05.6	13.2	06.7	08.0	15.1	02.1	34.8	47.VI	-21.8	30.XI	125	C1.8	C3	02.7	16	C3.0	19.5	C2.7	.	.	.	.	136	01.9	04	C2.2	616																																																										
φ = 43° 05' N λ = 17° 43' E Gr. ΔG = + 1h 11 min.																													ČAPLJINA-KLEPCI																													BR. ST. 133																												
I	-	C1.6	C5.8	04.7	05.2	10.3	CC.6	14.6	04	-05.0	14	16	C2.1	C7	01.7	C1	02.0	C4	01.0	.	.	.	C1	01.0	.	.	C1	C3.0	63																																																									
II	-	03.6	10.9	C5.6	06.5	11.8	02.5	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.																																																										
III	-	C3.1	12.7	06.7	07.3	13.6	01.7	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.																																																										
IV	-	08.8	15.0	09.7	10.8	16.4	05.2	22.0	30	01.0	18.16	11	C1.9	C5	02.0	C1	03.0	12	03.4	C6	02.5	10	02.1	.	.	02	C2.0	43																																																										
V	-	16.2	24.2	16.1	18.1	25.5	1C.0	32.5	06	05.0	11	07	C3.0	C6	02.5	.	.	.	C7	01.6	C3	03.3	14	02.1	.	.	04	01.2	52																																																									
VI	-	20.0	27.0	15.3	21.4	28.0	14.0	33.0	29	05.2	17	C6	C3.0	C3	02.3	C1	C4.0	C7	02.9	C2	03.5	11	02.6	03	03.3	02	C2.5	55																																																										
VII	-	21.8	29.4	21.5	23.5	30.6	16.0	36.5	18	11.5	29	07	C1.7	C1	02.0	.	.	.	C2	02.0	C6	02.2	14	02.6	01	C3.0	04	C2.2	58																																																									
VIII	-	18.8	29.6	21.2	22.7	30.7	15.3	35.0	08	11.5	16	C2	C2.5	C3	02.7	.	.	.	02	02.0	03	02.0	13	02.6	.	.	02	03.0	68																																																									
IX	-	16.2	27.4	18.6	20.2	28.3	13.2	33.0	06	07.0	13	C6	C2.2	C3	02.7	.	.	.	C8	02.0	.	.	.	12	02.1	.	.	01	C2.0	60																																																								
X	-	10.1	21.1	12.8	14.2	22.0	08.0	25.0	02	-0C.5	29	C7	C2.7	C9	03.8	C2	C1.5	C9	03.2	03	01.7	03	01.0	01	02.0	03	C2.0	56																																																										
XI	-	03.3	13.8	C6.4	07.4	14.9	01.0	21.0	17	-0C.5	29	13	C3.1	C4	03.8	.	.	.	04	02.5	C1	02.0	C2	C2.5	.	.	02	03.5	64																																																									
XII	-	04.C	08.9	05.2	05.8	10.1	01.3	16.5	26	-1C.0	02	1C	C2.3	C4	02.2	C1	C1.0	16	04.2	C2	03.5	.	.	.	03	C3.7	57																																																											
GCD.	-	10.6	19.2	12.3	13.6	20.2	07.4	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.																																																										
φ = 43° 40' N λ = 17° 46' E Gr. ΔG = + 1h 11 min.																													JABLANICA																													BR. ST. 134																												
I	-	0C.2	C6.0	C3.0	03.1	06.7	-0C.2	12.4	21	-05.6	27	13	C2.7	.	.	.	.	.	.	C3	02.0	.	.	.	C1	C3.0	.	.	72																																																									
II	-	C2.1	C7.8	04.7	04.8	08.7	01.5	17.0	08	-04.0	13	13	C2.5	.	.	.	.	.	.	C3	C2.3	.	.	.	C9	03.0	.	.	53																																																									
III	-	C2.1	10.8	C5.0	05.7	11.8	01.6	20.4	28	-04.0	02	08	C2.5	.	.	.	.	.	.	C9	C2.5	.	.	.	C1	C3.0	.	.	72																																																									
IV	-	07.1	14.1	09.8	10.2	15.7	05.5	25.2	30	CC.8	14	16	C2.7	.	.	.	.	.	.	10	02.6	.	.	.	09	03.4	.	.	41																																																									
V	-	14.0	23.9	18.C	18.5	25.3	11.7	32.6	22.06	05.4	17	1C	C2.8	C1	02.0	C8	C2.6	.	.	.	16	C3.1	.	.	.	C5	03.0	.	53																																																									
VI	-	16.6	25.4	2C.C	20.5	26.8	14.3	32.4	29	08.0	16	13	C2.2	.	.	.	.	.	.	C4	C2.5	.	.	.	15	03.1	.	.	50																																																									
VII	-	18.7	27.5	22.7	22.9	29.1	16.0	37.0	18	12.2	28.27	09	C2.3	.	.	.	.	.	.	C2	C3.5	.	.	.	09	03.8	.	.	70																																																									
VIII	-	18.1	27.9	20.3	21.6	29.2	15.3	34.0	07	12.0	16	14	C2.8	C2	02.0	C4	C2.8	.	.	.	C4	C2.8	.	.	.	06	02.7	.	63																																																									
IX	-	14.5	25.3	19.4	19.6	26.6	13.2	32.0	08.05	10.0	28	09	C2.7	.	.	.	.	.	.	C4	C2.8	.	.	.	C6	C3.2	.	.	68																																																									
X	-	C5.8	17.8	11.9	12.9	19.0	08.1	26.0	03	01.C	30	17	C2.4	.	.	.	.	.	.	C4	C3.0	.	.	.	C5	03.4	.	.	58																																																									
XI	-	C2.7	C5.7	C4.C	05.1	11.5	0C.1	18.0	16	-12.4	30	14	C2.5	C2	02.5	C1	C3.C	.	.	.	04	03.C	.	.	.	1C	C2.8	.	59																																																									
XII	-	01.5	C5.4	02.4	02.9	07.1	-00.5	16.0	26	-11.6	02.01	10	C2.4	.	.	.	.	.	.	C5	03.4	.	.	.	14	C4.1	.	.	52																																																									
GCD.	-	09.0	16.8	11.8	12.3	18.1	07.2	37.0	48.VII	-12.4	30.XI	146	C2.6	C5	02.2	58	C2.8	.	.	.	99	C3.3	.	.	.	75	C3.0	01	C3.0	711																																																								
φ = 43° 09' N λ = 17° 47' E Gr. ΔG = + 1h 11 min.																													DOLANJEVIĆI																													BR. ST. 135																												
I	-	C3.7	C5.2	05.1	05.7	10.C	C2.1	12.5	04	-03.2	11	4C	C2.7	.	.	.	.	.	.	C8	02.6	.	.	.	.	.	.	.	45																																																									
II	-	04.6	C5.8	C5.4	06.3	10.5	02.0	15.0	07	-04.6	27	23	C3.0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	35																																																									
III	-	04.8	11.9	07.1	07.8	12.4	02.3	15.4	31	-04.0	01	4C	C3.0	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	39																																																									
IV	-	09.4	15.0	10.3	11.3	15.4	05.5	2C.5	30	CC.8	16	19	C3.2	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	40																																																									
V	-	17.3	23.7	16.4	18.5	24.2	11.1	31.0	06	04.4	11	19	C3.1	.	.	.	.	.	.	.	.	.	.	.	.	.	.																																																											

Mesec	Vazdušni pritlak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																																					
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C																					
		7	14	21	Sred. (Djes)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		č.	j.	č.																		
φ = 43° 21' N λ = 17° 48' E Gr. ΔG = + 1h 11 min.																														MCSTAR										BR. ST. 136									
I	756.1	C4.2	C6.4	C5.7	C6.0	09.1	03.6	14.2	04	-03.4	15	25	C4.0	33	C4.7	C3	C3.7	.	.	C1	C1.0	C1	C3.0	C2	C2.0	C7	C2.6	21																					
II	745.3	C4.5	C9.6	C6.1	C6.6	10.6	03.8	16.7	08	-01.2	27	29	C3.9	26	C3.8	C1	C4.0	C2	C2.0	C6	C3.5	C3	C2.3	C4	C2.0	C4	C3.0	09																					
III	754.6	C5.5	12.6	07.8	08.4	13.1	04.4	20.4	31	-02.9	02	32	C3.9	34	C4.0	C4	C2.2	C2	C2.5	C4	C1.8	C1	C2.0	C2	C2.0	C5	C3.6	09																					
IV	745.5	08.7	14.9	10.2	11.0	16.2	06.2	25.0	30	01.8	13	14	C3.4	19	C2.8	C2	C3.0	C6	C3.3	C7	C3.1	12	C2.4	C5	C1.8	C3	C2.0	22																					
V	752.7	15.8	24.6	17.8	15.0	25.6	12.5	32.8	06	05.0	11	19	C3.2	10	C4.7	C2	C3.0	C2	C1.5	C4	C1.8	C7	C2.6	13	C2.0	C6	C2.7	30																					
VI	752.8	19.6	27.2	20.8	22.1	28.0	16.0	33.4	29	11.6	20	23	C2.5	14	C3.4	C3	C3.0	C3	C2.0	C8	C2.2	11	C2.5	07	C2.1	C6	C2.3	15																					
VII	745.6	21.9	30.0	23.7	24.8	31.3	18.8	37.7	18	13.4	29	27	C3.1	22	C2.8	C3	C2.0	C2	C1.5	C4	C2.8	09	C2.7	C9	C2.1	C6	C3.5	11																					
VIII	753.1	21.8	30.7	23.6	24.9	31.5	15.6	37.3	21	14.9	05	30	C3.1	29	C3.2	C2	C2.5	C3	C2.3	C6	C2.0	04	C3.2	C4	C2.0	C5	C2.6	10																					
IX	752.8	18.6	27.9	20.7	22.0	28.5	16.6	34.4	05	11.6	30	21	C3.1	22	C3.0	C2	C2.0	C1	C3.0	C5	C2.4	C2	C2.5	C2	C1.5	09	C3.1	26																					
X	753.6	13.2	20.0	14.9	15.7	21.0	12.0	28.9	03	04.1	24	27	C3.9	28	C3.8	C1	C1.0	C2	C3.0	C5	C2.6	C4	C1.8	C6	C2.0	C4	C2.8	16																					
XI	756.0	06.3	12.3	07.5	08.4	13.2	04.6	21.7	17	-04.8	29	38	C3.9	08	C6.2	.	.	C1	C2.0	C3	C2.7	C2	C2.0	C3	C1.3	05	C4.4	30																					
XII	754.3	04.3	07.7	05.3	05.7	08.8	02.6	15.3	24	-07.0	01	34	C2.8	10	C4.2	.	.	C3	C3.3	C4	C3.0	C1	C3.0	11	C1.9	C6	C3.3	24																					
GDD.	752.5	12.0	18.8	13.7	14.6	15.8	10.1	37.7	48.VI	-07.0	1.XII	319	C3.4	255	03.7	23	C2.6	27	C2.5	57	C2.5	57	C2.5	68	C1.9	66	C3.0	223																					
φ = 43° 24' N λ = 17° 53' E Gr. ΔG = + 1h 12 min.																														POTOCI-ZELJUŠA										BR. ST. 137									
I	-	C3.6	C7.9	04.8	05.3	08.5	02.3	13.2	30.04	-05.0	15	.	.	14	02.3	.	.	C4	C1.5	.	.	04	C1.5	.	.	70	C3.0	01																					
II	-	C4.3	08.9	05.2	05.9	10.2	03.0	17.5	07	-01.2	27	.	.	19	02.2	.	.	C3	C1.7	.	.	08	C2.8	.	.	54	C2.6	.																					
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																					
IV	-	05.6	14.6	10.5	11.3	16.0	05.9	24.3	30	01.0	13	.	.	17	C1.7	.	.	C4	C1.2	.	.	26	C3.1	.	.	43	C2.2	.																					
V	-	16.6	24.0	16.7	18.5	25.3	11.5	31.8	06	03.5	11	.	.	19	02.1	.	.	C4	C1.5	.	.	23	C2.3	.	.	47	C2.0	.																					
VI	-	15.6	26.6	15.6	21.4	27.7	14.7	32.2	29	10.9	17	.	.	12	01.8	.	.	C5	C1.4	.	.	18	C2.6	.	.	55	C1.9	.																					
VII	-	22.5	29.3	22.8	24.4	31.2	17.3	37.8	18	11.8	29	.	.	24	01.4	.	.	C3	C1.7	.	.	11	C3.4	.	.	55	C2.4	.																					
VIII	-	22.1	30.4	22.6	24.4	31.9	18.4	37.1	22	14.7	05	.	.	29	02.0	.	.	C2	C2.0	.	.	13	C2.4	.	.	49	C2.6	.																					
IX	-	18.5	26.9	19.4	21.1	27.9	15.4	34.5	05	11.5	30	.	.	22	02.0	.	.	C4	C1.5	.	.	14	C2.4	.	.	50	C2.5	.																					
X	-	12.8	19.3	14.0	15.0	20.4	10.6	28.2	02	02.9	24	C2	C1.0	22	C2.0	.	.	C4	C1.2	.	.	10	C2.5	01	C2.0	54	C3.0	.																					
XI	-	05.8	11.9	06.7	07.8	12.9	03.5	20.3	17	-06.8	29	19	C1.6	17	C2.2	.	.	C5	C1.4	01	C1.0	07	C1.9	03	C1.0	38	C2.8	.																					
XII	-	03.9	07.4	05.1	05.4	08.6	01.8	16.2	25.24	-07.3	01	22	C1.6	08	C1.8	.	.	C2	C1.0	.	.	05	C2.8	02	C1.0	54	C3.1	.																					
GDD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																					
φ = 43° 46' N λ = 18° 02' E Gr. ΔG = + 1h 12 min.																														IVAN SEDLC										BR. ST. 138									
I	-	-C3.0	-C6.7	-02.0	-01.9	00.0	-C4.1	C9.0	19	-11.6	14	.	.	20	01.4	28	01.6	.	.	.	.	17	C2.9	14	C3.9	.	.	14																					
II	-	-02.6	C6.3	-C1.2	-01.2	01.4	-03.6	05.3	08	-10.4	13	04	C1.5	23	C1.7	15	C2.5	.	.	.	.	09	C4.4	12	C4.8	.	.	17																					
III	-	-C2.1	C2.4	-C6.2	00.0	02.9	-03.1	11.6	27	-08.8	01	02	C1.5	29	C1.9	28	C2.5	.	.	.	.	C7	C1.9	C2	C2.5	.	.	25																					
IV	-	-02.8	C7.2	-03.7	04.4	C6.2	00.8	16.5	30	-04.8	14	01	C2.0	14	C2.1	12	C2.5	.	.	.	.	03	C4.7	22	C4.0	19	C4.3	19																					
V	-	11.1	16.5	11.6	12.7	17.9	07.4	27.0	06	00.6	14	04	C2.8	21	C1.4	C8	C2.2	.	.	.	.	18	C3.3	29	C3.6	.	.	13																					
VI	-	13.6	18.9	14.1	15.2	20.1	10.3	27.2	29	02.4	17	04	C1.0	26	C1.5	C8	C2.2	.	.	.	.	17	C2.6	24	C2.6	.	.	11																					
VII	-	15.1	21.2	15.5	16.8	22.0	11.5	30.2	18	07.6	29	05	C1.2	28	C1.5	C4	C1.8	.	.	.	.	C5	C4.2	27	C2.8	.	.	24																					
VIII	-	13.9	20.7	14.9	16.1	21.3	11.2	26.3	21	07.2	16	02	C1.0	35	C1.7	C4	C1.5	.	.	.	.	04	C1.2	06	C2.0	.	.	42																					
IX	-	11.9	18.5	13.1	14.2	19.3	05.6	24.6	25.09	03.5	14.13	03	C3	C2.0	17	C2.0	10	C2.3	.	.	.	.	11	C3.4	15	C2.6	.	.	30																				
X	-	05.6	10.8	06.7	07.4	11.5	03.9	20.0	01	-02.8	30	01	C1.0	36	C1.8	13	C2.5	.	.	.	.	14	C4.6	15	C4.2	.	.	14																					
XI	-	-C6.7	C3.6	-C6.6	01.0	05.0	-02.8	12.0	16	-13.0	29	.	.	29	01.9	09	03.0	.	.	.	.	01	C2.0	24	C4.6	16	C5.9	.	11																				
XII	-	-01.9	06.8	-00.7	-00.6	02.1	-04.2	05.1	31	-15.4	11	01	C1.0	10	C3.0	C7	C3.9	.	.	.	.	36	C4.2	23	C5.4	.	.	16																					
GDD.	-	05.3	10.0	06.3	07.0	11.0	03.1	30.2	48.VII	-15.4	1.XII	27	C1.6	288	01.8	150	C2.3	.	.	.	.	04	C4.0	184	03.7	206	C3.8	.	236																				
φ = 43° 06' N λ = 18° 11' E Gr. ΔG = + 1h 13 min.																														BERKVIČI										BR. ST. 139									
I	-	C1.5	C6.1	C3.0	03.4	C6.6	-00.1	10.8	08	-C6.2	14	31	C3.4	12	C1.8	18	C1.7	.	.	.	.	16	C1.2	C2	C2.0	.	.	12																					
II	-	C1.6	C6.2	C2.9	03.4	C6.8	-00.2	14.0	06	-07.8	27	30	C2.6	16	C2.1	18	C1.8	.	.	.	.	06	C1.8	C2	C2.0	.	.	14																					
III	-	C2.8	C8.3	04.1	04.8	C8.7	00.6	16.8	31	-05.2	01	39	C2.5	17	C1.8	12	C1.8	.	.	.	.	C7	C1.7	C4	C1.8	.	.	14																					
IV	-	06.9	12.1	07.6	08.5	12.6	03.5	20.0	30	-00.2	23	21	C2.9	18	C2.4	20	C2.0	.	.	.	.	14	C1.6	C6	C2.0	.	.	11																					
V	-	14.7	22.3	14.3	16.4	22.9	05.3	31.4	06	02.0	11	22	C2.5	C3	C1.7	10	C1.3	.	.	.	.	17	C1.3	12	C2.1	.	.	29																					
VI	-	17.7	24.1	17.0	18.9	24.4	12.5	31.0	29	08.2	20.18	22	C2.7	C8	C1.8	11	C1.8	.	.	.	.	15	C1.7	11	C2.0	.	.	23																					
VII	-	20.0	27.3	15.6	21.6	28.1	14.8	35.6	18	09.2	29	19	C2.5	C1	C1.0	C7	C1.9	.	.	.	.	18	C1.7	18	C2.0	.	.	30																					
VIII	-	18.8	26.1	19.1	20.8	27.1	14.6	32.4	22	11.2	06	23	C2.6	C5	C1.9	C8	C1.8	.	.	.	.	18	C1.5	C2	C2.0	.	.	33																					
IX	-	16.0	24.3	16.5	18.3	25.0	12.4	30.2	07	07.8	15	17	C3.4	C6	C2.0	C1	C1.0	.	.	.	.	25	C1.4	C2	C2.0	.	.	39																					
X	-	10.3	17.7	11.5	12.7	18.3	07.7	26.0	02	01.0	29	37	C2.4	C3	C2.0	C3	C1.7	.	.	.	.	26	C1.8	C2	C1.5	.	.	22																					
XI	-	03.0	C9.8	C4.0	05.2	10.5	00.8	16.6	17	-10.0	29	30	C5.4	.	.	C3	C4.7	09	01.4	.	.	22	C1.6	C1	C2.0	.	.	21																					
XII	-	00.9	C5.5	02.4	02.8	06.0	-C1.0	12.0	25	-12.4	01	15	C3.7	31	C2.1	C3	C2.0	.	.	.	.	17	C1.8	C1	C3.0	.	.	26																					
GDD.	-	09.5	15.8	10.2	11.4	16.4	06.2	35.6	48.VII	-12.4	1.XII	306	C2.8	131	C2.0	120	C1.7	.	.	.	.	201	C1.6	63	C2.0	.	.	274																					
φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min.																														BJELAŠNICA										BR. ST. 140									
I	552.1	-C6.2	-C5.3	-C6.0	-05.9	-04.0	-C7.8	00.0	02	-14.2	13	29	C6.3	13	C3.9	C2	C5.0	C4	C4.0	15	C5.5	23	C5.2	C1	C2.0	C1	C2.0	05																					
II	585.7	-C7.4	-C6.6	-07.4	-07.2	-04.8	-05.5	00.2	08	-17.4	28	37	C6.2	C4	C4.0	.	.	.	.	18	C6.6	17	C6.6	.	.	05	C4.4	03																					
III	550																																																

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Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetra nD, Pm (0-12)																																					
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C																					
		7	14	21	Sred. (Dias)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		č.	j.	č.	j.																	
φ = 43° 50' N λ = 18° 20' E Gr. ΔG = + 1h 13 min.																														SARAJEVC-AERODROM																BR. ST.141			
I	721.7	-02.1	01.8	-00.4	-00.3	02.6	-02.9	09.5	17	-11.6	14	.	.	C1	C3.0	C1	C2.0	C5	02.8	C1	01.0	.	.	05	01.6	13	C2.2	67																					
II	714.6	-00.6	03.7	00.6	01.1	05.2	-02.2	15.2	08	-08.8	13	01	C2.0	C2	01.5	C4	02.2	C5	03.8	C3	02.0	01	01.0	06	03.2	24	C2.2	34																					
III	719.5	-00.1	06.3	02.8	02.9	07.4	-01.1	17.0	27	-06.5	01	05	C2.0	C2	02.0	C5	02.4	05	02.2	04	01.2	.	.	14	02.1	13	C2.2	45																					
IV	714.5	04.3	11.4	06.7	07.3	12.9	02.1	22.2	30	-05.1	07	02	C2.0	C2	02.0	07	02.1	09	03.0	C7	04.3	02	03.0	09	03.7	11	C2.5	41																					
V	719.4	11.0	20.7	13.8	14.8	22.1	07.1	32.8	06	01.0	14	03	C3.3	C4	01.5	C3	C1.7	06	03.0	C4	02.0	02	03.0	17	02.7	14	02.6	40																					
VI	716.8	14.2	22.8	16.8	17.7	24.5	10.6	31.7	29	02.2	17	05	C2.0	C1	03.0	C5	01.8	06	02.7	04	02.8	.	.	08	02.5	18	02.5	43																					
VII	716.5	15.9	24.8	18.2	15.3	26.2	12.4	36.4	18	09.4	31	03	C1.7	C1	01.0	C2	C1.5	03	02.7	04	02.5	04	03.0	17	02.1	15	02.5	44																					
VIII	720.3	13.5	24.2	17.2	18.0	25.3	11.2	30.4	21	07	02	02	C3.5	.	.	C5	02.4	C6	01.7	C4	01.8	.	.	20	02.1	06	C2.0	50																					
IX	719.5	11.4	22.3	14.7	15.8	23.4	05.6	29.4	25	02.6	13	03	C1.7	.	.	C4	C1.5	02	02.0	06	03.0	.	.	19	01.8	05	02.2	51																					
X	720.1	06.1	13.6	07.7	08.8	15.0	04.2	24.8	17	-03.1	28	02	C2.5	.	.	C7	C2.6	C3	01.7	05	03.8	01	02.0	12	02.5	04	01.8	59																					
XI	721.0	-01.6	06.6	00.6	01.6	08.8	-04.0	17.9	06	-21.2	29	05	C1.8	01	02.0	C3	C1.3	03	02.3	06	01.8	02	01.5	07	02.0	03	02.3	60																					
XII	718.8	-03.7	01.2	-01.8	-01.5	03.3	-06.7	13.6	26	-24.6	01	01	C1.0	.	.	C1	02.0	16	04.5	C4	02.2	.	.	06	02.3	06	C2.7	59																					
GCD.	718.7	05.7	13.3	08.1	08.8	14.7	03.4	36.4	48	-24.6	4	XII	32	C2.1	14	C1.9	47	02.1	73	03.1	52	02.6	12	02.5	140	02.3	132	C2.3	593																				
φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min.																														SARAJEVC																BR. ST.142			
I	710.4	-01.7	02.1	-00.1	00.0	02.9	-02.4	10.2	17	-05.6	14	03	C1.0	04	01.5	15	C2.2	17	02.5	C5	01.2	04	02.0	13	01.2	07	C1.3	25																					
II	703.4	-00.6	03.6	00.9	01.2	05.2	-01.5	15.1	08	-07.6	13	04	C1.0	.	.	11	02.1	08	02.2	03	01.0	15	02.5	20	01.6	12	C1.3	11																					
III	708.4	00.1	06.0	02.3	02.7	06.8	-00.6	15.6	28	-06.5	01	02	C1.0	C5	01.2	24	02.6	15	02.4	04	01.0	03	01.0	12	01.5	07	C1.3	17																					
IV	703.7	04.9	10.9	07.1	07.5	12.5	02.8	21.4	30	-01.0	07	03	C2.3	.	.	17	02.4	09	02.7	09	04.4	08	02.8	20	02.0	11	C2.0	13																					
V	708.7	11.9	20.2	15.0	15.5	21.6	06.8	31.5	06	02.5	14	01	C2.0	C1	02.0	14	C1.9	12	01.7	C6	02.5	06	01.8	24	02.3	07	02.0	22																					
VI	706.2	14.6	22.1	17.3	17.8	23.5	11.8	31.0	29	04.0	17	02	C1.5	C3	02.3	12	C1.9	08	02.1	07	02.4	07	02.0	19	01.9	06	01.7	26																					
VII	706.0	16.0	24.4	18.5	19.4	25.4	13.4	35.5	18	05.8	31	03	C2.3	C1	01.0	10	C1.8	12	01.5	C2	01.0	09	02.4	18	02.1	10	01.6	28																					
VIII	705.7	14.3	24.4	17.5	18.4	25.5	12.1	30.4	22	07.5	11	05	C1.2	04	02.0	16	02.0	21	01.8	C3	01.3	03	01.7	07	01.6	05	01.6	29																					
IX	705.0	12.5	22.4	15.3	16.4	23.4	10.6	29.2	25	04.0	13	01	C2.0	.	.	11	C2.1	26	01.9	C4	C2.0	01	01.0	14	01.6	11	01.8	20																					
X	705.3	06.3	13.9	08.7	09.4	15.1	04.8	24.5	17	-03.1	29	02	C1.5	C2	02.0	15	C2.4	19	02.3	07	03.0	07	02.1	09	01.3	02	C2.0	30																					
XI	710.0	00.3	07.3	03.0	03.4	09.0	-01.1	17.2	06	-13.5	29	02	C3.5	.	.	08	02.6	19	01.6	05	03.0	10	02.0	19	01.7	09	02.0	18																					
XII	707.6	-01.4	02.6	00.4	00.5	04.3	-03.6	13.5	25	-16.5	01	02	C2.5	.	.	11	02.1	12	02.2	12	03.5	09	03.1	16	01.5	05	02.0	26																					
GCD.	707.9	06.4	13.3	08.8	09.4	14.6	04.6	35.5	45	-16.5	4	XII	30	C1.7	20	01.7	164	C2.2	184	02.0	67	02.7	82	02.3	191	01.8	92	01.7	265																				
φ = 43° 31' N λ = 18° 27' E Gr. ΔG = + 1h 14 min.																														KALINOVIK																BR. ST.143			
I	673.9	-01.5	00.3	-00.9	-00.8	00.9	-02.8	06.7	31	-10.4	11	02	C2.5	12	C2.6	38	C1.7	06	01.0	C3	01.0	04	02.0	08	01.2	02	C1.0	18																					
II	667.0	-01.2	01.4	-00.2	00.0	02.5	-02.2	10.5	08	-10.4	13	10	C2.3	12	02.0	18	C1.7	C7	01.1	C4	C1.0	16	02.8	04	02.8	05	01.4	08																					
III	670.5	-01.3	02.0	00.0	00.2	02.4	-02.5	11.6	24	-08.8	23	10	C2.2	25	01.8	30	C1.9	05	01.0	03	01.0	.	.	03	01.0	05	01.6	12																					
IV	667.3	03.4	07.4	04.5	05.0	08.4	01.7	18.2	30	-02.9	07	16	C2.4	10	01.4	C6	C1.0	C3	01.0	C9	02.4	26	03.5	10	02.7	.	.	10																					
V	673.7	11.4	16.8	11.5	12.8	17.6	07.6	28.1	06	01.9	10	14	C2.2	15	01.7	C5	C1.0	C4	01.2	08	01.0	21	03.0	10	02.1	04	01.0	08																					
VI	673.5	13.5	18.5	14.2	15.1	19.8	05.9	27.4	29	04.3	17	06	C2.7	C6	02.0	16	C1.8	C6	01.5	06	01.0	25	02.6	13	02.0	04	C1.0	08																					
VII	671.5	15.4	21.4	15.7	17.1	22.2	11.7	31.9	18	07.3	29	15	C1.5	16	01.6	11	C1.8	06	01.2	03	01.3	18	02.9	08	02.0	06	01.0	10																					
VIII	675.1	14.0	20.3	14.5	15.9	21.1	11.3	25.3	21	08.4	21	07	C1.6	C8	01.8	27	02.0	12	01.4	C3	01.3	C3	01.3	01	03.0	02	C1.5	30																					
IX	673.8	12.6	19.4	13.3	14.7	20.2	05.8	26.4	25	04.4	14	07	C1.5	C8	02.1	15	01.5	C5	01.0	04	01.2	14	02.7	05	02.0	01	01.0	31																					
X	673.0	06.8	11.8	08.3	08.8	13.1	05.0	23.4	03	-01.7	23	03	C2.0	C9	02.2	34	C2.2	06	01.3	02	01.0	14	04.3	10	02.0	01	02.0	14																					
XI	672.5	01.1	04.8	01.8	02.4	06.1	-01.3	14.3	04	-17.0	29	03	C3.0	C3	03.0	30	C2.3	C3	01.0	01	01.0	19	04.1	17	02.4	.	.	14																					
XII	670.4	-00.2	02.3	00.3	00.6	03.2	-04.0	09.8	31	-17.4	01	01	C3.0	C8	03.0	12	01.8	C7	01.1	11	01.6	17	04.0	27	02.6	.	.	10																					
GCD.	671.8	06.2	10.5	06.9	07.6	11.5	03.7	31.9	48	-17.4	4	XII	54	C2.1	136	02.0	242	01.5	70	01.2	57	01.3	177	03.2	116	02.2	30	C1.2	173																				
φ = 43° 10' N λ = 18° 33' E Gr. ΔG = + 1h 14 min.																														GACKO																BR. ST.144			
I	-	-01.9	02.5	-00.6	-00.1	03.3	-03.0	07.0	09	-08	14	.	.	43	03.7	.	.	10	02.5	C2	C2.0	01	C2.0	.	.	08	03.0	29																					
II	-	-01.5	02.4	-00.6	-00.1	03.2	-03.1	11.0	08	-07	27	.	.	40	03.6	.	.	24	03.1	01	02.0	.	.	.	11	03.3	08																						
III	-	-01.5	04.0	00.1	00.7	04.7	-02.8	14.0	31	-05.0	01	C1	C2.0	60	03.2	C1	C2.0	C4	02.0	.	.	.	03	03.0	17	02.3	07																						
IV	-	03.4	08.0	04.2	05.0	09.3	01.0	19.5	30	-02.6	18	.	.	23	03.3	.	.	34	03.6	.	.	09	03.6	01	04.0	13	C2.4	10																					
V	-	11.7	18.4	11.8	13.4	19.8	06.3	29.0	06	-01.0	11	C1	C4.0	40	02.9	.	.	14	02.8	C2	03.0	07	02.9	02	02.5	10	C2.3	17																					
VI	-	14.3	20.4	14.4	15.9	21.5	09.6	28.0	29	05.0	20	C1	C2.0	22	03.0	C1	C2.0	21	02.7	05	02.6	03	02.3	.	.	10	02.8	27																					
VII	-	16.1	23.1	16.2	17.9	24.1	11.3	31.0	18	07.4	28	C1	C2.0	43	02.8	C1	C2.0	C4	02.5	01	02.0	16	02.9	.	.	04	02.5	23																					
VIII	-	15.3	22.2	16.0	17.4	23.6	11.4	29.5	23	08.2	21	.	.	47	02.7	.	.	20	02.2	.	.	03	02.3	.	.	07	02.1	16																					
IX	-	13.0	21.1	14.2	15.6	22.0	09.3	26.5	09	05	15	02	C2.0	38	02.9	.	.	15	02.6	.	.	09	02.8	01	02.0	05	02.2	16																					
X	-	08.7	14.0	08.7	09.5	15.2	04.4	23.5	02	-03.0	29	01	C3.0	47	03.4	.	.	25	02.8	01	03.0	05	03.2	.	.	01	03.0	13																					
XI	-	00.0	06.5	01.5	02.4	07.7	-02.0	15.0	11	-16.0	29	.	.	48	03.3	.	.	15	02.4	C3	03.0</																												

Mesec	Vazdušni pritisk Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra ND, Pm (0-12)																									
		Tm				Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C																	
		7	14	21	Sred. (Dias)																																
φ = 43° 57' N λ = 18° 49' E Gr. ΔG = + 1h 15 min.																						SKELJAC										BR. ST. 146					
I	-	-05.7	-01.3	-04.2	-03.8	-06.7	-07.0	05.4	31	-18.6	15	18	C2.0	C1	01.0	.	.	C2	01.0	C5	01.0	02	01.0	.	.	07	C2.3	58									
II	-	-03.5	C1.3	-02.2	-01.6	C2.5	-04.8	11.0	08	-14.8	19	22	C2.3	.	.	.	.	C2	01.0	11	C2.7	C1	01.0	.	.	10	C2.8	38									
III	-	-03.4	02.4	-01.0	-00.8	C3.1	-04.5	1C.6	31	-13.0	18	20	C1.4	.	.	C1	01.0	.	.	09	01.4	01	01.0	.	.	09	C1.9	53									
IV	-	01.9	08.9	03.9	04.6	09.9	0C.0	15.3	10	-06.7	07	22	C2.1	C1	01.0	.	.	C4	02.8	24	C2.6	03	01.3	.	.	09	C2.8	27									
V	-	09.4	17.8	11.6	12.6	18.9	05.5	29.2	06	-03.0	09	17	C1.6	.	.	.	.	.	12	01.6	01	01.0	.	.	15	01.9	48										
VI	-	12.4	19.7	13.9	15.0	21.1	08.3	29.5	29	-00.4	17	17	C1.5	.	.	.	C1	01.0	10	01.5	06	C1.7	.	.	08	C2.2	48										
VII	-	13.6	21.6	14.5	16.3	22.6	05.6	32.0	18	05.4	31	09	C1.4	.	.	.	.	17	01.5	03	02.0	.	.	05	C2.2	59											
VIII	-	10.6	21.5	14.0	15.0	22.8	07.7	27.5	23	02.4	16	05	C1.0	06	02.0	.	.	.	08	01.1	03	C1.3	01	02.0	03	C1.7	67										
IX	-	08.4	19.5	11.8	12.9	20.8	06.4	26.2	06	-01.6	13	03	C1.3	C3	C2.0	.	.	1C	01.6	C5	C1.4	08	01.7	01	01.0	07	C2.4	58									
X	-	C2.7	13.0	06.2	07.0	13.9	00.6	22.6	17	01	29	10	C2.2	C1	01.0	.	.	04	02.0	12	02.6	01	01.0	.	.	12	C2.6	53									
XI	-	-C3.5	04.8	-C1.3	-00.4	04.6	-06.1	15.2	06	-25.2	29	13	C1.6	.	.	C1	02.0	.	.	14	01.6	05	01.6	.	.	08	C2.4	49									
XII	-	-C6.6	-00.7	-04.4	-00.4	00.9	-09.5	11.5	25	-27.5	11	07	C2.4	.	.	.	.	C4	01.2	20	01.3	02	02.5	.	.	06	C2.2	54									
GDD.	-	03.0	10.7	05.3	04.1	11.5	0C.5	32.0	48.VII	-27.5	M.XII	163	C1.8	12	C1.8	C2	C1.5	27	01.7	147	01.8	31	01.6	02	01.5	99	02.3	612									
φ = 43° 40' N λ = 18° 59' E Gr. ΔG = + 1h 16 min.																						GČRAŽICE										BR. ST. 147					
I	-	-C1.6	C2.0	-00.5	-00.1	02.3	-03.3	1C.4	31	-11.5	14	.	.	16	C1.0	.	.	C1	01.0	.	.	04	01.0	.	.	03	01.0	69									
II	-	00.0	C5.1	C1.2	01.9	05.9	-01.5	13.6	10	-07.0	13	.	.	17	01.3	.	.	.	.	.	10	01.1	.	.	05	C1.4	52										
III	-	01.0	C7.6	C3.2	C3.8	08.2	-00.3	17.0	27	-05.0	01	.	.	13	01.3	.	.	C5	01.1	.	.	02	01.5	.	.	07	C1.1	62									
IV	-	06.1	12.9	07.4	08.5	14.3	02.3	22.6	30	-01.0	23	C3	C2.0	04	01.0	C1	01.0	10	01.3	C6	03.8	09	01.1	01	02.0	08	C1.8	48									
V	-	12.2	22.3	13.5	15.4	23.0	07.5	34.2	06	03.0	14	.	.	C6	C1.2	.	.	C8	01.0	.	.	15	01.1	.	.	02	01.0	62									
VI	-	15.1	24.1	16.4	18.0	25.1	11.5	33.2	29	07.0	20	18	.	.	C3	01.0	.	.	15	01.0	.	.	08	01.0	.	.	03	01.0	60								
VII	-	16.5	25.8	17.5	19.3	27.1	13.2	35.4	18	1C.0	28	01	.	.	.	.	.	05	01.1	.	.	19	01.1	.	.	03	01.0	62									
VIII	-	14.6	25.5	16.6	18.3	26.5	11.5	31.4	21	07.0	12	.	.	C6	01.2	.	.	C8	01.1	.	.	16	01.1	.	.	01	C1.0	62									
IX	-	12.9	24.0	14.5	16.5	25.1	10.8	36.6	10	04.5	13	12	C4	C1.0	C1	01.0	.	.	1C	01.6	01	01.0	08	01.0	.	.	01	01.0	65								
X	-	07.3	14.9	08.0	09.6	15.8	05.2	27.6	17	-04.0	28	.	.	C6	01.0	.	.	1C	01.1	.	.	15	01.5	.	.	08	01.5	54									
XI	-	00.1	07.9	02.4	03.2	08.8	-02.6	19.6	06	-16.0	30	.	.	16	01.2	.	.	C4	01.2	.	.	09	01.1	.	.	07	01.1	54									
XII	-	-02.9	C1.8	-01.5	-01.0	03.0	-05.6	16.0	25	-19.0	01	.	.	19	01.4	.	.	C6	01.2	.	.	05	01.2	.	.	05	C1.0	58									
GDD.	-	06.8	14.5	08.2	09.4	15.4	04.1	35.4	48.VII	-15.0	4.XII	C7	C1.4	1C7	01.2	C1	C1.0	94	01.1	C7	03.4	120	01.1	01	02.0	50	C1.3	708									
φ = 42° 58' N λ = 18° 06' E Gr. ΔG = + 1h 17 min.																						LJUBINJE										BR. ST. 148					
I	-	0C.1	07.8	02.2	03.1	09.2	-01.2	14.0	25	-11.0	14	16	C3.4	.	.	.	.	C4	01.5	10	C1.8	C5	01.2	.	.	06	C1.5	52									
II	-	01.8	04.7	01.6	02.4	C5.3	0C.8	1C.0	06	-05.2	28	28	C2.2	.	.	.	.	.	.	47	01.4	.	.	.	.	04	01.2	05									
III	-	01.7	07.7	02.5	03.6	08.5	0C.7	17.5	31	-02.6	02	57	C1.6	C2	01.0	.	.	C5	01.8	10	01.8	.	.	.	01	C2.0	18										
IV	-	06.5	12.1	08.1	08.7	13.5	03.1	20.0	30	-03.6	23	22	C2.1	C2	C1.5	.	.	C2	02.5	35	C2.3	C1	01.0	.	.	07	C2.1	21									
V	-	14.2	21.1	14.5	16.1	23.1	1C.5	30.0	06	-03.0	11	14	C2.0	.	.	.	.	.	.	16	02.0	05	01.4	.	.	15	C1.7	43									
VI	-	17.9	23.0	18.1	19.3	25.0	15.3	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.									
VII	-	19.8	26.3	20.3	21.7	28.0	16.2	34.2	18	11.2	28	25	C1.5	C1	01.0	.	.	.	.	28	01.8	.	.	.	.	09	C1.9	30									
VIII	-	18.7	26.7	20.3	21.5	28.0	16.5	32.4	22	14.2	28	04	20	C1.6	.	.	.	.	.	23	01.3	.	.	.	.	08	C2.2	42									
IX	-	16.5	24.4	18.4	19.5	25.4	14.0	30.0	07	05.6	30	23	C1.5	.	.	.	.	.	.	22	01.5	.	.	.	.	12	C1.3	33									
X	-	08.8	18.4	13.7	13.4	19.5	07.5	25.2	03	-03.2	30	33	C1.4	C3	01.7	.	.	C4	02.0	18	01.3	06	C1.5	C5	01.0	.	.	21									
XI	-	03.4	11.6	07.4	07.4	13.4	01.9	19.2	04	-12.4	29	34	C1.1	C1	01.0	.	.	C2	01.5	18	01.3	08	01.1	03	01.7	02	C1.0	22									
XII	-	01.4	06.8	04.2	04.2	08.2	.	14.0	31	.	.	12	C1.6	C5	01.2	C4	C1.2	C1	01.0	36	01.6	08	01.0	05	01.2	06	01.0	16									
GDD.	-	09.2	15.9	10.9	11.8	17.3	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.									
φ = 42° 53' N λ = 18° 27' E Gr. ΔG = + 1h 14 min.																						BILEČA										BR. ST. 149					
I	-	C1.7	07.4	03.3	03.9	08.5	0C.1	12.7	04	-05.8	11	27	C2.0	C5	C1.0	27	C1.1	C5	01.8	C7	C1.7	04	01.2	07	01.3	07	C2.3	.									
II	-	01.6	07.2	03.1	03.8	08.2	-00.4	14.8	08	-08.4	27	26	C2.3	C9	C1.3	17	C1.5	13	C2.1	10	01.9	02	01.0	C2	01.0	04	C3.0	01									
III	-	01.5	09.5	04.1	04.8	1C.1	-00.3	16.0	27	-07.8	01	31	C2.0	11	01.0	17	C1.1	06	01.2	10	01.4	05	01.6	05	01.0	08	01.8	.									
IV	-	05.7	11.5	07.6	08.1	13.3	03.9	21.4	30	0C.4	16	18	C1.8	C4	01.2	19	C1.3	16	02.2	21	02.4	02	01.5	02	01.5	08	C2.8	.									
V	-	13.0	22.0	15.5	16.5	23.0	09.9	31.2	06	02.6	11	22	C2.1	11	C1.1	22	C1.1	08	01.1	23	01.9	.	.	.	04	03.0	02	02.5	01								
VI	-	16.6	24.0	18.9	19.6	25.4	13.3	31.0	29	08.4	17	25	C2.3	C8	01.0	18	C1.4	14	C1.6	17	C2.2	C2	01.5	C1	02.0	05	01.8	.									
VII	-	17.3	24.6	19.2	20.1	27.4	15.0	34.5	18	05.8	29	23	C1.4	C6	01.2	27	C1.2	C8	01.6	22	C2.0	01	02.0	C2	01.6	04	02.0	.									
VIII	-	16.8	26.3	20.1	20.8	28.1	15.0	33.8	22	11.6	05	15	C1.6	10	01.0	29	C1.0	C6	01.0	14	C1.4	03	01.0	C5	01.4	11	C2.3	.									
IX	-	15.1	24.8	18.3	19.2	26.2	13.2	30.8	05	05.0	15	13	14	C1.8	15	01.0	22	01.2	10	01.6	18	C1.5	C1	C1.0	C3	01.7	07	01.7	.								
X	-	09.8	18.6	12.5	13.3	19.4	07.8	25.6	02	01.4	24	21	C2.0	11	01.4	22	C1.0	12	01.2	17	C1.9	04	01.0	C2	01.0	06	C3.3	.									
XI	-	03.0	11.0	05.1	06.0	11.8	01.1	17.2	11	-12.8	30	27	C2.3	C7	01.1	19	C1.1	C5	01.8	12	C1.8	04	01.0	C3	01.0	06	02.2	03									
XII	-	01.5	06.2	03.2	03.5	07.6	-C1.2	12.6	24	-14.6	01	22	C1.5	C9	01.0	15	C1.5	14	02.1	12	C2.0	C4	01.0	C8	01.0	08	C2.6	01									
GDD.	-	08.6	16.1	10.9	11.6	17.5	06.5	34.5	48.VII	-14.6	4.XII	271	C2.0	110	01.1	252	C1.2	121	01.8	183	C1.9	32	01.2	44	01.4	76	C2.3	06									
φ = 42° 43' N λ = 18° 29' E Gr. ΔG = + 1h 14 min.																						LAŠTVA										BR. ST. 150					
I	-	C1.0	08.1	02.8	03.7	08.6	-0C.4	12.4	01	-07.2	15	.	.	C4	03.5	C6	C1.3	27	C1.2	.	.	C1	C1.0	C2	C1.5	03	C2.0	50									
II	-	C2.0	08.6	03.5	04.4	09.3	00.4	15.2	05	-08.4	27	.	.	16	01.6	C6	C2.0	15	01.6	.	.	C1	C2.0	.	.	1C											

Mesec	Oblačnost Nm (0-10)				Ineolacija broj sati	Vlažnost vazduha						Padavine R mm			Broj dana nasa:																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
	7	14	21	Sred. (Dias)		e _m mm	U m %					Σ	Max	Dat.	Tn 	Tx Λ	Tn Λ	Tx Λ	Tx Λ	Tn Λ	F (0-12)		R mm						●	*	•	Δ	◊	▲	T	≡	☒																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
							7	14	21	Sred.	Min											Λ	Λ	Λ	Λ	Λ	Λ	Λ										Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	

Mesec	Oblačnost hm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm			Broj dana n s a:																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
	7	14	21	Sred. (Dias)		e _m mm	U m t				Σ	Max	Dat.	Tn 	Tx Λ	Tn Λ	Tx Λ	Tx Λ	Tn Λ	F(0-12)		R mm						●	*	*	Δ	Δ	Δ	T	≡	☐																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
							7	14	21	Sred.										Min		Λ	Λ	Λ	Λ	Λ	Λ										Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	Λ	

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetra nD, Pm (0-12)																								
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C								
		7	14	21	Sred. (Dias)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.									
$\varphi = 43^{\circ} 25' N$ $\lambda = 20^{\circ} 17' E$ Gr. $\Delta G = +1h 21 min.$																																				
BELE VGDE-GLIJA																BR. ST. 196																				
I	-	-04.5	-01.4	-04.4	-03.6	00.2	-07.4	06.0	22	-16.0	11	03	01.0	01	01.0	01	01.0	13	01.9	02	01.0	06	01.3	02	01.0	06	01.5	62								
II	-	-04.3	-01.2	-04.3	-03.5	00.7	-07.6	09.5	09.08	-13.0	28.27	03	01.0	01	01.0	01	01.0	07	02.7	01	01.0	18	02.1	03	01.0	13	02.2	40								
III	-	-04.7	-01.2	-04.0	-03.4	00.1	-06.4	09.0	26	-12.0	01	01	01.0	06	01.3	05	01.2	15	02.1	01	01.0	02	01.5	02	03.0	23	01.5	40								
IV	-	00.9	05.4	01.5	02.3	06.8	-01.7	15.0	10	-06.0	15	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
V	-	09.1	13.3	08.3	09.7	15.3	03.8	27.0	06	-01.5	18	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VI	-	11.5	15.2	10.9	12.2	17.5	07.4	24.0	29	00.0	18	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VII	-	12.4	16.9	12.3	13.5	18.6	09.3	28.5	18	05.5	26	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VIII	-	12.1	16.6	11.2	12.8	17.9	06.6	22.0	21	05.0	31.12	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
IX	-	03.7	09.6	04.0	05.3	10.8	01.5	18.4	17	-06.1	26.25	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
X	-	-02.2	01.5	-02.0	-01.1	03.9	-04.6	11.2	05	-15.3	30	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
XI	-	-02.8	00.4	-03.1	-02.1	02.2	-06.2	10.0	30	-17.0	01	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
GDD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
$\varphi = 43^{\circ} 53' N$ $\lambda = 20^{\circ} 19' E$ Gr. $\Delta G = +1h 21 min.$																																				
ČAČAK																BR. ST. 197																				
I	-	-01.8	01.3	-00.7	-00.5	02.1	-02.5	08.2	31	-11.9	27	01	01.0	01	01.0	01	01.0	13	02.6	01	01.0	02	02.0	01	01.0	01	01.0	75								
II	-	00.5	06.4	01.7	02.6	07.1	-00.7	16.0	08	-06.6	13	01	01.0	01	01.0	01	01.0	04	02.2	01	01.0	06	01.8	07	02.1	03	02.7	64								
III	-	01.6	07.4	03.2	03.8	08.3	00.4	18.3	27	-04.0	14	01	02.0	01	03.0	01	03.0	07	02.1	01	01.0	08	02.0	07	02.0	01	01.0	68								
IV	-	06.0	14.1	08.9	09.5	15.5	04.0	27.0	10	-00.4	07	01	02.0	01	03.0	01	03.0	10	02.1	01	01.0	18	02.1	10	01.9	02	03.0	50								
V	-	14.1	22.2	14.5	16.3	23.4	10.3	33.5	06	02.5	18	01	02.0	03	02.3	02	02.0	04	02.0	01	01.0	15	01.9	01	01.0	01	03.0	66								
VI	-	16.8	25.1	16.8	18.8	26.0	13.2	33.0	29	06.3	17	01	02.0	02	02.0	01	01.0	01	01.0	01	01.0	09	02.2	09	01.4	02	02.5	66								
VII	-	15.4	26.5	18.6	20.8	27.8	15.5	41.0	18	12.2	31.28	01	02.0	04	02.5	03	02.0	05	01.4	02	02.0	04	02.5	14	01.6	04	02.2	57								
VIII	-	17.4	26.6	18.5	20.2	27.5	14.3	32.9	21	11.5	15	01	02.0	01	02.0	01	02.0	01	01.0	01	01.0	01	03.0	10	01.5	01	01.0	77								
IX	-	14.8	23.2	15.5	17.2	24.0	12.1	31.0	10	06.3	13	01	01.0	01	01.0	01	02.0	01	03.0	01	01.0	02	02.0	05	01.6	03	02.3	77								
X	-	07.2	16.0	08.8	10.2	16.5	04.8	25.0	17	-03.2	28.27	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	07	02.3	12	02.0	01	01.0	74								
XI	-	-00.3	07.2	01.0	02.5	06.4	-02.3	19.5	06	-13.1	29	01	02.0	01	01.0	01	01.0	01	01.0	01	01.0	06	02.3	11	01.7	01	01.0	71								
XII	-	-03.3	02.6	-01.3	-00.8	03.3	-05.0	12.7	26	-14.5	02	01	02.0	01	02.0	01	02.0	01	01.0	01	01.0	02	02.5	10	02.2	01	01.0	78								
GDD.	-	07.7	14.9	08.6	10.0	15.8	05.3	41.0	48.71	-14.5	2.111	05	01.8	12	02.3	13	01.9	45	02.2	03	02.0	80	02.1	95	01.8	17	02.3	825								
$\varphi = 43^{\circ} 08' N$ $\lambda = 20^{\circ} 31' E$ Gr. $\Delta G = +1h 21 min.$																																				
NOVI PAZAR																BR. ST. 198																				
I	-	-03.1	01.3	-01.2	-01.1	01.8	-04.3	16.4	08	-09.0	13	01	01.0	09	01.9	01	01.0	06	02.3	04	01.2	07	02.0	01	01.0	04	01.5	53								
II	-	-01.0	05.5	00.6	01.4	06.5	-02.2	16.4	08	-09.0	13	01	01.0	09	01.9	01	01.0	06	02.3	04	01.2	07	02.0	01	01.0	04	01.5	53								
III	-	00.3	06.5	01.8	02.6	07.2	-01.0	17.0	27	-05.5	01	02	01.0	15	01.5	01	01.0	01	02.0	01	01.0	01	02.0	01	01.0	07	01.7	67								
IV	-	04.6	12.7	06.9	07.8	14.2	01.9	24.0	10	-02.2	23	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
V	-	11.7	20.9	13.0	14.6	22.0	07.8	34.0	06	03.5	15	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VI	-	15.0	23.2	15.6	17.4	24.7	10.3	32.2	29	02.5	18	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VII	-	16.1	25.3	16.7	18.7	26.4	11.8	31.0	18	02.5	18	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
VIII	-	12.7	24.9	17.4	18.1	26.3	11.1	30.5	21	06.0	11	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
IX	-	11.6	23.0	14.2	15.8	24.1	05.6	25.6	25	02.5	13	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
X	-	05.1	16.9	07.1	09.0	17.5	02.7	28.0	18	-06.5	30	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
XI	-	-02.5	06.8	-00.3	00.9	07.7	-04.2	18.0	06	-20.5	29	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
XII	-	-05.4	01.5	-03.5	-02.7	02.5	-07.5	12.4	22	-19.6	01	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01	01.0	01								
GDD.	-	05.4	14.0	07.4	08.5	15.1	03.0	41.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
$\varphi = 43^{\circ} 44' N$ $\lambda = 20^{\circ} 41' E$ Gr. $\Delta G = +1h 23 min.$																																				
KRALJEVO																BR. ST. 199																				
I	748.6	-01.4	01.7	-00.2	00.0	02.6	-02.5	08.6	01	-11.2	27	01	01.0	01	01.0	01	01.0	06	02.7	01	01.0	01	01.0													

Mesec	Vazdušni pritisak Pm, mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetra nD, Pm (0-12)																	
		Tm																											
		7	14	21	Sred. (Djes.)	Max	Min	Max	Det.	Min	Det.	N		NE		E		SE		S		SW		W		NW		C	
		č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	
$\varphi = 43^{\circ} 56' N$ $\lambda = 21^{\circ} 23' E$ Gr. $\Delta G = +1h25$ min.												ČUPRIJA BR. ST.206																	
I	757.7	-01.9	01.4	-00.7	-00.5	02.0	-02.9	08.3	19	-14.7	27	02	02.5	.	.	22	03.5	17	02.9	03	02.0	01	02.0	06	02.3	10	02.4	32	
II	748.6	00.8	05.6	02.6	02.9	06.5	-00.7	16.3	08	-08.7	13	03	02.0	.	.	10	03.7	10	02.7	02	03.0	.	.	07	03.0	14	02.7	38	
III	753.9	02.2	07.8	04.1	04.5	08.6	00.9	19.4	24	-04.2	18	07	01.7	02	01.5	14	03.0	04	02.5	03	02.3	01	02.0	08	02.8	12	02.6	42	
IV	747.7	07.0	14.5	09.3	10.0	16.2	04.1	26.4	10	-01.2	01	02	02.0	.	.	07	03.4	09	06.0	03	02.0	01	02.0	06	02.0	18	02.0	44	
V	751.7	14.1	21.6	15.4	16.6	22.7	10.2	32.0	06	01.6	18	04	02.0	.	.	11	01.9	05	02.0	04	01.8	01	03.0	15	02.3	12	02.1	41	
VI	751.0	17.1	24.1	17.7	19.1	25.3	13.5	32.5	25	03.4	17	05	01.8	03	01.7	17	02.2	04	02.2	01	02.0	02	01.0	06	02.5	05	02.4	47	
VII	748.3	18.4	25.6	19.1	20.5	27.0	15.0	37.1	18	09.4	31	01	02.0	.	.	06	02.0	.	.	01	03.0	03	02.0	15	02.1	07	02.9	60	
VIII	752.7	15.9	26.4	17.6	19.4	27.3	12.4	31.6	21	07.2	11	06	02.5	01	02.0	04	02.8	03	02.0	02	01.0	04	01.2	04	02.5	08	02.4	61	
IX	752.4	13.4	23.6	15.5	17.0	24.6	11.1	31.6	09	03.8	13	01	02.0	01	03.0	14	02.7	06	01.8	03	01.3	.	.	07	01.9	05	02.4	53	
X	753.8	06.6	16.9	08.6	10.2	17.8	04.2	31.3	17	-06.3	27	.	.	01	02.0	07	02.7	08	02.1	02	02.0	01	03.0	05	02.8	10	02.4	59	
XI	755.5	00.6	07.6	02.4	03.3	09.1	-01.3	19.0	06	-09.8	29	.	.	.	.	04	02.5	04	02.8	10	01.9	03	01.7	09	02.4	16	02.2	44	
XII	753.8	-01.6	03.8	00.3	00.7	05.1	-03.4	16.2	23	-19.0	02	.	.	31	01.0	09	02.4	12	03.0	11	02.2	01	02.0	07	02.6	06	03.2	46	
600.	752.3	07.7	14.9	09.3	10.3	16.0	05.3	37.1	18	-19.0	2	31	02.0	09	01.8	125	02.8	82	02.6	45	02.0	18	01.8	95	02.4	123	02.4	567	
$\varphi = 43^{\circ} 14' N$ $\lambda = 21^{\circ} 36' E$ Gr. $\Delta G = +1h26$ min.												PROKUPLJE BR. ST.207																	
I	-	-01.9	02.0	-00.5	-00.2	02.6	-02.7	07.8	22	-11.6	15	.	.	08	01.9	.	.	01	02.0	.	.	06	02.5	04	02.8	03	02.0	71	
II	-	00.8	05.9	02.2	02.8	07.3	-00.6	16.9	08	-05.1	13	05	02.2	04	02.0	.	.	11	02.8	02	05.0	02	05.0	10	03.1	08	02.4	42	
III	-	01.2	07.0	03.4	03.7	08.1	00.2	16.5	27	-04.2	14	06	02.8	09	02.0	.	.	02	03.0	03	02.3	03	01.3	13	02.6	05	02.0	52	
IV	-	06.3	14.2	09.3	09.8	15.7	03.8	24.9	17	-00.5	23	04	02.2	02	03.0	01	03.0	12	03.2	03	05.0	09	03.0	07	02.7	06	02.7	46	
V	-	12.8	21.1	14.6	15.9	22.3	05.7	32.2	06	02.0	18	07	03.9	03	01.3	01	03.0	10	02.0	01	02.0	02	02.5	08	03.0	07	02.7	54	
VI	-	16.1	24.2	17.7	19.0	26.0	12.7	33.0	23	04.5	17	05	02.8	02	01.5	.	.	08	01.6	.	.	04	01.5	05	02.6	08	02.9	58	
VII	-	17.6	25.9	19.2	20.5	27.5	14.8	37.2	18	10.2	31	05	02.2	03	01.0	.	.	04	02.0	02	01.5	01	02.0	13	02.6	03	02.6	63	
VIII	-	15.6	25.6	16.1	19.3	26.9	12.9	31.6	21	08.5	12	03	03.0	07	02.1	.	.	03	01.7	.	.	01	02.0	01	04.0	11	02.8	67	
IX	-	13.2	23.6	15.9	17.1	24.5	11.5	31.0	25	04.6	15	01	02.0	03	02.3	.	.	02	03.0	.	.	.	.	03	02.0	09	02.1	72	
X	-	06.7	16.7	08.8	10.2	17.8	05.0	26.6	18	-05.0	30	11	03.1	02	02.0	.	.	07	02.1	01	04.0	08	04.0	03	03.3	03	03.3	58	
XI	-	-00.1	07.7	01.9	02.9	08.7	-01.0	16.4	06	-09.9	29	06	03.0	.	.	.	.	07	02.6	.	.	04	01.8	05	02.2	03	03.3	63	
XII	-	-01.9	03.7	00.1	00.5	05.0	-03.8	15.2	26	-17.6	01	03	02.7	.	.	02	03.5	08	03.4	02	07.0	06	02.5	01	04.0	04	03.2	67	
600.	-	07.2	14.8	09.3	10.2	16.1	05.2	37.2	18	-17.6	1	58	02.9	43	01.9	04	03.2	75	02.5	14	03.9	47	02.7	61	02.8	80	02.6	713	
$\varphi = 43^{\circ} 39' N$ $\lambda = 21^{\circ} 51' E$ Gr. $\Delta G = +1h26$ min.												SČKO BANJA BR. ST.208																	
I	-	-02.9	-00.2	-02.1	-01.8	01.0	-04.5	10.0	19	-15.2	27	01	01.0	07	03.7	34	03.6	.	.	.	.	09	02.3	08	02.9	.	.	34	
II	-	01.1	04.8	01.8	02.4	06.2	-00.8	16.2	09	-06.0	13	01	02.0	01	05.0	17	02.8	01	03.0	02	02.5	10	02.5	24	02.8	.	.	28	
III	-	01.5	05.8	03.2	03.4	06.8	00.0	17.9	24	-05.0	14	03	02.0	06	03.3	20	02.9	.	.	05	01.6	14	02.1	13	01.9	.	.	32	
IV	-	06.5	13.9	09.6	09.9	15.6	04.4	23.1	11	-00.5	23	01	03.0	02	04.0	08	03.0	.	.	03	05.0	08	02.6	24	01.9	01	06.0	43	
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	15.7	23.8	17.7	18.7	25.5	12.0	32.5	29	03.0	18	17	01	02.0	03	03.7	12	02.4	01	03.0	.	.	02	02.0	14	02.1	01	03.0	56
VII	-	18.1	25.6	19.2	20.5	27.1	14.5	36.0	18	09.5	31	01	01.0	.	.	03	02.0	.	.	02	02.5	10	02.5	19	01.9	.	.	58	
VIII	-	15.7	25.5	17.9	19.2	26.7	12.8	32.0	23	07.5	12	02	02.5	07	03.6	18	02.8	.	.	.	.	03	02.0	13	02.1	.	.	50	
IX	-	13.3	22.0	16.2	16.9	23.3	11.8	30.0	09	07	06.0	17	01	03.0	04	02.8	17	02.4	.	.	03	04.0	.	.	08	02.0	.	.	59
X	-	07.1	15.6	10.5	10.9	16.7	05.1	27.0	18	17	-04.5	30	.	.	02	02.5	26	04.2	02	08.0	01	03.0	04	05.0	08	02.0	.	.	50
XI	-	00.8	06.7	02.6	03.2	08.1	-01.5	16.9	25	06	-11.1	29	02	03.5	.	.	06	03.3	.	.	02	06.0	10	04.2	12	02.1	.	.	58
XII	-	00.2	04.5	01.5	01.9	06.2	-02.4	13.9	23	-13.5	01	.	.	01	01.0	16	02.8	.	.	10	05.4	06	02.7	09	01.8	.	.	51	
600.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 43^{\circ} 20' N$ $\lambda = 21^{\circ} 54' E$ Gr. $\Delta G = +1h26$ min.												NIS BR. ST.209																	
I	750.3	-01.1	02.1	00.0	00.3	02.7	-01.5	08.9	01	-09.9	15	04	02.2	03	03.7	24	03.0	12	01.7	.	.	01	01.0	01	01.0	32	02.0	16	
II	741.7	01.5	05.9	02.9	03.0	07.3	00.0	17.9	08	-03.8	13	05	02.6	.	.	15	01.5	07	01.3	02	02.0	02	01.0	05	02.2	26	02.7	22	
III	746.7	01.8	08.9	04.2	04.3	08.1	00.7	18.8	27	-03.4	21	04	01.2	03	03.7	23	02.3	04	01.0	03	01.0	05	01.6	05	01.2	27	01.6	19	
IV	741.1	07.4	14.5	09.8	10.4	16.1	04.5	25.6	10	00.8	01	05	01.2	01	01.0	08	01.5	09	01.4	12	02.5	.	.	05	01.0	24	02.4	26	
V	745.0	14.2	21.6	15.6	16.7	22.9	10.9	33.8	06	04.3	18	01	03.0	.	.	05	01.8	09	01.2	05	01.8	03	01.3	07	01.1	28	02.3	35	
VI	744.3	17.4	24.4	18.5	19.7	26.1	13.7	33.3	23	04.9	17	05	01																

[illegible]

1973

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																							
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C							
		7	14	21	Sted. (Dias)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.								
$\varphi = 42^{\circ} 01' N$ $\lambda = 20^{\circ} 53' E$ Gr. $\Delta G = +1h 24 min.$																																			
POPOVA ŠAPKA															BR. ST. 251																				
I	-	-04.7	-02.2	-04.1	-03.8	-06.1	-06.4	05.4	22	-14.5	12	.	.	01	02.0	.	.	07	02.0	06	02.0	01	02.0	.	.	22	02.6	56							
II	-	-05.0	-02.2	-04.3	-04.0	-06.3	-06.8	08.2	08	-16.8	27	01	03.0	.	.	.	.	03	01.7	03	03.0	09	03.2	01	01.0	34	03.1	33							
III	-	-05.8	-03.1	-04.6	-04.6	-01.5	-07.5	07.5	26	-14.4	01	02	04.5	.	.	.	.	08	01.6	05	02.4	07	02.7	01	04.0	37	02.4	33							
IV	-	-00.1	02.2	00.5	00.8	03.9	-02.4	05.6	10	-07.3	16	01	01.0	01	01.0	.	.	03	01.3	02	03.0	16	02.9	06	03.2	24	03.1	37							
V	-	05.1	11.5	09.1	09.7	13.1	05.8	22.3	06	-01.3	11	02	02.5	03	02.0	.	.	11	01.3	.	.	.	.	08	03.0	42	02.4	27							
VI	-	10.5	12.6	10.4	11.0	14.2	07.0	20.8	29	00.0	17	01	04.0	02	02.0	.	.	19	01.2	03	02.0	06	02.7	01	02.0	31	02.2	27							
VII	-	13.0	15.0	12.6	13.3	16.5	09.8	26.6	18	04.0	27	01	01.0	02	01.5	02	03.0	17	01.5	.	.	17	02.9	06	03.7	19	01.8	29							
VIII	-	11.7	13.2	11.1	11.8	14.6	08.5	18.0	25	05.0	16	04	02.0	01	01.0	01	02.0	19	02.3	02	01.5	14	01.7	04	01.8	22	02.1	26							
IX	-	10.8	12.8	10.4	11.1	14.0	07.7	20.3	24	01.9	12	.	.	02	01.5	01	02.0	17	01.8	02	03.5	04	02.8	02	03.0	09	02.0	53							
X	-	05.3	07.4	05.2	05.8	09.0	02.5	18.5	18	-07.2	24	.	.	01	01.0	.	.	12	01.8	03	01.7	09	02.6	13	05.4	12	03.3	43							
XI	-	03.6	09.5	05.1	05.8	10.7	01.5	10.0	12	-16.5	29	.	.	02	02.0	.	.	06	01.3	01	04.0	06	02.8	06	03.2	31	02.9	38							
XII	-	-02.4	-00.5	-01.9	-01.7	02.3	-05.6	08.2	25	-16.1	01	.	.	03	02.0	01	01.0	02	01.0	02	03.0	10	04.0	09	04.9	22	03.0	44							
GOO.	-	03.8	06.4	04.1	04.6	08.0	01.2	26.6	18 VII	-18.1	4 XII	12	02.6	18	01.8	05	02.2	124	01.6	29	02.4	99	02.8	57	03.8	305	02.6	446							
$\varphi = 42^{\circ} 00' N$ $\lambda = 20^{\circ} 58' E$ Gr. $\Delta G = +1h 24 min.$																																			
TETOVO															BR. ST. 252																				
I	-	-01.8	01.3	-00.7	-00.5	02.5	-02.3	07.2	21	-11.0	15	03	01.0	04	01.2	.	.	02	01.0	08	01.0	06	01.0	.	.	01	04.0	70							
II	-	-00.2	05.3	01.9	02.2	06.9	-01.1	14.2	08	-12.5	27	05	02.4	06	01.3	.	.	03	01.0	02	01.0	01	02.0	01	01.0	01	01.0	65							
III	-	00.9	06.9	04.0	04.0	07.7	00.3	16.5	27	-03.4	21	11	01.8	03	01.0	01	01.0	04	01.8	03	01.3	01	01.0	.	.	01	01.0	69							
IV	-	07.1	13.5	09.6	09.9	15.2	04.1	24.0	10	-00.8	23	10	02.1	05	01.2	01	01.0	05	01.6	03	03.0	03	02.7	01	01.0	02	01.5	60							
V	-	13.7	21.3	15.8	16.6	22.5	10.0	30.5	23	04.0	12	06	01.3	04	01.2	02	01.0	01	01.0	02	01.0	.	.	.	.	02	03.0	76							
VI	-	16.7	24.3	18.7	19.6	25.5	12.4	32.0	29	04.6	18	08	01.1	06	01.3	02	01.5	02	01.0	02	02.0	04	02.2	.	.	01	01.0	65							
VII	-	17.8	26.1	20.0	21.0	27.6	14.0	35.0	23 VII	07.6	28	02	01.0	08	01.8	.	.	.	.	01	01.0	02	01.5	.	.	02	01.5	78							
VIII	-	15.9	23.4	18.4	19.6	26.4	12.1	30.2	22	08.2	12	05	01.8	03	02.0	.	.	.	.	02	01.5	.	.	01	01.0	01	01.0	81							
IX	-	13.2	23.1	15.9	17.0	24.0	11.2	29.0	09	05.2	15	03	01.0	.	.	.	.	.	.	01	01.0	01	02.0	01	01.0	01	02.0	83							
X	-	07.2	17.3	10.0	11.1	18.2	05.6	28.5	18	-04.0	30	04	01.8	02	01.0	.	.	04	01.2	06	03.3	04	02.0	.	.	01	03.0	72							
XI	-	-00.7	06.6	01.8	02.4	08.0	-01.7	17.5	25	-10.0	29	05	01.2	01	03.0	01	02.0	06	01.7	01	02.0	03	01.7	01	01.0	02	01.0	70							
XII	-	-03.8	00.2	-02.5	-02.2	01.6	-05.4	12.2	27	-18.0	01	06	02.0	01	07.0	01	01.0	01	02.0	05	01.0	.	.	.	.	02	02.0	76							
GOO.	-	07.2	14.3	09.4	10.1	15.5	04.9	35.0	18 VII	-18.0	4 XII	68	01.6	43	01.5	08	01.2	27	01.4	33	01.8	30	01.6	05	01.0	16	01.9	865							
$\varphi = 42^{\circ} 08' N$ $\lambda = 21^{\circ} 43' E$ Gr. $\Delta G = +1h 27 min.$																																			
KUMANOVCI															BR. ST. 253																				
I	-	-00.6	02.7	00.5	00.8	04.3	-01.3	11.8	22	-12.4	15	11	03.5	04	02.5	.	.	02	02.5	01	01.0	01	01.0	01	01.0	35	02.2	15							
II	-	00.7	04.7	02.1	02.7	08.3	-01.0	15.0	08	-12.2	27	12	02.6	05	02.0	.	.	04	01.8	09	02.9	07	02.0	03	02.0	38	02.1	06							
III	-	01.5	06.9	03.5	03.8	07.8	00.1	18.2	27	-04.3	07	12	02.8	.	.	.	.	14	01.2	05	01.6	08	01.8	.	.	54	01.7	.							
IV	-	07.2	15.0	09.7	10.4	16.0	05.0	22.6	10	00.1	23	07	02.6	02	01.0	.	.	08	01.4	13	02.3	18	01.5	02	01.0	40	02.0	.							
V	-	13.8	22.2	15.8	16.9	24.5	11.1	31.2	24	05.4	11	20	02.0	04	02.8	.	.	11	01.3	13	01.3	14	01.4	03	01.0	28	01.8	.							
VI	-	16.8	25.5	19.3	20.2	26.9	13.4	33.0	23	05.5	18	14	01.9	02	03.0	01	02.0	03	01.0	05	01.6	20	01.4	02	01.0	40	01.8	03							
VII	-	18.8	27.0	21.1	22.0	28.4	15.8	35.7	18	10.2	28	16	02.5	02	01.0	02	01.0	.	.	03	01.7	03	01.7	04	01.5	54	01.7	09							
VIII	-	17.4	27.0	20.3	21.3	27.7	14.7	31.3	22	09.0	17	13	02.4	.	.	02	01.0	07	01.4	05	02.2	01	01.0	03	01.0	60	01.6	02							
IX	-	14.4	24.1	16.9	18.1	25.1	12.7	30.0	05	04.4	16	16	02.2	.	.	01	01.0	09	01.4	10	01.4	08	02.1	01	01.0	42	01.4	03							
X	-	07.8	18.0	11.0	11.9	18.7	06.2	29.0	18	-02.4	30	09	03.2	.	.	02	01.5	05	01.4	11	01.2	05	02.4	06	01.0	53	01.7	02							
XI	-	00.6	07.3	02.5	03.2	08.5	-01.0	16.6	17	-07.0	29	38	03.2	01	06.0	07	01.4	05	01.0	04	01.8	08	01.8	03	01.0	16	02.1	08							
XII	-	-02.2	02.4	00.8	-00.3	03.7	-03.9	12.2	27	-13.2	07	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.							
GOO.	-	08.0	15.4	10.2	10.9	16.7	06.0	35.7	18 VII	-13.2	7 XII	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.								
$\varphi = 42^{\circ} 05' N$ $\lambda = 22^{\circ} 09' E$ Gr. $\Delta G = +1h 29 min.$																																			
KRATOVO															BR. ST. 254																				
I	-	-01.3	01.4	-00.3	-00.1	02.6	-02.4	07.8	20	-09.4	15	08	01.8	04	02.2	04	01.0	14	01.9	10	02.2	11	01.9	06	01.8	07	02.1	29							
II	-	00.7	04.7	02.7	02.7	06.6	-01.2	14.3	08	-10.8	28	05	02.2	03	01.7	06	01.8	20	02.4	09	01.0	07	02.1	04	01.5	07	02.4	23							

Mesec	Oblačnost Rm (0-10)				Inzolacija broj sati	Vlažnost vazduha				Padavine R mm			Broj dana nase:																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
	7	14	21	Sred. (Dien)		e _m mm	U m %			Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)		R mm						●	★	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱	✱

1973

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																							
		Tm				Max	Min	Max	Det.	Min	Det.	N		NE		E		SE		S		SW		W		NW		C							
		7	14	21	Sred. (01es)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.								
$\varphi = 41^{\circ} 31' N$ $\lambda = 20^{\circ} 32' E$ Gr. $\Delta G = +1h 22 min.$																																			
DEBAR															BR. ST. 256																				
I	-	-01.2	01.6	-00.2	00.0	02.6	-02.5	06.0	19	-10.0	15	06	02.0	.	.	06	07.8	.	.	26	01.5	.	.	36	01.1	.	.	19							
II	-	-00.4	04.6	01.9	02.0	05.7	-01.5	14.0	08	-15.0	28	04	02.2	.	.	07	03.6	.	.	45	01.9	.	.	24	01.3	.	.	04							
III	-	-00.4	05.7	02.6	02.6	06.7	-01.5	14.0	27	23	02	03	01.3	.	.	08	04.2	.	.	52	01.8	01	01.0	13	01.5	02	03.0	14							
IV	-	05.7	11.2	07.9	08.2	13.0	02.6	23.5	10	-02.0	23	05	01.8	.	.	05	04.6	.	.	53	02.1	.	.	21	01.6	.	.	06							
V	-	11.5	21.9	15.2	16.0	23.6	07.9	32.0	06	03.0	12	08	02.1	.	.	.	.	.	.	38	01.4	.	.	19	01.3	.	.	28							
VI	-	14.9	23.4	18.4	18.8	24.6	11.0	32.0	08	05.0	18	03	01.3	.	.	01	01.0	.	.	32	01.8	.	.	35	01.6	.	.	19							
VII	-	17.5	25.7	20.8	21.2	27.3	14.3	38.0	18	08.0	29	01	02.0	.	.	.	.	.	.	47	01.4	.	.	21	01.5	.	.	24							
VIII	-	15.2	25.0	20.1	20.1	26.0	12.5	30.5	23	10.0	12	11	.	.	.	.	.	.	.	38	01.7	.	.	38	01.8	.	.	17							
IX	-	14.1	23.0	16.5	17.5	24.4	11.0	30.0	24	06.0	15	02	02.0	.	.	04	03.0	.	.	35	01.9	.	.	35	01.8	.	.	14							
X	-	07.9	16.7	10.0	11.1	17.9	05.1	26.0	18	17	30	02	01.0	.	.	11	04.5	.	.	29	01.8	.	.	19	01.5	.	.	32							
XI	-	00.2	06.5	02.1	02.7	08.2	-01.8	17.0	07	-13.0	29	02	03.0	.	.	.	.	.	.	23	01.3	.	.	37	01.6	.	.	28							
XII	-	-01.7	01.3	-01.9	-01.0	02.4	-04.7	13.0	27	-19.0	01	05	01.2	.	.	.	.	.	.	35	01.5	.	.	39	01.4	.	.	14							
GOD.	-	06.9	13.9	09.4	09.9	15.2	04.4	38.0	18	VI	41	01.8	.	.	.	42	04.6	.	.	453	01.7	01	01.0	337	01.5	02	03.0	219							
$\varphi = 41^{\circ} 11' N$ $\lambda = 20^{\circ} 41' E$ Gr. $\Delta G = +1h 23 min.$																																			
STRUHA															BR. ST. 257																				
I	-	-00.9	03.3	00.2	00.7	03.8	-01.7	08.6	19	-08.7	15	13	01.9	06	03.2	.	.	02	02.0	03	01.3	.	.	06	01.0	53	01.9	10							
II	-	-00.3	04.9	01.8	02.0	06.3	-01.0	12.6	10	-10.4	28	10	02.0	01	02.0	.	.	03	03.0	14	02.3	01	02.0	06	01.5	45	01.7	04							
III	-	00.3	05.8	02.4	02.8	08.8	-00.6	14.3	27	-09.1	02	13	01.8	05	02.4	01	02.0	04	03.0	15	01.9	.	.	04	01.2	37	01.7	16							
IV	-	05.5	10.9	07.9	08.0	12.7	03.3	20.0	09	00.0	23	10	02.5	04	01.0	01	01.0	05	02.2	23	02.3	07	02.6	08	01.6	23	01.8	09							
V	-	13.5	20.1	15.0	15.9	22.0	06.7	28.3	24	03.5	12	13	01.8	04	02.8	02	01.5	.	.	26	02.0	03	02.3	01	01.0	28	01.6	16							
VI	-	15.9	22.5	17.4	18.3	24.2	11.2	30.3	23	05.5	18	18	02.0	02	02.0	.	.	01	01.0	20	02.0	04	02.8	06	01.7	17	01.4	22							
VII	-	18.1	25.2	19.5	20.6	27.0	13.4	36.5	18	07.4	28	09	01.7	02	01.0	.	.	03	02.3	22	02.0	04	03.8	07	01.7	24	01.5	22							
VIII	-	16.8	24.9	18.6	19.7	26.1	12.8	29.3	08	10.0	18	25	02.0	01	02.0	02	01.5	.	.	21	02.1	01	02.0	02	02.0	33	01.3	08							
IX	-	13.9	22.2	15.9	17.0	23.5	11.6	27.6	10	07.7	15	22	02.4	.	.	.	.	.	.	20	02.2	02	03.5	03	01.0	33	01.5	10							
X	-	08.5	17.2	10.7	11.8	18.0	06.6	26.5	18	-03.5	30	26	02.2	09	02.8	.	.	02	02.5	14	02.3	09	02.7	04	02.8	25	01.4	04							
XI	-	01.5	09.0	03.6	04.4	10.0	-00.5	15.5	07	-07.0	29	16	02.3	01	03.0	01	03.0	01	02.0	14	02.1	10	03.1	03	02.3	36	01.8	08							
XII	-	00.0	05.0	01.7	02.1	06.0	-01.8	12.0	27	26	01	10	02.1	01	02.0	.	.	.	.	15	02.4	03	03.3	04	02.0	35	01.6	25							
GOD.	-	07.7	14.2	09.6	10.3	15.5	05.2	36.5	18	VI	185	02.1	36	02.4	07	01.7	19	02.4	207	02.2	44	02.9	54	01.6	389	01.6	154								
$\varphi = 41^{\circ} 32' N$ $\lambda = 20^{\circ} 42' E$ Gr. $\Delta G = +1h 23 min.$																																			
LAZARPOLE															BR. ST. 258																				
I	-	-03.7	-00.4	-03.5	-02.7	00.8	-05.4	05.1	19	-12.8	13	07	01.4	02	02.0	14	01.6	10	02.2	02	02.0	.	.	05	02.2	04	01.5	49							
II	-	-03.4	00.7	-02.3	-01.8	02.0	-04.8	09.6	08	-16.8	28	04	01.8	02	01.5	18	01.8	07	02.1	.	.	03	01.3	13	02.2	13	01.8	24							
III	650.0	-04.2	00.9	-02.2	-01.9	02.5	-05.4	09.7	27	23	01	03	01.7	07	01.4	18	01.7	04	02.2	.	.	.	.	11	01.5	03	02.3	47							
IV	647.9	02.0	05.9	02.6	03.3	07.6	-00.4	16.5	09	-05.1	17	.	.	05	01.6	10	01.9	04	01.5	03	02.7	01	04.0	20	02.2	03	02.0	44							
V	653.6	10.6	16.6	10.1	11.8	17.8	06.3	26.9	06	06.8	15	02	02.0	11	01.4	09	01.6	02	02.0	02	02.0	02	02.0	23	02.1	06	02.0	36							
VI	652.6	12.6	18.2	12.0	13.7	19.2	08.1	25.1	23	02.6	18	04	02.0	04	01.5	07	01.6	.	.	03	01.7	04	02.5	26	02.1	08	02.4	34							
VII	651.7	14.4	19.9	14.2	15.7	21.7	10.2	31.4	18	04.0	28	02	01.5	13	01.3	07	01.1	03	01.3	01	01.0	08	02.2	25	02.1	07	01.9	27							
VIII	654.7	12.3	20.1	12.7	14.4	21.1	05.1	25.2	22	05.8	16	01	01.0	23	01.0	06	01.5	02	01.0	.	.	02	02.0	12	01.9	05	01.6	42							
IX	654.2	10.6	17.8	11.7	12.9	19.6	06.7	25.7	24	03.2	14	04	01.6	26	01.5	19	01.7	02	01.5	.	.	05	02.0	12	02.0	06	02.2	16							
X	653.1	05.8	12.2	06.6	07.8	13.2	03.7	20.4	18	-03.7	24	02	01.5	30	01.1	14	01.9	04	01.5	.	.	07	03.1	07	01.6	07	01.7	12							
XI	652.5	-00.3	04.6	00.4	01.2	05.8	-02.4	12.7	11	-15.5	29	02	01.5	21	01.3	01	02.0	01	01.0	02	03.0	15	02.3	19	02.2	04	01.8	25							
XII	650.8	-01.3	01.9	-00.6	-00.2	03.1	-03.7	08.2	25	-17.7	01	03	01.3	07	01.4	03	01.3	13	01.5	04	02.8	04	02.2	11	01.9	09	01.8	39							
GOD.	-	04.6	09.9	05.1	06.2	11.2	02.0	31.4	18	VI	34	01.6	151	01.3	126	01.7	52	01.8	17	02.3	61	02.4	184	02.0	75	01.9	395								
$\varphi = 41^{\circ} 42' N$ $\lambda = 20^{\circ} 45' E$ Gr. $\Delta G = +1h 23 min.$																																			
MAVRČI ANOVI															BR. ST. 259																				
I	-	-03.4	-00.3	-02.8	-02.3	00.8	-04.8	06.0	22	-11.4	14	.	.	33	02.4	.	.	.	.	.	.	.	16	02.8	.	.	.	44							
II	-	-03.1	01.4	-01.8	-01.3	02.2	-04.2	11.4	08	-15.0	28	.	.	25	02.5	.	.	.	.	.	.	.	22	02.8	.	.	.	37							
III	-	-03.9	01.3	-01.7	-01.5	01.9	-05.1	10.0	27	-11.4	21	.	.	17	02.6	.	.	.	.	.															

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm				Broj dana n s a:																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								
	7	14	21	Sred. (Dias)		mm	U m t			Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F (0-12)		R mm						●	*	*	Δ	Δ	Δ	Δ	R	T	≡	☐																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
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Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																							
		7m				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C							
		7	14	21	Sred. (Dien)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.								
GOSTIVAR																																			
φ = 41° 48' N λ = 20° 55' E Gr. ΔG = + 1h 24 min.															BR. ST. 261																				
I	-	-02.4	06.9	-01.7	-01.2	02.3	-	06.2	23.21	-	-	27	06	02.0	10	02.0	-	-	02	03.0	06	04.8	05	03.4	-	-	09	02.3	46						
II	-	-00.3	04.9	01.6	02.0	06.3	-03.4	14.6	10	-16.0	-	27	06	02.0	10	02.0	-	-	02	03.0	06	04.8	05	03.4	-	-	09	02.3	46						
III	-	00.5	06.5	02.5	03.0	07.7	-02.4	16.0	27	-10.2	01	07	02.1	16	02.4	-	-	01	03.0	-	07	02.9	-	-	-	-	13	02.4	49						
IV	-	07.5	13.1	08.0	09.2	14.6	03.0	23.4	10	00.0	22	06	05	02.0	10	02.6	-	-	-	04	04.2	28	04.8	-	-	-	20	02.6	23						
V	-	14.6	21.1	13.8	15.8	22.4	07.3	29.6	24	05.0	11	03	02.7	05	03.8	-	-	01	03.0	-	-	15	02.9	-	-	41	02.6	28							
VI	-	17.4	23.6	17.2	18.8	24.7	10.1	31.4	29	05.0	17	04	02.0	14	02.8	-	-	-	01	03.0	15	03.2	-	-	-	30	02.4	26							
VII	-	18.2	25.1	18.6	20.2	26.8	12.5	35.0	18	08.0	31	28	01	02.0	08	02.1	-	-	-	-	13	02.8	-	-	-	32	02.2	39							
VIII	-	16.6	24.5	18.1	19.3	25.6	10.9	28.6	23	08.0	01	-	-	13	02.2	-	-	-	-	01	02.0	-	-	-	-	33	02.2	46							
IX	-	14.3	21.9	15.6	16.9	22.9	08.9	27.2	24	09	04.6	16	-	-	13	02.2	-	-	-	-	01	02.0	-	-	-	35	02.3	41							
X	-	07.9	16.3	09.0	10.5	17.2	03.8	28.0	18	-04.2	30	15	02.4	07	02.6	-	-	-	-	-	16	04.5	-	-	-	17	02.5	38							
XI	-	-00.1	06.7	01.7	02.5	07.9	-03.2	18.6	16	-12.4	30	20	02.2	08	02.0	-	-	-	-	-	10	05.5	-	-	-	15	02.1	37							
XII	-	-05.5	00.1	-03.7	-03.2	01.8	-08.7	10.6	27	-16.0	07	03	04.0	08	02.0	-	-	-	-	01	03.0	03	03.0	-	-	-	10	03.3	68						
GOD.	-	07.4	13.7	08.4	09.5	15.0	-	35.0	48.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
φ = 41° 31' N λ = 20° 58' E Gr. ΔG = + 1h 24 min.															KICEVO																				
															BR. ST. 262																				
I	-	-02.3	01.4	-00.9	-00.7	01.9	-03.8	06.0	21	-14.2	15	28	02.1	14	02.9	10	02.0	01	02.0	08	01.9	01	02.0	12	01.7	04	02.0	15							
II	-	-00.3	05.3	02.4	02.4	06.1	-01.6	15.0	10	-13.8	27	35	02.4	06	03.2	09	01.6	01	02.0	15	02.4	06	02.5	11	02.2	-	-	01							
III	-	-00.4	06.7	03.4	03.3	07.7	-01.2	16.0	27	-09.4	03	02	16	02.4	15	02.5	23	02.2	02	01.5	28	01.8	02	02.5	02	02.0	02	01.5	03						
IV	-	04.6	12.9	08.7	08.7	14.6	03.3	23.5	10	-01.2	23	23	02.7	04	02.5	06	02.3	02	02.5	39	02.5	01	01.0	10	02.2	02	01.5	03							
V	-	11.0	23.5	15.8	16.5	24.6	08.9	32.8	06	03.5	12	33	02.7	09	02.7	10	01.9	02	01.5	13	01.9	05	01.8	15	01.9	03	02.3	03							
VI	-	13.4	26.0	18.4	19.1	27.1	11.5	33.2	23	05.5	19	28	24	02.6	08	02.5	15	01.9	-	-	12	03.0	05	02.6	13	02.2	03	02.3	10						
VII	-	14.9	26.5	19.7	20.2	27.8	13.3	37.5	18	07.2	28	20	02.2	15	02.7	06	02.2	-	-	17	02.9	09	02.0	18	01.6	03	01.7	05							
VIII	-	13.5	26.0	18.6	19.2	26.8	12.3	31.6	23	08.4	12	16	02.4	13	03.1	09	01.6	01	01.0	07	01.7	12	02.0	25	01.6	01	04.0	09							
IX	-	12.1	23.9	16.3	17.1	24.5	11.3	29.8	23	06.0	15	20	02.0	08	02.1	13	01.8	01	01.0	07	01.9	04	01.0	21	01.6	06	01.5	10							
X	-	07.2	17.8	10.2	11.4	18.5	06.0	29.0	18	-04.5	30	23	02.4	16	02.6	07	02.0	04	02.5	19	02.0	06	02.3	12	01.8	03	02.0	03							
XI	-	00.4	09.0	03.7	04.2	10.2	-00.9	18.2	07	-08.2	29	34	02.4	12	02.0	04	02.8	03	01.7	18	02.9	06	02.0	06	01.5	02	01.5	05							
XII	-	-01.8	02.5	00.2	00.3	03.9	-03.5	14.0	27	-20.0	01	25	01.8	20	02.0	09	01.2	03	01.7	13	01.9	05	01.6	07	01.9	-	-	11							
GOD.	-	06.0	15.1	09.7	10.1	16.1	04.6	37.5	48.VII	-20.0	4.XII	297	02.4	140	02.5	121	01.9	20	01.9	196	02.3	62	02.0	152	01.8	29	01.9	78							
φ = 41° 05' N λ = 21° 01' E Gr. ΔG = + 1h 24 min.															RESEN																				
															BR. ST. 263																				
I	-	-02.3	01.5	-00.9	-00.6	02.3	-04.1	08.6	19	-15.5	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	-	-00.8	04.0	01.2	01.4	05.3	-02.6	12.9	08	-14.7	28	17	01.2	12	02.2	12	02.5	04	01.5	10	02.9	08	01.9	08	02.2	01	01.0	12							
III	-	-00.5	03.9	00.5	01.1	04.9	-02.2	12.0	27	-10.0	02	01	10	01.0	13	01.5	23	02.3	05	02.4	11	02.2	06	01.7	05	01.8	01	03.0	19						
IV	-	04.4	10.2	06.5	06.9	11.6	02.2	19.2	09	-01.8	23	12	01.2	08	01.9	06	02.0	02	01.0	14	02.8	04	02.0	11	02.7	04	02.0	29							
V	-	12.8	20.9	13.0	14.9	22.3	07.5	29.3	23	06	01.3	12	14	01.3	06	02.3	09	02.3	03	01.7	09	01.8	11	02.4	05	02.4	03	01.0	33						
VI	-	15.4	21.7	15.0	16.8	23.4	05.5	29.8	08	03.2	18	15	01.4	09	01.9	06	01.8	07	01.1	08	02.5	06	02.0	08	02.4	04	02.8	27							
VII	-	16.7	24.7	17.1	18.9	26.0	11.3	35.0	18	05.5	30	29	12	01.4	08	01.8	10	01.5	06	01.2	03	01.7	11	02.2	04	02.0	09	01.6	30						
VIII	-	15.4	23.7	16.1	17.8	24.6	10.9	29.3	26	08.0	12	13	01.4	15	01.5	16	01.8	03	01.3	03	01.3	05	01.4	-	-	01	01.0	37							
IX	-	12.5	21.4	13.5	15.2	22.2	10.2	28.1	24	06.4	23	22	15	01.3	08	01.6	12	01.8	01	03.0	10	01.7	02	02.0	01	02.0	01	01.0	40						
X	-	07.4	15.5	08.6	10.0	16.8	04.7	25.2	21	-07.2	29	06	01.3	13	03.1	18	02.2	02	01.5	14	01.6	08	02.4	02	02.0	03	01.3	27							
XI	-	01.5	08.8	02.6	03.9	10.5	-01.2	16.3	14	-08.2	02	18	01.5	11	01.8	09	04.1	05	02.6	05	01.2	16	02.5	06	02.3	06	02.2	14							
XII	-	00.4	05.0	01.6	02.1	06.3	-03.0	11.9	27	-20.5	01	13	01.5	08	01.9	11	02.1	05	01.6	09	01.6	25	02.2	02	01.5	04	01.5	16							
GOD.	-	06.9	13.4	07.5	09.0	14.7	03.6	35.0	48.VII	-20.5	4.XII	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
φ = 41° 31' N λ = 21° 13' E Gr. ΔG = + 1h 25 min.															MAKEDONSKI BROD																				
															BR. ST. 264																				
I	-	-02.6	03.1	-00.8	-00.3	03.3	-04.3	06.4	19	-15.0	14	04	02.0	-	-	02	03.0	-	-	11	01.9	-	-	-	-	-	-	76							
II	-	-01.2	06.2	00.6	01.6	06.4	-03.0	14.0	08	-16.6	27	03	02.0	-	-	02	02.0	-	-	04	02.5</														

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																							
		Tm				Max	Min	Max	Det.	Min	Det.	N		NE		E		SE		S		SW		W		NW		C							
		7	14	21	Sred. (Dias)							Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.								
$\varphi = 41^{\circ} 03' N$ $\lambda = 21^{\circ} 22' E$ Gr. $\Delta G = +1h 25 min.$																																			
BITOLA															BR. ST. 266																				
I	714.6	-02.4	06.6	-01.9	-01.4	01.6	-04.0	04.6	23	-14.1	15	30	01.5	15	01.6	02	02.0	.	.	10	03.0	01	03.0	06	01.3	03	01.3	26							
II	706.9	-00.4	04.9	02.4	02.3	04.3	-01.3	15.0	10	-11.0	28	19	02.1	14	01.9	04	01.2	03	01.7	13	04.1	02	03.5	06	02.2	08	03.1	15							
III	711.4	00.4	05.7	02.9	03.0	04.7	-00.5	14.1	27	-07.0	02	18	01.9	20	02.0	06	01.7	01	04.0	15	03.7	02	01.5	01	03.0	03	01.7	27							
IV	707.4	07.2	13.1	09.4	09.8	14.8	04.5	22.6	09	-00.4	23	16	02.4	12	03.1	03	02.7	05	02.8	17	03.5	06	03.0	04	03.0	13	04.7	14							
V	711.7	13.7	22.5	16.3	17.2	24.0	09.4	32.0	23	03.0	12	13	02.3	20	02.0	05	02.2	03	02.3	10	02.3	05	01.4	06	03.5	15	03.1	16							
VI	711.4	16.7	24.8	18.9	19.8	26.3	12.6	33.9	23	05.3	18	19	02.5	16	02.1	03	01.0	05	02.4	21	02.8	03	03.0	07	02.7	07	04.3	09							
VII	708.8	18.5	27.3	21.5	22.2	28.5	13.8	36.4	18	07.0	28	31	02.2	11	02.1	01	02.0	03	01.3	10	01.8	06	01.8	06	03.2	12	03.2	13							
VIII	712.5	16.3	26.0	19.3	20.2	27.3	12.3	31.9	25	06.4	12	22	02.0	12	02.4	01	01.0	03	02.3	13	02.5	01	01.0	07	01.7	07	01.7	27							
IX	712.4	13.4	23.3	16.5	17.4	24.3	11.2	28.8	23	06.4	15	11	02.2	10	02.0	05	01.4	03	01.3	13	03.2	06	01.7	02	01.5	05	01.4	39							
X	712.7	07.3	17.5	10.1	11.2	18.4	05.8	30.0	18	-03.8	30	22	01.9	03	02.3	03	01.7	02	03.0	13	02.4	02	01.0	11	02.3	06	01.5	31							
XI	713.6	00.3	08.5	03.3	03.8	10.0	-01.6	18.0	17	-07.5	02	19	02.8	14	02.1	02	01.5	10	02.4	09	02.6	07	02.7	02	01.0	04	03.5	23							
XII	712.5	-01.8	02.8	-00.8	-00.2	04.4	-04.3	14.9	27	-18.0	07	17	01.8	14	01.9	04	02.2	08	01.9	11	03.4	05	02.6	05	01.8	06	01.7	23							
GDD.	711.3	07.4	14.8	09.8	10.4	16.1	04.8	38.4	48 VII	-18.0	7 XII	237	02.1	161	02.1	39	01.7	46	02.2	155	03.0	46	02.2	63	02.3	89	02.9	259							
$\varphi = 41^{\circ} 57' N$ $\lambda = 21^{\circ} 38' E$ Gr. $\Delta G = +1h 27 min.$																																			
SKOPJE															BR. ST. 267																				
I	747.1	-00.6	03.0	00.6	00.9	03.8	-01.4	09.2	22	-10.7	15	16	02.5	13	02.8	03	01.7	08	01.6	05	02.6	01	02.0	07	01.4	07	01.6	33							
II	738.8	00.2	06.9	02.5	03.0	08.3	-01.2	14.0	09	-13.9	27	16	02.2	09	02.8	04	01.2	08	02.4	04	02.8	04	01.0	08	02.4	07	01.7	24							
III	743.6	02.1	08.1	04.2	04.6	09.2	01.0	18.6	27	-03.8	02	23	02.6	09	02.7	05	01.6	12	02.3	08	02.1	.	.	01	02.0	11	02.3	24							
IV	738.3	07.5	15.6	10.2	10.9	16.8	04.7	24.0	10	-01.1	23	10	01.7	08	01.6	02	01.5	14	02.7	09	02.4	08	01.8	08	02.6	11	02.6	29							
V	742.4	14.0	22.1	15.8	16.9	23.5	10.0	31.3	23	04.3	12	13	03.5	09	02.6	09	01.3	15	01.7	10	01.4	.	.	03	01.7	05	02.0	29							
VI	741.6	17.4	25.8	19.4	20.5	27.0	12.7	33.6	23	04.4	18	11	02.5	07	03.1	06	02.0	16	02.1	09	02.4	.	.	07	02.3	09	02.2	25							
VII	738.8	19.1	27.9	21.4	22.4	29.6	15.6	37.0	18	08.8	29	14	03.1	08	02.9	09	01.4	05	01.8	10	01.4	05	01.8	09	01.8	11	02.5	22							
VIII	742.7	17.4	27.6	20.8	21.7	28.6	14.1	32.6	22	09.9	16	13	02.8	07	02.4	07	01.3	12	01.6	04	01.8	06	01.8	12	02.2	07	02.1	25							
IX	742.8	14.5	24.9	17.8	18.8	25.9	12.8	30.4	10	06.2	15	06	03.7	10	02.3	05	01.0	09	01.7	12	01.8	04	01.5	06	01.7	03	01.7	35							
X	743.8	07.9	18.6	11.1	12.2	19.6	06.5	30.3	18	-04.2	30	13	02.7	08	02.8	10	01.6	10	02.1	13	01.8	04	01.2	04	01.8	04	01.8	27							
XI	745.8	-00.4	07.8	02.7	03.2	09.1	-01.7	13.6	16	-07.8	29	16	02.8	10	02.7	10	01.0	04	01.5	03	01.7	03	01.7	09	01.4	04	02.0	31							
XII	744.9	-03.3	00.8	-02.1	-01.7	02.3	-05.3	14.1	27	-17.9	01	08	03.2	08	02.5	15	01.1	04	01.2	02	02.0	01	01.0	05	02.0	04	03.0	46							
GDD.	742.6	08.0	15.8	10.4	11.1	17.0	05.6	37.0	48 VII	-17.9	1 XII	159	02.7	106	02.6	85	01.3	117	02.0	89	01.9	36	01.6	79	02.0	83	02.2	341							
$\varphi = 41^{\circ} 59' N$ $\lambda = 21^{\circ} 31' E$ Gr. $\Delta G = +1h 26 min.$																																			
TRUBAREVO															BR. ST. 268																				
I	-	-00.4	03.7	00.9	01.3	05.3	-01.5	11.0	22	-10.4	15	.	.	02	01.5	03	01.0	18	01.1	06	01.0	32	01.0	02	01.0	04	01.0	26							
II	-	00.0	07.5	02.8	03.3	08.9	-01.5	14.0	10	-10.8	27	.	.	03	01.0	03	01.0	09	01.1	06	01.0	20	01.0	03	02.7	07	01.7	33							
III	-	02.3	09.1	04.5	05.1	10.3	01.3	18.6	27	-02.8	07	.	.	03	01.0	03	01.3	17	01.1	01	01.0	13	01.0	04	01.5	13	01.6	39							
IV	-	07.0	16.6	10.0	10.9	17.6	04.5	24.8	10	00.0	23	.	.	04	01.0	.	.	20	01.2	03	01.0	19	01.0	04	01.2	17	01.4	23							
V	-	13.3	23.5	16.2	17.3	24.4	16.4	32.2	24	05.0	12, 11	.	.	11	01.0	03	01.0	15	01.1	05	01.0	23	01.0	01	01.0	06	01.2	29							
VI	-	16.5	27.0	19.0	20.4	28.0	12.8	34.0	23	04.0	18	.	.	07	01.0	01	01.0	16	01.0	02	01.0	17	01.0	03	01.0	08	01.2	36							
VII	-	18.2	29.1	20.7	22.1	30.1	15.3	36.8	18	06.7	29	.	.	11	01.0	01	01.0	21	01.0	03	01.0	21	01.0	01	01.0	05	01.2	30							
VIII	-	15.9	28.5	19.8	21.0	29.5	13.8	33.6	21	10.0	12, 11	.	.	08	01.0	02	01.0	15	01.0	06	01.0	15	01.0	01	01.0	02	01.0	44							
IX	-	13.9	26.2	17.0	18.5	26.8	12.1	31.0	10, 08	05.2	15	01	01.0	03	01.0	.	.	16	01.1	08	01.0	25	01.0	04	01.0	04	01.0	29							
X	-	07.6	20.0	10.6	12.2	20.5	06.0	30.2	10	-03.8	30	.	.	05	01.0	02	01.0	21	01.0	06	01.0	26	01.1	02	01.0	06	01.0	25							
XI	-	00.0	08.0	01.9	03.1	09.5	-01.8	15.3	16	-08.2	29	02	01.0	03	01.0	01	01.0	11	01.0	06	01.0	26	01.0	04	01.0	09	01.2	28							
XII	-	-03.1	01.7	-01.8	-01.3	02.6	-05.3	08.0	23	-18.3	01	01	01.0	03	01.0	.	.	16	01.0	06	01.0	33	01.1	02	01.0	04	01.2	28							
GDD.	-	07.6	16.8	10.1	11.2	17.8	05.5	36.8	48 VII	-18.3	1 XII	04	01.0	63	01.0	19	01.0	195	01.1	58	01.0	270	01.0	31	01.3	85	01.3	370							
$\varphi = 41^{\circ} 20' N$ $\lambda = 21^{\circ} 34' E$ Gr. $\Delta G = +1h 26 min.$																																			
PRILEP															BR. ST. 269																				

1973

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetra nD, Pm (0-12)																
		Tm				Max	Min	Max	Det.	Min	Det.	N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dias)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	
φ = 41° 58' N λ = 22° 46' E Gr. ΔG = + 1h 31 min.												DELČEVO																BR. ST. 281
I	-	-01.4	02.9	-00.2	00.3	03.4	-02.6	08.6	22	-10.4	15	13	02.2	10	02.1	01	01.0	02	02.0	01	01.0	08	02.2	07	01.7	05	02.4	46
II	-	-00.8	05.6	02.0	02.2	06.6	-01.8	13.5	10	-15.5	28	12	01.8	04	01.8	02	01.5	02	03.0	05	04.0	04	01.7	09	01.8	13	02.5	31
III	-	-00.2	06.2	02.7	02.8	06.9	-00.7	17.0	27	-08.4	01	14	01.6	04	02.0	01	01.0	07	01.7	04	01.0	05	02.2	03	01.7	08	01.9	47
IV	-	06.1	13.9	08.7	09.3	14.8	05.1	22.0	09	-00.5	05	08	02.0	02	03.0	03	02.0	14	02.8	04	01.2	08	02.0	09	02.3	09	02.9	33
V	-	12.3	21.4	14.8	15.8	22.3	11.2	30.0	22	05.5	30	17	02.5	02	02.5	.	.	.	.	04	01.2	02	03.0	13	02.4	07	03.3	48
VI	-	15.8	23.8	17.8	18.8	24.7	12.9	31.5	23	05.0	18.17	21	02.1	03	02.7	01	02.0	17	02.2	08	01.5	03	02.0	03	02.0	02	02.5	32
VII	-	17.3	26.0	19.7	20.7	27.2	14.3	36.5	18	06.5	31	14	02.1	02	02.0	02	01.5	02	02.0	14	01.4	04	02.8	04	02.5	05	02.6	46
VIII	-	15.7	25.1	18.2	19.3	25.7	10.7	29.2	22	02.2	13	18	02.0	05	02.2	06	01.2	05	01.8	09	01.8	05	02.0	02	02.0	03	02.7	40
IX	-	12.9	23.4	15.5	16.8	24.0	09.8	30.0	24	03.0	15	13	02.0	01	02.0	01	01.0	02	02.0	06	01.5	06	01.5	03	02.3	09	02.0	49
X	-	06.0	17.2	09.2	10.4	17.8	04.2	28.5	18	-05.5	30	12	01.8	07	02.3	.	.	06	01.5	02	01.0	01	03.0	07	01.4	02	02.0	56
XI	-	-01.5	07.8	02.1	02.6	09.4	-02.8	16.5	17.07	-11.0	29	12	02.3	02	01.5	01	01.0	04	02.0	05	03.2	02	02.0	05	02.0	06	02.3	53
XII	-	-02.7	05.6	00.2	00.8	06.0	-04.7	13.5	27.26	-22.5	01	09	01.8	02	01.5	01	01.0	09	02.7	05	01.2	09	02.7	05	01.4	02	03.0	51
600.	-	06.6	14.9	09.2	10.0	15.7	04.6	36.5	45.0	-22.5	4.12	163	02.0	44	02.1	19	01.4	70	02.2	67	01.7	59	02.2	70	02.0	71	02.5	532
φ = 41° 43' N λ = 22° 51' E Gr. ΔG = + 1h 31 min.												BERČVO																BR. ST. 282
I	692.4	-03.3	01.5	-02.1	-01.5	02.3	-04.8	08.8	20.19	-16.2	15	21	01.9	.	.	.	.	05	02.0	02	01.0	01	01.0	01	01.0	02	01.0	61
II	685.5	-02.4	04.3	00.4	00.7	05.6	-04.0	13.7	08	-20.2	27	16	01.4	01	02.0	03	01.0	08	02.5	06	02.0	06	01.5	.	.	06	01.7	38
III	685.7	-02.3	04.3	00.6	00.8	05.5	-03.7	15.2	27	-15.7	01	30	01.5	01	01.0	02	01.5	06	01.5	03	01.7	05	01.8	.	.	10	01.6	36
IV	686.4	04.9	11.8	06.2	07.3	13.2	02.1	20.4	10	-02.5	23	15	01.3	04	01.2	.	.	11	02.5	09	03.1	09	02.3	.	.	08	01.5	32
V	691.0	11.6	19.8	12.8	14.3	20.9	06.4	28.4	06	00.8	15	22	02.2	01	02.0	.	.	02	01.5	01	03.0	08	02.5	02	02.0	09	01.9	48
VI	691.1	14.0	21.4	14.9	16.3	23.1	08.3	29.6	23	00.7	17	14	01.9	07	02.0	.	.	03	02.3	08	01.6	09	02.8	02	02.0	10	02.0	37
VII	686.7	15.4	23.2	16.6	18.0	24.8	10.8	32.4	18	04.2	29	07	01.6	02	02.0	.	.	05	01.4	01	02.0	13	02.2	04	02.0	11	01.8	50
VIII	692.3	13.2	23.2	15.2	16.7	24.6	06.8	28.3	22	04.3	16	14	01.9	03	01.7	.	.	04	02.0	.	.	03	03.7	03	01.7	03	02.0	63
IX	692.2	10.7	21.4	13.5	14.8	22.6	07.8	29.7	24	02.3	15	07	01.6	05	01.2	.	.	04	02.8	01	01.0	02	01.5	04	02.0	06	01.3	61
X	691.9	04.3	16.0	07.1	06.6	16.9	02.1	26.3	18	-08.5	30	20	01.7	01	02.0	01	01.0	02	01.5	05	02.2	04	02.5	02	01.5	03	02.0	55
XI	691.9	-02.8	07.6	-00.2	01.1	08.9	-05.1	16.3	17	-17.3	29	17	01.8	.	.	.	.	02	02.5	06	02.5	03	02.0	01	03.0	09	01.4	52
XII	691.0	-03.9	04.7	-01.0	-00.3	05.8	-06.1	12.4	24	-23.7	01	06	02.5	02	01.0	.	.	07	01.4	12	02.1	02	01.5	01	01.0	01	01.0	62
600.	690.3	05.0	13.3	07.0	08.1	14.5	01.9	32.4	48.0	-23.7	6.12	185	01.7	27	01.6	06	01.2	59	02.0	54	02.2	65	02.3	20	01.9	78	01.7	595

